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FAULT CURRENT CALCULATION IN INDUSTRIAL POWER SYSTEMS

Jae-Ryong Hwang

A MAJOR TECHNICAL REPORT  
in the  
Faculty of Engineering

Presented in partial fulfilment of the requirements for  
the Degree of Master of Engineering at  
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ABSTRACT

FAULT CURRENT CALCULATION  
IN INDUSTRIAL POWER SYSTEMS

Jae-Ryong Hwang

Two methods of constructing the bus impedance matrix ( $Z_{BUS}$ ) are reviewed.

Also, basic formulae to be used for the calculation of fault current based on the  $Z_{BUS}$  are derived.

Practical fault current calculation methods recommended by two ANSI standards are described.

Finally, an efficient and convenient computer program, incorporating the theory described in this report and necessary recommendations of the ANSI standards, is developed and presented.

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## 1. INTRODUCTION

Nowadays most of the fault current studies are done with the bus impedance matrix ( $Z_{BUS}$ ), or a driving point and transfer impedance matrix for a multi-terminal network.

Two methods of constructing  $Z_{BUS}$  are reviewed.

One is a basic topological method, which consists of formation of a bus admittance matrix ( $Y_{BUS}$ ) and inversion of it to give  $Z_{BUS}$ .

The other is a method developed by Stagg, et. al. (1,2) which efficiently constructs  $Z_{BUS}$  directly from line information without any inversion operation of matrix.

Basic formulae to be used for the calculation of circuit values based on  $Z_{BUS}$ , incidence matrix, and primitive network matrix are, then, derived.

Simplified methods for considering the transient component of fault current and correction factors for machine impedances to take into account the change of them during transient period are described as recommended by ANSI C37.010-1972 and C37.13-1973.

Finally a digital computer program using the algorithm developed by Stagg, et. al., incorporating all necessary requirements and recommendations of the ANSI standards, and equipped with a maximum degree of flexibility, efficiency, and abundant option features, is developed.

In the appendix, a User Manual for the use of the program, the whole copy of the program in Fortran version, and several sample runnings are included.



## 2. ZBUS CONSTRUCTION

### 2.1 Singular Transformation

#### 2.1.1 Incidence matrices

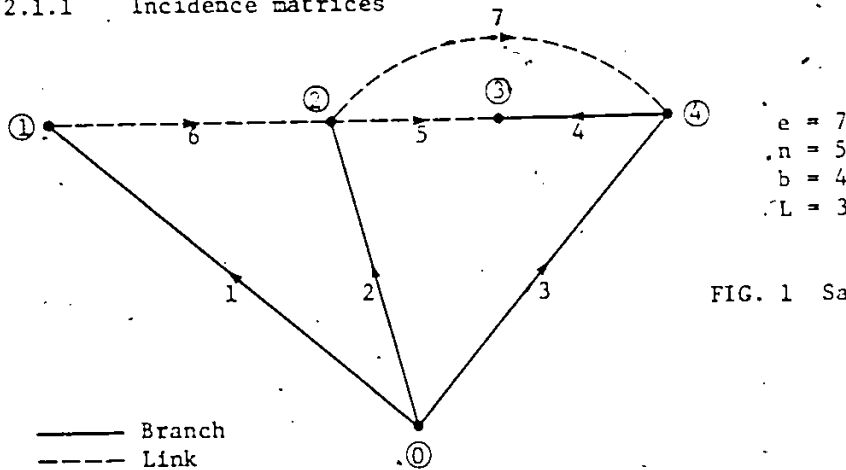


FIG. 1 Sample Graph

#### Element-node incidence matrix $A$

The incidence of elements to nodes in a connected graph is shown by the element-node incidence matrix. The elements of the matrix are as follows:  
 $a_{ij} = 1$  if the  $i$  th element is incident to and oriented away from the  $j$  th node

$a_{ij} = -1$  if the  $i$  th element is incident to and oriented toward the  $j$  th node

$a_{ij} = 0$  if the  $i$  th element is not incident to the  $j$  th node

The dimension of the matrix is  $e \times n$ , where  $e$  is the number of elements and  $n$  is the number of nodes in the graph. The element-node incidence matrix for the graph shown in Fig. 1 is equation (1).

$$\bar{A} = \begin{array}{c|cccccc} & n & & & & & \\ \hline e & & 0 & 1 & 2 & 3 & 4 \\ \hline 1 & & 1 & -1 & & & \\ 2 & & 1 & & -1 & & \\ 3 & & 1 & & & & -1 \\ 4 & & & & & -1 & 1 \\ 5 & & & & 1 & -1 & \\ 6 & & & 1 & -1 & & \\ 7 & & & & 1 & & -1 \end{array} \quad (1)$$

Since

$$\sum_{j=0}^n a_{ij} = 0 \quad i = 1, 2, \dots, e$$

the columns of  $\bar{A}$  are linearly dependent. Hence, the rank of  $\bar{A} < n$ .

Bus incidence matrix A

Any node of a connected graph can be selected as the reference node.

Then, the variables of the other nodes, referred to as buses, can be measured with respect to the assigned reference. The matrix obtained

$$A = \begin{array}{c|cccc} & \text{bus} & & & & \\ \hline e & & 1 & 2 & 3 & 4 \\ \hline 1 & & -1 & & & \\ 2 & & & -1 & & \\ 3 & & & & & -1 \\ 4 & & & & -1 & 1 \\ 5 & & & 1 & -1 & \\ 6 & & 1 & -1 & & \\ 7 & & & 1 & & -1 \end{array} \quad (2)$$

from  $A$  by deleting the column corresponding to the reference node is the element-bus incidence matrix  $A$ , which will be called the bus incidence matrix. The dimension of this matrix is  $e \times (n - 1)$  and the rank is  $n - 1 = b$ , where  $b$  is the number of branches in the graph. Selecting node 0 as reference for the graph shown in Fig. 1,  $A$  is equation (2). This matrix is rectangular and therefore singular.

If the rows of  $A$  are arranged according to a particular tree, the matrix can be partitioned into submatrices  $A_b$  of dimension  $b \times (n - 1)$  and  $A_L$  of dimension  $L \times (n - 1)$ , where the rows of  $A_b$  correspond to branches and the rows of  $A_L$  to links. The partitioned matrix for the graph shown in Fig. 1 is equation (3).

	bus	1	2	3	4
e					
1		-1			
2			-1		
3					-1
4				-1	1
5			1	-1	
6		1	-1		
7			1		-1

$A =$

	bus	Buses
e		
		$A_b$
		$A_L$

(3)

$A_L$  is a nonsingular square matrix with rank  $(n - 1)$ .

Float network element-bus incidence matrix  $A_f$

If all the elements incident to bus 0 are eliminated, the remaining network constitutes a reduced or "float" network, for which the topology may be described by an element-bus incidence matrix.

This matrix,  $A_f$ , is obtained by partitioning  $A$  provided the rows



The performance equation of an element in impedance form is

$$v_{pq} + e_{pq} = z_{pq} i_{pq} \quad (5)$$

or in admittance form is

$$i_{pq} + j_{pq} = y_{pq} v_{pq} \quad (6)$$

The parallel source current in admittance form is related to the series source voltage in impedance form by

$$j_{pq} = -y_{pq} e_{pq} \quad (7)$$

A set of unconnected elements is defined as a primitive network. The performance equations of a primitive network can be derived from (5) or (6) by expressing the variables as vectors and the parameters as matrices. The performance equation in impedance form is

$$\bar{v} + \bar{e} = (z) \bar{i} \quad (8)$$

or in admittance form is

$$\bar{i} + \bar{j} = (y) \bar{v} \quad (9)$$

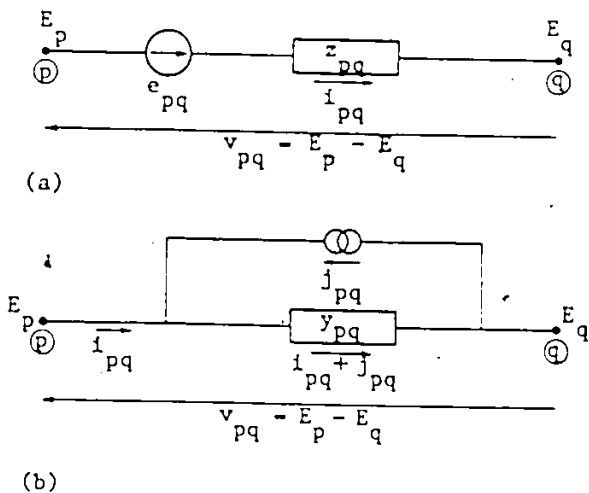


Fig. 2  
Representations of a  
network component.

- (a) Impedance form
- (b) Admittance form

A diagonal element of the matrix  $(z)$  or  $(y)$  of the primitive network is the self-impedance  $z_{pq,pq}$  or self-admittance  $y_{pq,pq}$ . An off-diagonal element is the mutual impedance  $z_{pq,rs}$  or the mutual admittance  $y_{pq,rs}$  between the elements  $p-q$  and  $r-s$ . The primitive admittance matrix  $(y)$  can be obtained by inverting the primitive impedance matrix  $(z)$ . The matrices  $(z)$  and  $(y)$  are diagonal matrices if there is no mutual coupling between elements. In this case the self-impedances are equal to the reciprocals of the corresponding self-admittances.

The relationship between  $\bar{e}$  and  $\bar{j}$  in equations (8) and (9) is

$$(z)\bar{j} = -\bar{e} \quad (10)$$

### 2.1.3 Formation of network matrices by singular transformations

#### Network performance equations

A network is made up of an interconnected set of elements. In the bus frame of reference, the performance of an interconnected network is described by  $n - 1$  independent nodal equations, where  $n$  is the number of nodes. In matrix notation, the performance equation in impedance form is

$$\bar{E}_{BUS} = Z_{BUS}\bar{I}_{BUS} \quad (11)$$

or in admittance form is

$$\bar{I}_{BUS} = Y_{BUS}\bar{E}_{BUS} \quad (12)$$

where  $\bar{E}_{BUS}$  = vector of bus voltages measured with respect to the reference bus

$\bar{I}_{BUS}$  = vector of impressed bus currents

$Z_{BUS}$  = bus impedance matrix whose elements are open circuit driving point and transfer impedances

$Y_{BUS}$  = bus admittance matrix whose elements are short circuit driving point and transfer admittances

Bus admittance and bus impedance matrices

The bus admittance matrix  $Y_{BUS}$  can be obtained by using the bus incidence matrix  $A$  to relate the variables and parameters of the primitive network to bus quantities of the interconnected network. The performance equation of the primitive network

$$\bar{i} + \bar{j} = (y)\bar{v}$$

is premultiplied by  $A^t$ , the transpose of the bus incidence matrix, to obtain

$$A^t \bar{i} + A^t \bar{j} = A^t (y) \bar{v} \quad (13)$$

Since the matrix  $A$  shows the incidence of elements to buses,  $A^t \bar{i}$  is a vector in which each element is the algebraic sum of the currents leaving the bus. In accordance with Kirchhoff's current law, the algebraic sum of the currents at a bus is zero. Then

$$A^t \bar{i} = 0 \quad (14)$$

Similarly,  $A^t \bar{j}$  gives the algebraic sum of the source currents at each bus and equals the vector of impressed bus currents. Therefore

$$\bar{i}_{BUS} = A^t \bar{j} \quad (15)$$

Substituting from equations (14) and (15) into (13) yields

$$\bar{i}_{BUS} = A^t (y) \bar{v} \quad (16)$$

Power into the network is  $(\bar{i}_{BUS}^*)^t \bar{E}_{BUS}$  and the sum of the powers in the primitive network is  $(\bar{j}^*)^t \bar{v}$ . The power in the primitive and interconnected networks must be equal, that is, the transformation of variables must be power-invariant. Hence

$$(\bar{i}_{BUS}^*)^t \bar{E}_{BUS} = (\bar{j}^*)^t \bar{v} \quad (17)$$

Taking the conjugate transpose of equation (15)

$$(\bar{i}_{BUS}^*)^t = (\bar{j}^*)^t A^*$$

Since A is a real matrix

$$A^* = A$$

and

$$(\bar{I}_{BUS}^*)^t = (\bar{J}^*)^t A \quad (18)$$

Substituting from equation (18) into (17)

$$(\bar{J}^*)^t A \bar{E}_{BUS} = (\bar{J}^*)^t \bar{v}$$

Since this equation is valid for all values of  $\bar{J}$ , it follows that

$$A \bar{E}_{BUS} = \bar{v} \quad (19)$$

Substituting from equation (19) into (16)

$$\bar{I}_{BUS} = A^t(y) A \bar{E}_{BUS} \quad (20)$$

Since the performance equation of the network is

$$\bar{I}_{BUS} = Y_{BUS} \bar{E}_{BUS} \quad (21)$$

it follows from equations (20) and (21) that

$$Y_{BUS} = A^t(y) A$$

The bus incidence matrix A is singular and therefore  $A^t(y)A$  is a singular transformation of  $(y)$ .

The bus impedance matrix can be obtained from

$$Z_{BUS} = Y_{BUS}^{-1} = (A^t(y)A)^{-1} \quad (22)$$

## 2.2 Direct Method

### 2.2.1 Introduction

The methods presented in the previous section require transformation and inversion of matrices to obtain network matrices. An alternative method based on an algorithm can be used to form the bus impedance



matrix directly from system parameters and coded bus numbers. The underlying principle of the algorithm is the formation of the bus impedance matrix in steps, simulating the construction of the network by adding one element at a time.<sup>(1,2)</sup> A matrix is formed for the partial network represented after each element is connected to the network.

Most of the following description is direct quotation from Stagg's book.<sup>(2)</sup>

### 2.2.2 Algorithm for formation of bus impedance matrix

#### Performance equation of a partial network

Assume that the bus impedance matrix  $Z_{BUS}$  is known for a partial network of  $m$  buses and a reference node 0. The performance equation of this network, shown in Fig. 3, is

$$\bar{E}_{BUS} = Z_{BUS} \bar{I}_{BUS} \tag{23}$$

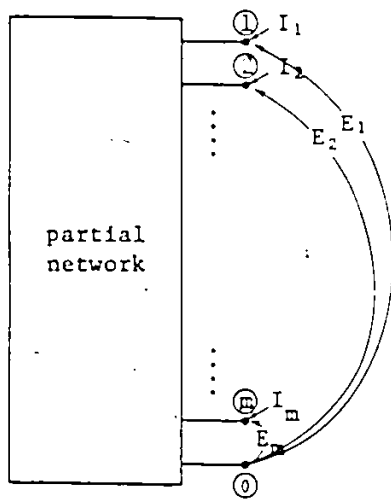
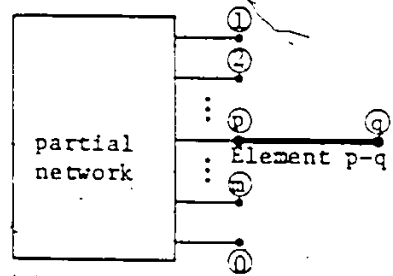
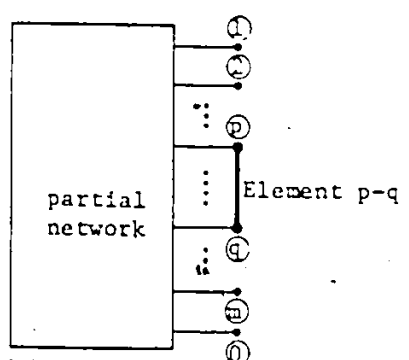


Fig. 3 Representation of a partial network.



(a)



(b)

Fig. 4 Representations of a partial network with an added element.

- (a) Addition of a branch
- (b) Addition of a link.

where  $\bar{E}_{BUS}$  = an  $m \times 1$  vector of bus voltages measured with respect to the reference node

$\bar{I}_{BUS}$  = an  $m \times 1$  vector of impressed bus currents

Where an element p-q is added to the partial network, it may be a branch or a link as shown in Fig. 4.

If p-q is a branch, a new bus q is added to the partial network and the resultant bus impedance matrix is of dimension  $(m + 1) \times (m + 1)$ . The new voltage and current vectors are of dimension  $(m + 1) \times 1$ . To determine the new bus impedance matrix requires only the calculation of the elements in the new row and column.

If p-q is a link, no new bus is added to the partial network. In this case, the dimensions of the matrices in the performance equation are unchanged, but all the elements of the bus impedance matrix must be

recalculated to include the effect of the added link.

Addition of a branch

The performance equation for the partial network with an added branch p-q is

		1			p		m	q	
E <sub>1</sub>	1	Z <sub>11</sub>	Z <sub>12</sub>	...	Z <sub>1p</sub>	...	Z <sub>1m</sub>	Z <sub>1q</sub>	I <sub>1</sub>
E <sub>2</sub>		Z <sub>21</sub>	Z <sub>22</sub>	...	Z <sub>2p</sub>	...	Z <sub>2m</sub>	Z <sub>2q</sub>	I <sub>2</sub>
⋮		⋮	⋮	⋮	⋮	⋮	⋮	⋮	⋮
E <sub>p</sub>	p	Z <sub>p1</sub>	Z <sub>p2</sub>	...	Z <sub>pp</sub>	...	Z <sub>pm</sub>	Z <sub>pq</sub>	I <sub>p</sub>
⋮		⋮	⋮	⋮	⋮	⋮	⋮	⋮	⋮
E <sub>m</sub>	m	Z <sub>m1</sub>	Z <sub>m2</sub>	...	Z <sub>mp</sub>	...	Z <sub>mm</sub>	Z <sub>mq</sub>	I <sub>m</sub>
E <sub>q</sub>	q	Z <sub>q1</sub>	Z <sub>q2</sub>	...	Z <sub>qp</sub>	...	Z <sub>qm</sub>	Z <sub>qq</sub>	I <sub>q</sub>

(24)

It is assumed that the network consists of bilateral passive elements. Hence  $Z_{qi} = Z_{iq}$  where  $i = 1, 2, \dots, m$  and refers to the buses of the partial network, not including the new bus q. The added branch p-q is assumed to be mutually coupled with one or more elements of the partial network.

The elements  $Z_{qi}$  can be determined by injecting a current at the i th bus and calculating the voltage at the q th bus with respect to the reference node as shown in Fig. 5. Since all other bus currents equal zero, it follows from equation (24) that

$$\begin{aligned}
 E_1 &= Z_{1i} I_i \\
 E_2 &= Z_{2i} I_i \\
 &\vdots \\
 E_p &= Z_{pi} I_i \\
 &\vdots
 \end{aligned}$$

(25)

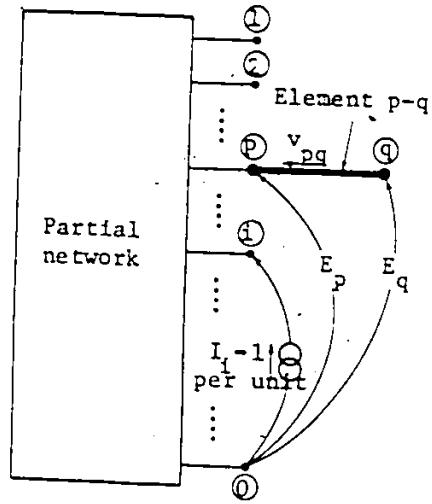


Fig. 5 Injected current and bus voltages for calculation of  $Z_{qi}$

$$E_m = Z_{mi} I_i$$

$$E_q = Z_{qi} I_i$$

Letting  $I_i = 1$  per unit in equations (25),  $Z_{qi}$  can be obtained directly by calculating  $E_q$ .

The bus voltages associated with the added element and the voltage across the element are related by

$$E_q = E_p - v_{pq} \tag{26}$$

The currents in the elements of the network in Fig. 5 are expressed in terms of the primitive admittances and the voltages across the elements by

$$\begin{bmatrix} i_{pq} \\ i_{rs} \end{bmatrix} = \begin{bmatrix} y_{pq,pq} & y_{pq,rs} \\ y_{rs,pq} & y_{rs,rs} \end{bmatrix} \begin{bmatrix} v_{pq} \\ v_{rs} \end{bmatrix} \tag{27}$$

In equation (27) pq is a fixed subscript and refers to the added element

and  $rs$  is a variable subscript and refers to all other elements. Then,

$i_{pq}$  and  $v_{pq}$  are, respectively, current through and voltage across the added element

$\bar{i}_{rs}$  and  $\bar{v}_{rs}$  are the current and voltage vectors of the elements of the partial network

$y_{pq,pq}$  is the self-admittance of the added element

$\bar{y}_{pq,rs}$  is the vector of mutual admittances between the added element  $p-q$  and the elements  $r-s$  of the partial network

$\bar{y}_{rs,pq}$  is the transpose of the vector  $\bar{y}_{pq,rs}$

$\begin{pmatrix} y_{rs,rs} \end{pmatrix}$  is the primitive admittance matrix of the partial network

The current in the added branch, shown in Fig. 5, is

$$i_{pq} = 0 \quad (28)$$

However  $v_{pq}$  is not equal to zero since the added branch is mutually coupled to one or more of the elements of the partial network. Moreover,

$$\bar{v}_{rs} = \bar{E}_r - \bar{E}_s \quad (29)$$

where  $\bar{E}_r$  and  $\bar{E}_s$  are the voltages at the buses in the partial network.

From equations (27 and 28),

$$i_{pq} = y_{pq,pq} v_{pq} + \bar{y}_{pq,rs} \bar{v}_{rs} = 0$$

and therefore,

$$v_{pq} = - \frac{\bar{y}_{pq,rs} \bar{v}_{rs}}{y_{pq,pq}} \quad (30)$$

Substituting for  $\bar{v}_{rs}$  from equation (29),

$$v_{pq} = - \frac{\bar{y}_{pq,rs} (\bar{E}_r - \bar{E}_s)}{y_{pq,pq}} \quad (31)$$

Substituting for  $v_{pq}$  in equation (26) from (31),

$$E_q = E_p + \frac{\bar{y}_{pq,rs}(\bar{E}_r - \bar{E}_s)}{y_{pq,pq}}$$

Finally, substituting for  $E_q$ ,  $E_p$ ,  $\bar{E}_r$  and  $\bar{E}_s$  from equation (25) with

$$I_i = 1,$$

$$Z_{qi} = Z_{pi} + \frac{\bar{y}_{pq,rs}(\bar{Z}_{ri} - \bar{Z}_{si})}{y_{pq,pq}} \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq q \end{matrix} \quad (32)$$

The element  $Z_{qq}$  can be calculated by injecting a current at the  $q$ th bus and calculating the voltage at that bus. Since all other bus currents equal zero, it follows from equation (24) that

$$E_1 = Z_{1q} I_q$$

$$E_2 = Z_{2q} I_q$$

⋮

$$E_p = Z_{pq} I_q$$

⋮

$$E_m = Z_{mq} I_q$$

$$E_q = Z_{qq} I_q$$

(33)

Letting  $I_q = 1$  per unit in equations (33),  $Z_{qq}$  can be obtained directly by calculating  $E_q$ .

The voltages at buses  $p$  and  $q$  are related by equation (26), and the current through the added element is

$$i_{pq} = -I_q = -1 \quad (34)$$

The voltages across the elements of the partial network are given by equation (29) and the currents through these elements by (27). From equations (27) and (34),

$$i_{pq} = y_{pq,pq} v_{pq} + \bar{y}_{pq,rs} \bar{v}_{rs} = -1$$

and therefore,

$$v_{pq} = - \frac{1 + \bar{y}_{pq,rs} \bar{v}_{rs}}{y_{pq,pq}}$$

Substituting for  $\bar{v}_{rs}$  from equation (29),

$$v_{pq} = - \frac{1 + \bar{y}_{pq,rs} (\bar{E}_r - \bar{E}_s)}{y_{pq,pq}} \quad (35)$$

Substituting for  $v_{pq}$  in equation (26) from (35),

$$E_q = E_p + \frac{1 + \bar{y}_{pq,rs} (\bar{E}_r - \bar{E}_s)}{y_{pq,pq}}$$

Finally, substituting for  $E_q$ ,  $E_p$ ,  $\bar{E}_r$  and  $\bar{E}_s$  from equation (33) with

$$I_q = 1,$$

$$Z_{qq} = Z_{pq} + \frac{1 + \bar{y}_{pq,rs} (\bar{Z}_{rq} - \bar{Z}_{sq})}{y_{pq,pq}} \quad (36)$$

If there is no mutual coupling between the added branch and other elements of the partial network, then the elements of  $\bar{y}_{pq,rs}$  are zero and

$$z_{pq,pq} = \frac{1}{y_{pq,pq}} \quad (37)$$

It follows from equation (32) that

$$Z_{qi} = Z_{pi} \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq q \end{matrix} \quad (38)$$

and from equation (36) that

$$Z_{qq} = Z_{pq} + z_{pq,pq} \quad (39)$$

Furthermore, if there is no mutual coupling and p is the reference node,

$$Z_{pi} = 0 \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq q \end{matrix} \quad (40)$$

and

$$Z_{qi} = 0 \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq q \end{matrix} \quad (41)$$

Also

$$Z_{pq} = 0 \quad (42)$$

and therefore,

$$Z_{qq} = z_{pq,pq} \quad (43)$$

Addition of a link

If the added element p-q is a link, the procedure for recalculating the elements of the bus impedance matrix is to connect in series with the added element a voltage source  $e_t$  as shown in Fig. 6. This creates a

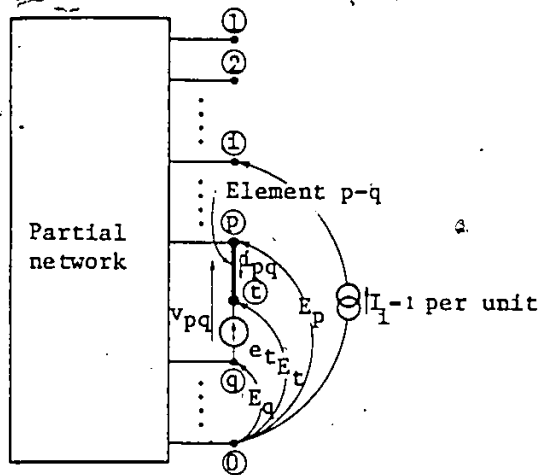


Fig. 6 Injected current voltage source in series with added link and bus voltages for calculation of  $Z_{ti}$ .

fictitious node t which will be eliminated later. The voltage source  $e_t$  is selected such that the current through the added link is zero.



The performance equation for the partial network with the added element p-t and the series voltage source  $e_t$  is

		1		p		m	t		
$E_1$	1	$Z_{11}$	$Z_{12}$	...	$Z_{1p}$	...	$Z_{1m}$	$Z_{1t}$	$I_1$
$E_2$		$Z_{21}$	$Z_{22}$	...	$Z_{2p}$	...	$Z_{2m}$	$Z_{2t}$	$I_2$
$\vdots$		$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$E_p$	= p	$Z_{p1}$	$Z_{p2}$	...	$Z_{pp}$	...	$Z_{pm}$	$Z_{pt}$	$I_p$
$\vdots$		$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$	$\vdots$
$E_m$	m	$Z_{m1}$	$Z_{m2}$	...	$Z_{mp}$	...	$Z_{mm}$	$Z_{mt}$	$I_m$
$e_t$	t	$Z_{t1}$	$Z_{t2}$	...	$Z_{tp}$	...	$Z_{tm}$	$Z_{tt}$	$I_t$

(44)

Since

$$e_t = E_t - E_q$$

the element  $Z_{ti}$  can be determined by injecting a current at the  $i$ th bus and calculating the voltage at the  $t$ th node with respect to bus  $q$ .

Since all other bus currents equal zero, it follows from equation (44)

that

$$E_k = Z_{ki} I_i \quad k = 1, 2, \dots, m$$

$$e_t = Z_{ti} I_i \tag{45}$$

Letting  $I_i = 1$  per unit in equations (45),  $Z_{ti}$  can be obtained directly by calculating  $e_t$ .

The series voltage source is

$$e_t = E_p - E_q - v_{pt} \tag{46}$$

Since the current through the added link is

$$i_{pq} = 0$$

the element p-t can be treated as a branch. The current in this element in terms of primitive admittances and the voltages across the elements is

$$i_{pt} = y_{pt,pt} v_{pt} + \bar{y}_{pt,rs} \bar{v}_{rs}$$

where

$$i_{pt} = i_{pq} = 0$$

Therefore

$$v_{pt} = - \frac{\bar{y}_{pt,rs} \bar{v}_{rs}}{y_{pt,pt}}$$

Since

$$\bar{y}_{pt,rs} = \bar{y}_{pq,rs} \quad \text{and} \quad y_{pt,pt} = y_{pq,pq}$$

then

$$v_{pt} = - \frac{\bar{y}_{pq,rs} \bar{v}_{rs}}{y_{pq,pq}} \tag{47}$$

Substituting in order from equations (47), (29), and (45) with  $I_i = 1$  into equation (46) yields

$$Z_{ti} = Z_{pi} - Z_{qi} + \frac{\bar{y}_{pq,rs} (\bar{Z}_{ri} - \bar{Z}_{si})}{y_{pq,pq}} \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq t \end{matrix} \tag{48}$$

The element  $Z_{tt}$  can be calculated by injecting a current at the t th bus with bus q as reference and calculating the voltage at the t th bus with respect to bus q. Since all other bus currents equal zero, it follows from equation (44) that

$$\begin{aligned} E_k &= Z_{kt} I_t \quad k = 1, 2, \dots, m \\ e_t &= Z_{tt} I_t \end{aligned} \tag{49}$$

Letting  $I_t = 1$  per unit in equation (49),  $Z_{tt}$  can be obtained directly by calculating  $e_t$ .

The current in the element p-t is

$$i_{pt} = -I_t = -1$$

This current in terms of primitive admittances and the voltages across the elements is

$$i_{pt} = y_{pt,pt} v_{pt} + \bar{y}_{pt,rs} \bar{v}_{rs} = -1$$

Again, since

$$\bar{y}_{pt,rs} = \bar{y}_{pq,rs} \quad \text{and} \quad y_{pt,pt} = y_{pq,pq}$$

then

$$v_{pt} = - \frac{1 + \bar{y}_{pq,rs} \bar{v}_{rs}}{y_{pq,pq}} \quad (50)$$

Substituting in order from equations (50), (29), and (49) with  $I_t = 1$  into (46) yields

$$Z_{tt} = Z_{pt} - Z_{qt} + \frac{1 + \bar{y}_{pq,rs} (\bar{Z}_{rt} - \bar{Z}_{st})}{y_{pq,pq}} \quad (51)$$

If there is no mutual coupling between the added element and other elements of the partial network, the elements of  $\bar{y}_{pq,rs}$  are zero and

$$z_{pq,pq} = \frac{1}{y_{pq,pq}} \quad (52)$$

It follows from equation (48) that

$$Z_{ti} = Z_{pi} - Z_{qi} \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq t \end{matrix} \quad (53)$$

and from equation (51),

$$Z_{tt} = Z_{pt} - Z_{qt} + z_{pq,pq} \quad (54)$$

Furthermore, if there is no mutual coupling and p is the reference node,

$$Z_{pi} = 0 \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq t \end{matrix} \quad (55)$$

and

$$Z_{ti} = -Z_{qi} \quad \begin{matrix} i = 1, 2, \dots, m \\ i \neq t \end{matrix} \quad (56)$$

Also

$$Z_{pt} = 0 \quad (57)$$

and therefore,

$$Z_{tt} = -Z_{qt} + z_{pq,pq} \quad (58)$$

The elements in the  $t$ th row and column of the bus impedance matrix for the augmented partial network are found from equations (48) and (51). It remains to calculate the required bus impedance matrix to include the effect of the added link. This can be accomplished by modifying the elements  $Z_{ij}$ , where  $i, j = 1, 2, \dots, m$ , and eliminating the  $t$ th row and column corresponding to the fictitious node.

The fictitious node  $t$  is eliminated by short circuiting the series voltage source  $e_t$ . From equation (44),

$$\bar{E}_{BUS} = Z_{BUS} \bar{I}_{BUS} + \bar{Z}_{it} I_t \quad (59)$$

and

$$e_t = \bar{Z}_{tj} \bar{I}_{BUS} + Z_{tt} I_t = 0 \quad (60)$$

where  $i, j = 1, 2, \dots, m$ . Solving for  $I_t$  from equation (60) and substituting into (59)

$$\bar{E}_{BUS} = \left( Z_{BUS} - \frac{\bar{Z}_{it} \bar{Z}_{tj}}{Z_{tt}} \right) \bar{I}_{BUS} \quad (61)$$

which is the performance equation of the partial network including the link  $p$ - $q$ . It follows that the required bus impedance matrix is

$$Z_{BUS(\text{modified})} = Z_{BUS(\text{before elimination})} - \frac{\bar{Z}_{it} \bar{Z}_{tj}}{Z_{tt}} \quad (62)$$

where any element of  $Z_{BUS}(\text{modified})$  is

$$Z_{ij}(\text{modified}) = Z_{ij}(\text{before elimination}) - \frac{Z_{it}Z_{tj}}{Z_{tt}} \quad (63)$$

A summary of the equations for the formation of the bus impedance matrix is given in Table 1.

Table 1 Summary of equations for formation of bus impedance matrix

	Add p-q	p is not the reference bus	p is the reference bus
With mutual coupling	Branch	$Z_{qi} = Z_{pi} + \frac{\bar{y}_{pq,rs}(\bar{z}_{ri} - \bar{z}_{si})}{\bar{y}_{pq,rs}}$ $i = 1, 2, \dots, n$ $i \neq p$ $Z_{pp} = Z_{pp} + \frac{1 + \bar{y}_{pq,rs}(\bar{z}_{rp} - \bar{z}_{sp})}{\bar{y}_{pq,rs}}$	$Z_{qi} = \frac{\bar{y}_{pq,rs}(\bar{z}_{ri} - \bar{z}_{si})}{\bar{y}_{pq,rs}}$ $i = 1, 2, \dots, n$ $i \neq p$ $Z_{pp} = \frac{1 + \bar{y}_{pq,rs}(\bar{z}_{rp} - \bar{z}_{sp})}{\bar{y}_{pq,rs}}$
	Link	$Z_{ti} = Z_{pi} - Z_{qi} + \frac{\bar{y}_{pq,rs}(\bar{z}_{ri} - \bar{z}_{si})}{\bar{y}_{pq,rs}}$ $i = 1, 2, \dots, n$ $i \neq t$ $Z_{tt} = Z_{pt} - Z_{qt} + \frac{1 + \bar{y}_{pq,rs}(\bar{z}_{rt} - \bar{z}_{st})}{\bar{y}_{pq,rs}}$	$Z_{ti} = -Z_{qi} + \frac{\bar{y}_{pq,rs}(\bar{z}_{ri} - \bar{z}_{si})}{\bar{y}_{pq,rs}}$ $i = 1, 2, \dots, n$ $i \neq t$ $Z_{tt} = -Z_{qt} + \frac{1 + \bar{y}_{pq,rs}(\bar{z}_{rt} - \bar{z}_{st})}{\bar{y}_{pq,rs}}$
Without mutual coupling	Branch	$Z_{qi} = Z_{pi}$ $i = 1, 2, \dots, n$ $i \neq p$ $Z_{pp} = Z_{pp} + x_{pp,rs}$	$Z_{qi} = 0$ $i = 1, 2, \dots, n$ $i \neq p$ $Z_{pp} = x_{pp,rs}$
	Link	$Z_{ti} = Z_{pi} - Z_{qi}$ $i = 1, 2, \dots, n$ $i \neq t$ $Z_{tt} = Z_{pt} - Z_{qt} + x_{pp,rs}$	$Z_{ti} = -Z_{qi}$ $i = 1, 2, \dots, n$ $i \neq t$ $Z_{tt} = -Z_{qt} + x_{pp,rs}$

### 3. SHORT CIRCUIT NETWORK AND CIRCUIT VALUES

#### 3.1 Short Circuit Network

An example of a short circuit network for 3-phase short circuit is shown in Fig. 7.

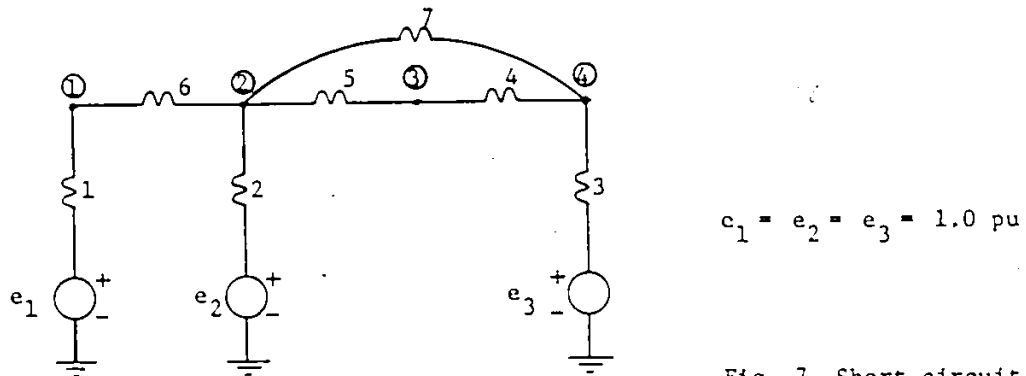


Fig. 7 Short circuit network with constant voltage-sources

In this network all the circuit parameters are generally given in p.u. All the sources of fault current - generator, motor, utility system, etc. - are assumed to be in phase and represented by 1.0 pu constant voltage sources together with their appropriate transient or sub-transient impedances.

To take advantage of  $Z_{BUS}$ , it is also worthwhile to convert voltage sources to constant current sources. Fig. 8 shows the resultant circuit with equivalent bus-current sources. Note that in the S.C. network, no link contains sources.

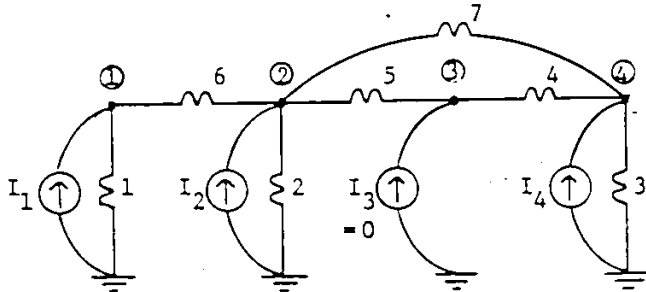


Fig. 8 Short circuit network with constant bus-current sources.

The values of bus-current sources may be obtained from primitive voltage-sources by

$$\bar{j} = - (z)^{-1} \bar{e}$$

$$\bar{I}_{BUS} = A^t \bar{j} \tag{64}$$

Restricting the analysis only to actual electrical power system short circuit network, no source impedance has mutual coupling with any other network impedance. Thus,

$$\bar{I}_{BUS} = \begin{bmatrix} \frac{1.0}{z'_{1,0}} \\ \frac{1.0}{z'_{2,0}} \\ \vdots \\ \frac{1.0}{z'_{n,0}} \end{bmatrix} = \begin{bmatrix} y'_{1,0} \\ y'_{2,0} \\ \vdots \\ y'_{n,0} \end{bmatrix} \tag{65}$$

where  $z'_{1,0}$ , for instance, is the total impedance of the sources connected to the bus 1.

3.2 Circuit Values

Generally the following relationship stands.

$$\bar{E}_{BUS} = Z_{BUS} \bar{I}_{BUS}$$

or

$$\begin{bmatrix} E_1 \\ E_2 \\ \vdots \\ E_n \end{bmatrix} = \begin{bmatrix} Z_{11} & \dots & Z_{1n} \\ \vdots & \ddots & \vdots \\ Z_{n1} & \dots & Z_{nn} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \end{bmatrix}$$

By inspecting Fig. 7, it can be seen that, before fault,

$$\begin{bmatrix} E_1 \\ E_2 \\ \vdots \\ E_n \end{bmatrix} = \begin{bmatrix} 1.0 \\ 1.0 \\ \vdots \\ 1.0 \end{bmatrix} = \begin{bmatrix} Z_{11} & \dots & Z_{1n} \\ \vdots & \ddots & \vdots \\ Z_{n1} & \dots & Z_{nn} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \end{bmatrix} \tag{66}$$

If fault occurs at jth bus, the fault current can be obtained

by Thevenin theorem:

$$I_F = \frac{1.0}{Z_{jj}}$$

Having a fault at this bus is identical to connecting a new current source

$I_F$  flowing from the jth bus to ground, as shown in Fig. 9.



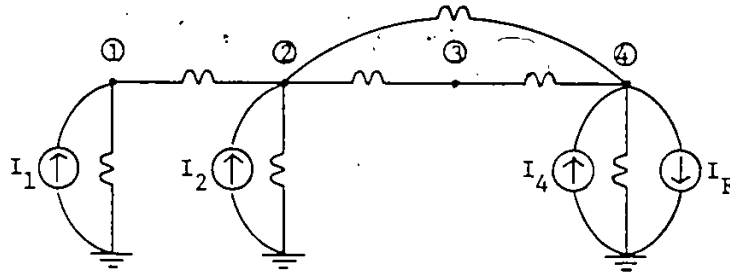


Fig. 9 New current source  $I_F$  simulating fault at bus 4.

Thus, after fault, the circuit is described by

$$\bar{E}'_{BUS} = \begin{bmatrix} E'_1 \\ \vdots \\ E'_j \\ \vdots \\ E'_n \end{bmatrix} = \begin{bmatrix} Z_{11} & \dots & Z_{1n} \\ \vdots & \ddots & \vdots \\ Z_{n1} & \dots & Z_{nn} \end{bmatrix} \begin{bmatrix} I_1 \\ \vdots \\ I_j - I_F \\ \vdots \\ I_n \end{bmatrix}$$

$$= \begin{bmatrix} 1.0 \\ \vdots \\ 1.0 \\ \vdots \\ 1.0 \end{bmatrix} - I_F \begin{bmatrix} Z_{1j} \\ \vdots \\ Z_{jj} \\ \vdots \\ Z_{nj} \end{bmatrix} \tag{67}$$

Equation (67) gives the bus voltages during fault at bus j.

Line currents with fault at bus j are obtained in the following manner.

- For a line connecting 2 buses -

For the "float" network in which all lines connecting buses and

ground (i.e. sources) are removed, the following stand. The subscript f denotes "float" network.

$$\bar{i}_f = (y_f) \bar{v}_f$$

$$(y_f) = (z_f)^{-1}$$

$$\bar{v}_f = A_f \bar{E}'_{BUS}$$

Thus line currents are

$$\bar{i}_f = (z_f)^{-1} A_f \bar{E}'_{BUS} \quad (68)$$

If a line has no mutual coupling,

$$i_{p,q} = \frac{E'_p - E'_q}{z_{p,q}} \quad (p \neq 0, q \neq 0) \quad (69)$$

- For a line connecting a bus p and ground -

In this case the line current is simply

$$i_{o,p} = \frac{1.0 - E'_p}{z_{o,p}} \quad (70)$$

where it has been taken into account that in physical system, a fault current source, e.g. generator, etc., has no mutual coupling with other network elements.

4. ANSI METHODS FOR FAULT CURRENT CALCULATION

4.1 ANSI C37.010-1972

This standard recommends methods of calculating fault current to be used mainly for the application of high voltage circuit breakers.

4.1.1 Interrupting Duty

The standard introduces several methods, only one of which is most general and will be described here.

The basic philosophy of the method, called "E/X Method Corrected for AC and DC Decrements", is to find E/X and apply a correction factor to it.

The value obtained thus is compared with the circuit breaker interrupting rating with proper consideration of system operation voltage.

E/X implies the voltage at the fault point before fault divided by the Thevenin reactance ignoring all network resistances.

Table 2 Impedance correction factors for machines

Fault Current		X and R to be used	I.C.F.		
			C37.010-1972		C37.13-1973
			Int. Duty	Mom. Duty	Int. Duty
All turbo-generators, all hydro-generators with amortisseur windings, and all condensers		$X'_d$ R	1.0	1.0	1.0
Hydro-generators without amortisseur windings		$X'_d$ R	0.75	0.75	1.0
All synchronous motors		$X'_d$ R	1.5	1.0	1.0
Induction Motors	Above 1000 HP at 1800 rpm, above 250 HP at 3600 rpm	$X'_d$ R	1.5	1.0	1.0
	All others, 50 HP and above	$X'_d$ R	3.0	1.2	1.0
	3-phase induction motors below 50 HP and all single-phase motors	$X'_d$ R	$\infty$	$\infty$	1.0
Non-rotating equipment		X R	1.0	1.0	1.0
Utility supply		X R	1.0	1.0	1.0

For the calculation of X, network reactance data should be prepared in accordance with Table 2. The factors appearing in the table may be called "Impedance Correction Factors (ICE)".

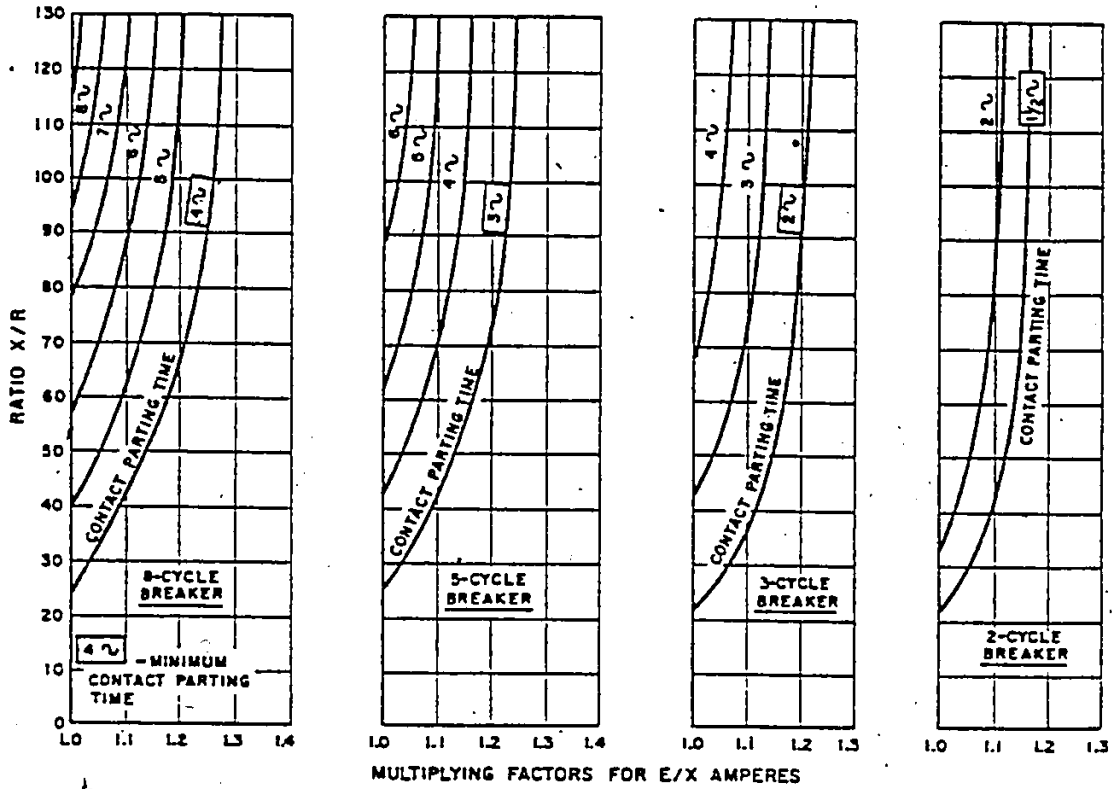


Fig. 10 Multiplying factors for three-phase faults fed predominantly from generators through not more than one transformation (From ANSI Standard C37.010-1972).

E/X is, in other words, the steady state component of fault current obtained assuming that machine reactances are constant at their corrected values.

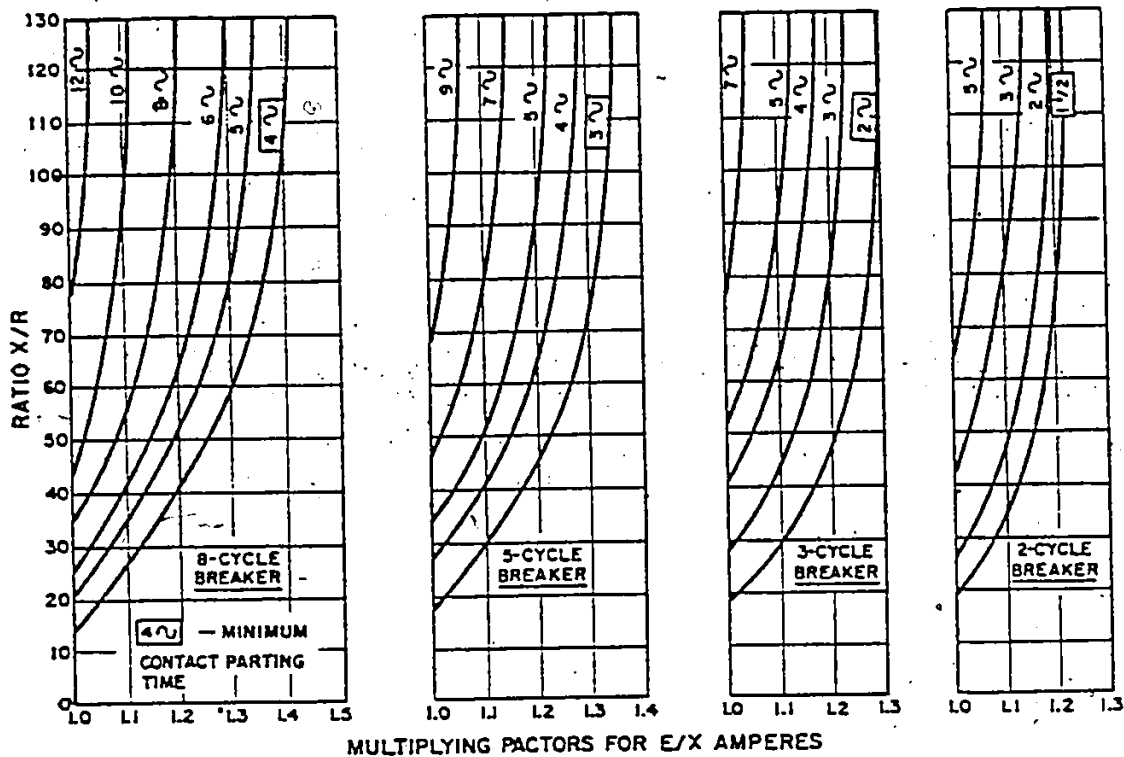


Fig. 11 Multiplying factors for line-to-ground faults fed predominantly from generators through not more than one transformation (From ANSI Standard C37.010-1972).

To take into account the DC and AC transient components of the fault current, a correction factor, "Current Correction Factor (CCF)", is applied to E/X.

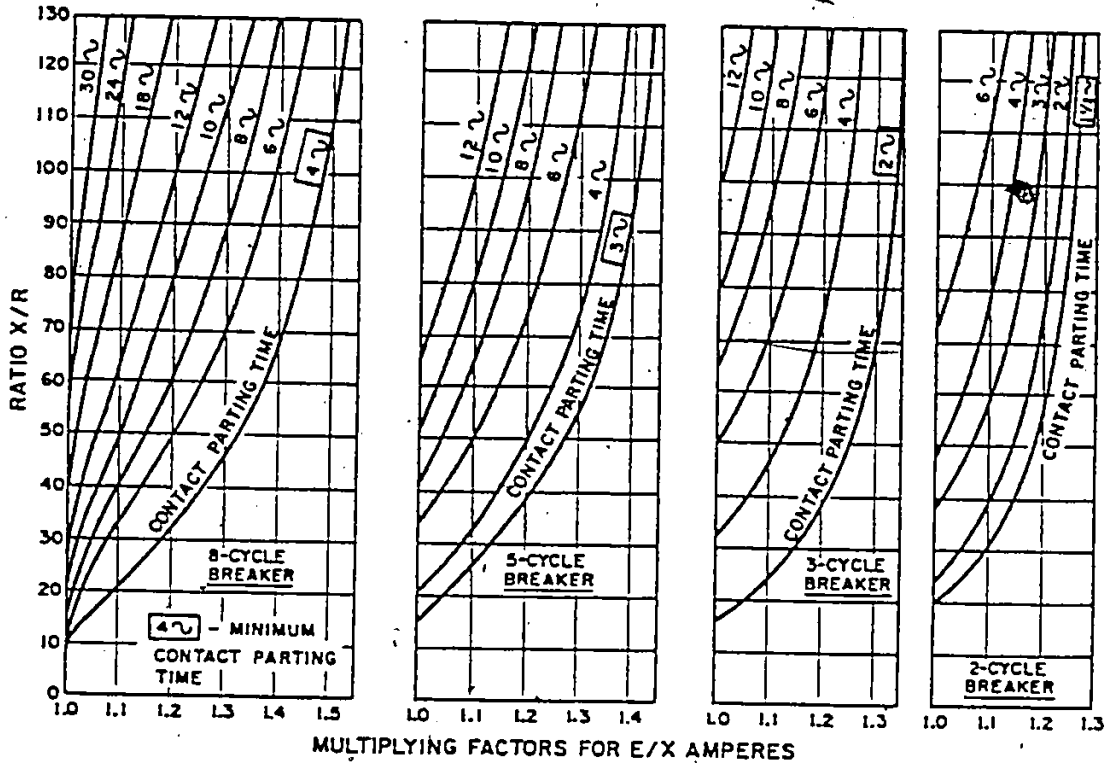


Fig. 12 Multiplying factors for three-phase and line-to-ground faults fed predominantly through two or more transformations (From ANSI C37.010-1972).

CCF depends on the rated interrupting time and contact parting time of the circuit breaker and on the X/R ratio of the network seen from the fault point. The R, which is necessary to find X/R, is also obtained with complete disregard for the reactances and with proper correction in accordance with Table 2, like X. Given these three pieces of information, CCF is obtained from Fig. 10, 11 and 12.\*

\* CCF = "Multiplying factors" of Fig. 10, 11 and 12

In utilizing Fig. 10, 11, and 12, there is a difficulty concerning number of transformations.

As noted from these curve titles, the Current Correction Factors are a function of the number of transformations the faulted bus is away from the generators. The standard does not define an impedance or transformer size to put a definite fix on what is considered an equivalent transformation. This procedure leaves doubt as to what to do in some cases. For example, why should a 20MVA transformer and a 1000kVA transformer each be considered a transformation, since the per unit impedances of each are greatly different? Can reactors or long lines be equivalent to a transformer, since the impedances may be of equal magnitude? How does one consider a bus with a generator on it and a generator two transformations away?

Those interpretations in Ref. 5 and 6 furnish answers to these questions. The answer is to measure the amount of fault current from the local generators and remote utility sources. The designated remote sources are always considered "remote", while local generators may have both a "local" and "remote" portion of fault current contribution depending on the fault location. As the fault location is removed away from the local generators terminals, the remote portion of the fault current increases. This interpretation provides a gradation between the "local" and "remote" extremes of AC decay provided in the standards. The local and remote portion of the fault current is determined from the expressions:

$$\begin{aligned} \text{Local portion} &= \frac{(\text{Contribution of the gen. to faulted bus})}{(\text{Contribution of the gen. if fault occurs at the gen. terminals})} \\ &\times (\text{Contribution of the gen. to faulted bus}) \\ \text{Remote portion} &= (\text{Contribution of the gen. to faulted bus}) \\ &- (\text{Local portion}) \end{aligned}$$



If there are more than one local generators, remote portion for each generator should be calculated. A measure as to the closeness the generators are to the fault bus is determined by a No. A.C. Decrement ratio.

$$\text{NACD ratio} = \frac{\text{Sum of remote portions}}{\text{Total gen. contribution to fault current}}$$

If the ratio is 0, Fig. 10 or 11 would be used, while Fig. 12 would be used if the ratio is equal to 1. Fig. 13 gives some of the interpreted values between Fig. 10 or 11, and 12.

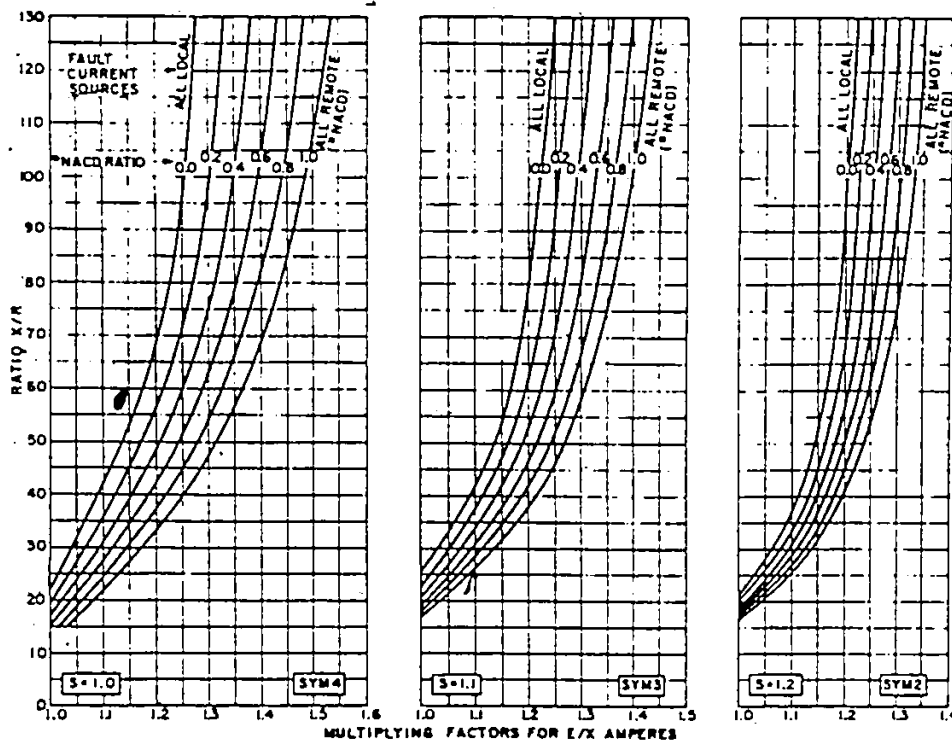


Fig. 13 Multiplying factors (symmetrical current rating basis) for three-phase faults fed from both local and remote generations. (5,6)

For 3-phase short circuit calculation, NACD ratio is determined by the above mentioned method. For 1L-G short circuit calculation, because of certain limitations of the program, exact value of NACD ratio is difficult to obtain. But as a good approximation, NACD ratio is obtained from the zero sequence network.

#### 4.1.2 Momentary Duty

Momentary duty to be obtained by calculation is  $E/X$  where  $X$  is Thevenin reactance reduced from the network with corrected machine reactances in accordance with Table 2.

$E/X$  obtained thus is compared with the momentary rating of circuit breaker with proper consideration of operating voltage of the system.

It is to be noted that the standard does not show which one of  $E/X$  and  $E/Z$  ( $Z$ : Thevenin impedance) should be used. To be more conservative, generally  $E/X$  is used.

#### 4.2 ANSI C37.13-1973

This standard includes certain guides for the calculation of low voltage circuit breaker interrupting duty. Note that for low voltage circuit breaker, interrupting duty and momentary duty are not distinguished.

The recommended method is first to obtain  $E/X$ , where  $X$  is Thevenin reactance neglecting resistance of the network and then to apply a correction factor to it. The value obtained thus is compared with the interrupting rating of the circuit breaker.

For a low voltage network,  $E/Z$ , where  $Z$  is the Thevenin impedance, is frequently used. However, to be more conservative,  $E/X$  is nevertheless

used especially when the network consists mainly of motors.

For the calculation of X, the network reactances are directly used without any correction as shown in Table 2.

The correction factor applied to E/X, say "Current Correction Factor (CCF)", is employed to take into account the effect of system resistances on the fault current. CCF depends on system X/R. But X/R is not as clearly defined in the standard as in C37.010-1972. Thus, in this report the same definition is used. With X/R given, CCF is obtained from Table 3.

Table 3 Current correction factors:  
from ANSI C37.13-1973

X/R ratio	C.C.F.
6.6 or smaller	1.00
8.27	1.04
9.95	1.07
11.72	1.09
14.25	1.11
20.0 or bigger	1.15

5. COMPUTER PROGRAM - SHTCCT

The computer program (App. B) can be used primarily for the calculation of 3-phase short circuit current (also 1 line-to-ground short circuit current with some limitations) based on the recommendations of two ANSI standards, C37.010-1972 and C37.13-1973.

The method used is a driving point and transfer impedance matrix approach. In the program two separate matrices,  $R_{BUS}$  and  $X_{BUS}$ , are constructed instead of having one  $Z_{BUS}$  to go by ANSI recommendations.

To form  $R_{BUS}$  and  $X_{BUS}$  the direct method described in section 2-2 is used. Since these matrices are symmetrical, only the lower half is stored for each of them to reduce storage requirement.

Based on these matrices, circuit values are calculated by the simple manipulations described in Chapter 3.

To give flexibility to the program, abundant options have been incorporated. For details of these flexibilities, User Manual (App. A) can be referred to.

To take into account the Current Correction Factors for H.V. circuit breakers, almost all of the related curves given in Figs. 10, 11, and 12 have been fitted into sixth order polynomials by least square fitting and put in a subroutine.

Also for C.C.F. of L.V. circuit breaker, Table 3 is fitted into a group of formulae which will give C.C.F. by linear interpolation.

To demonstrate the validity and efficiency in application of the program, studies of several sample systems are included in App. C.

6. CONCLUSION

The methods of calculating short circuit duties are not new features. One of them has been simply reviewed in Chapter 2 of this report.

A newly defined "float" network element-bus incidence matrix  $A_f$  has been introduced (Eq. 4) and one of its convenient applications has been demonstrated (Eq. 68).

A computer program has been developed using part of this method for practical applications in line with current ANSI standards.

What is important in developing a program for digital computers to calculate short circuit currents are:

- how to manipulate the system
- how to apply the theory
- what to calculate
- how to consider standard recommendations

to achieve the purpose of minimum cost and maximum benefits, and it can be said that with this program much of the purpose has been achieved.

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APPENDIX A

USER MANUAL

FOR PROGRAM

SHTCCT

MACHINE CDC 172

COMPILER FTN

LANGUAGE FORTRAN IV

1. SINGLE LINE DIAGRAM

Draw a single line diagram showing all quantities in per unit on a common base. Then number the buses using only the numbers between 1 and 99. Even when more than 2 independent networks are to be analyzed by one running, no number can be used multiple times throughout the whole network.

For 3 phase short circuit study, one single line diagram, which represents the positive sequence network of the system, is enough.

For 1-line-to-ground short circuit study, a zero sequence single line diagram is also needed in addition to the positive sequence single line diagram. In the program it has been assumed that positive sequence network is identical to negative sequence network except in the latter there is no source.

An important note is that 1 L-G study should always be preceded by 3 phase study since some values obtained in 3 phase study are used for the following 1 L-G study. In this case the "Case Connection Card" (explained later) between card deck for 3 phase study and that for 1 L-G study should read 2, which is same code as that for "NEW CASE". The same bus numbers should be used for both 3 phase and 1 L-G study.

In zero sequence network there will be usually several subnetworks which are independent from each other. Subnetworks which do not contain a line connecting a real bus and the ground should be completely removed. The program is written such that a subnetwork which is not connected to the ground results in an error message:

•.EACH SUBNETWORK SHOULD CONTAIN ZERO-BUS"

and computation is terminated.



## 2. INPUT DATA CARDS

### 2.1 Case Bundles

Input data card deck consists of several case bundles. There are six card groups and a flag card, called "CASE CONNECTION CARD", in each case bundle.

There is no limitation on the number of case bundles.

The general structure of data deck is shown in Table A1.

#### Comments on Case-Connection Card

On this card 1, 2 or 0 (or blank) should be put in the first column.

1...A change case based on the present case follows.

2...A new case on 1 L-G study case follows.

0...No more case.

#### Comments on Change Case and New Case

When the next case is a new case, all information given so far is discarded.

When the next case is a change case, all the network topology which has been given cumulatively to the computer so far is retained. But other information than that is completely discarded.

When the next case is 1 L-G study case, all information given so far is discarded like a new case except Thevenin X and R obtained from the present case for all network buses.

For change cases, addition of lines and buses is accomplished simply by putting them in the 6th card group of the next case bundle.

Table A1 Structure of input card deck

Case bundle	Group	Identification
1st case bundle	1st group	"Job name"
	2nd group	"Base MVA, etc"
	3rd group	"Bus in question"
	4th group	"Remote monitoring"
	5th group	"Bus voltages"
	6th group	"Impedances"
	case connection card	"Case connection"
2nd case bundle	⋮	⋮
⋮	⋮	⋮

To remove existing lines, the negative of R and X of existing lines should be put in the 6th card group of the next case bundle. When there is more than one line connecting two buses, same number of negative line information should be given one by one to remove all of the existing lines. Removal of a bus is achieved by eliminating all lines incident to the bus.

2.2 Groups

Each case bundle consists of six card groups and one connection card. The six groups will be explained below one by one.

1st Group

- Job name and Description
- Only one card

This card contains any information which the user may want to show on the printout to identify project.

Use 1-40th columns for job name and 51-80th column for additional information.

(Example)

Input

1 .....	41...
EXAMPLE...G.W. STAGG	NONE

Output

JOB NAME = EXAMPLE...G.W. STAGG

DESCRIPTION = NONE

2nd Group

- Base MVA, Fault type, Option code for  $R_{BUS}$  and  $X_{BUS}$  matrices printing.

- Only one card

Put the base MVA at any place in the first 10 columns with decimal point, the code 3 or 1 in the 11th column for type of fault, and the code 0 or 1 in the 12th column for option for  $R_{BUS}$  and  $X_{BUS}$  matrices printing.

(Example)

1	2	3	4	5	6	7	8	9	10	11	12	
		2	5	0						3	1	
A						B		C				

A : Base MVA

B : Type of fault

3 = 3 phase short circuit

1 = 1 L-G short circuit

C : Option

0 - Don't print matrices

1 - Print them

3rd Group

- Buses in question,

Duty classifications to be considered.

- As many cards as needed

This group should be one of the following two configurations.

(1) Only one card showing 111 in its first three columns.

Put this card when duty calculations for all buses are required. The card should be

1	2	3	...
1	1	1	

When this card is put, duty calculations are done, as follows, for all buses.

L.V. Bus = Int. duty

H.V. Bus = Mom. duty

Int. duty for the breakers:

2 cycle Int. time 1.5 cycle parting time

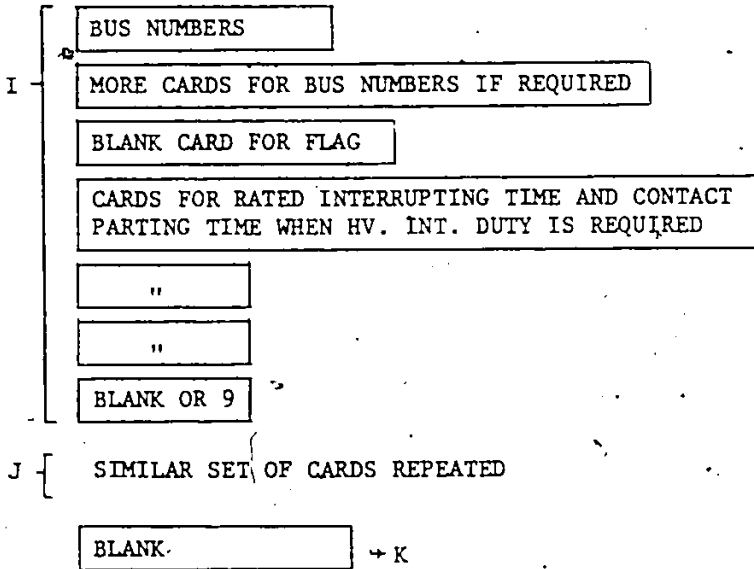
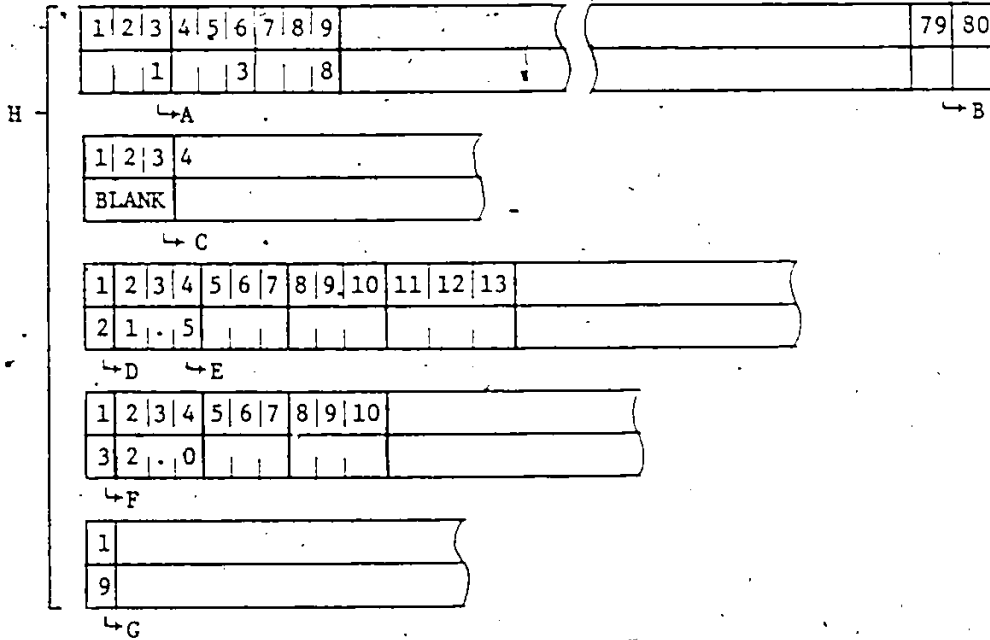
3 cycle Int. time 2.0 cycle parting time

5 cycle Int. time 3.0 cycle parting time

8 cycle Int. time 4.0 cycle parting time

(2) As many cards as required to specify the bus numbers and breakers rated interrupting time and contact parting time, etc., as illustrated below by examples.

(Example 1)



Explanation

A : Put bus numbers carefully.

Each bus number occupies 3 columns.

Note the difference between

1	2	3
		1

and

1	2	3
	1	

. The former is 1 while the latter is 10.

One card may contain 26 bus numbers.

Note that the biggest bus number possible is 99.

If a card contains zero, like:

	13	14	15	

Blanks or zeros

then the zero is ignored but the subsequent information is respected.

For example, with a card like

...	13	14	15	16	17	18	19	20	21	22	23	24	...
		0				4			1	9			

bus numbers 4 and 19 are respected.

B : Any information in 79 and 80th columns is ignored.

C : This is a flag to end cards for bus numbers.

D : Rated interrupting time should be put in the first column, if required.

E : Contact parting times, corresponding to the rated interrupting time put in the first column, should be put in three columns.

If one more contact parting time is to be examined it can be put in the next three columns.

Contact parting time must be REAL number (i.e. it must include decimal point).

F : If another rated interrupting time is to be examined, use another card and put the rated interrupting time in the first column and the corresponding contact parting times in the subsequent blocks of three columns.

G : This is a flag to end the first "subgroup".

This flag should be either 9 or zero.

9 : first cycle duty required

0 (or blank) : first cycle duty - not required

H : This is the first "subgroup" of the 3rd Card Group.

For this particular example, duty calculations will be done as follows:

For bus 1 (assume this bus is H.V.)

- Interrupting duty calculation

: for 2 cycle R. I. time, 1.5 cycle C.P. time

: for 3 cycle R. I. time, 2.0 cycle C.P. time

\*See note on the next page.

- Momentary duty (first cycle duty) calculation will be done.

For buses 3 and 8 (assume these are L.V.)

- Interrupting duty (first cycle duty) calculation will be done.

I : Put another "subgroup" if wanted.

If buses included in this subgroup are all L.V. buses, cards for R.I. time and C.P. time are not required.

J : Put another subgroup if wanted.

K : This is flag to end the 3rd Card Group.

The number of "subgroups" in this 3rd Card Group is unlimited.



\*NOTE

- (1) The maximum number of cases for H.V. Int. duty calculation per "subgroup" cannot exceed 7.

e.g.

1	3	8
0		
2	1.5	2.0
3	2.0	3.0 4.0
5	3.0	
8	4.0	5.0
9		

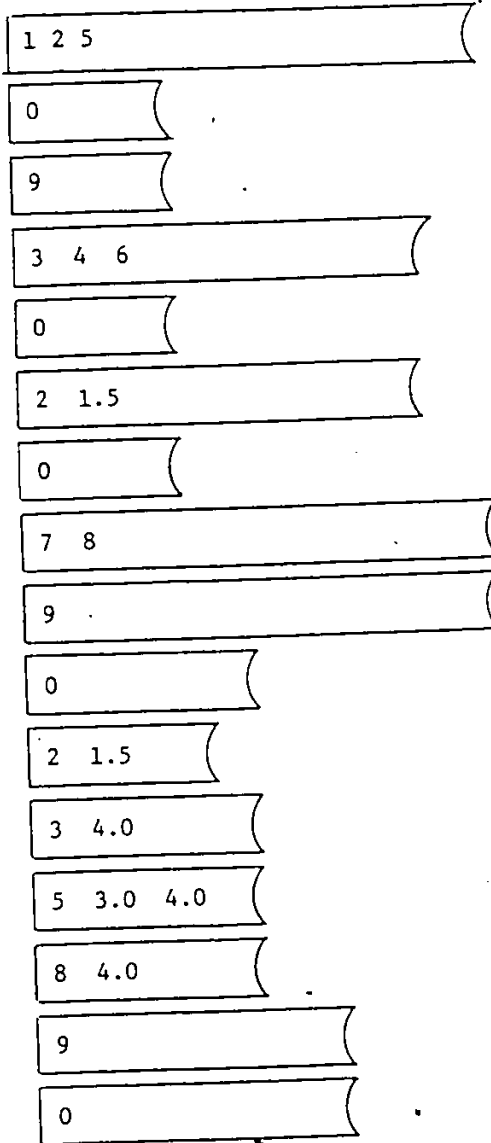
The above is invalid because 8 cases are requested. Actually this makes a big error. No diagnosis is provided.

- (2) Permitted combinations are as follows:

R.I. Time	C.P. Time
2	1.5 , 2.0
3	2.0 , 3.0 , 4.0
5	3.0 , 4.0 , 5.0 , 6.0
8	4.0 , 5.0 , 6.0 , 7.0 , 8.0

Thus, for example, request for "2 cycle R.I. time and 3.0 cycle C.P. Time" duty calculation is invalid. Error message is provided.

(Example 2)



Explanation will not be given for this additional example.

4th Group

- Remote monitoring
- As many cards as required

By giving the identifications of lines, the current through the lines and the bus voltages at both ends of the lines can be obtained corresponding to a particular faulted bus.

(Example)

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	
2	5		1	6		1	5		2	7		2	8		
A	B <sub>1</sub>		B <sub>2</sub>		C <sub>1</sub>			C <sub>2</sub>		D					
	B				C					D					

E

	18		19		31		35

F

1	2	3	4	5	6	7	8	9	10	11	12	
2	6											

G


Explanation

A : Faulted Bus number.

B : Line identification

B<sub>1</sub> : From-bus

B<sub>2</sub> : To-bus

C, D : same as B

\*If there is more than one line between bus  $B_1$  and  $B_2$ , current through each individual line is printed.

\*If the whole card is empty except the columns for faulted bus (position A), then monitoring for all lines is performed for that faulted bus.

E : If one more card is needed to accommodate all monitored line identifications corresponding to the faulted bus, the first three columns of the continuing card should be left empty and the rest of it can be used for bus pairs.

F : For monitoring corresponding to another faulted bus, another set of information similar to A-E should be given.

G : The 4th Card Group is terminated by this blank card.

\*If no remote monitoring is wanted, one blank card should be put in the 4th Card Group position.

\*The number of cases of "remote monitoring" should be compared with the value of MAXMON. (See DATA statement of the program SHTCCT).

If, e.g., the whole 4th Card Group is like this,

1 5	2 2	2 3	2 3	3 1	
1 8	2 0	2 2			
	3 2	2 0	2 2	2 5	
BLANK					

then the number of "remote monitoring cases" is 5.

And faulted buses appearing in this card group is 2.

Then MAXMON should not be smaller than 7 (=5 + 2).

5th Group

- Bus voltages
- As many cards as needed

For all buses listed in the 3rd card group ("BUS IN QUESTION") the bus voltages should be given.

Excess information is not used, i.e. any bus voltage specification for a bus which is not listed in "BUS IN QUESTION" is ignored.

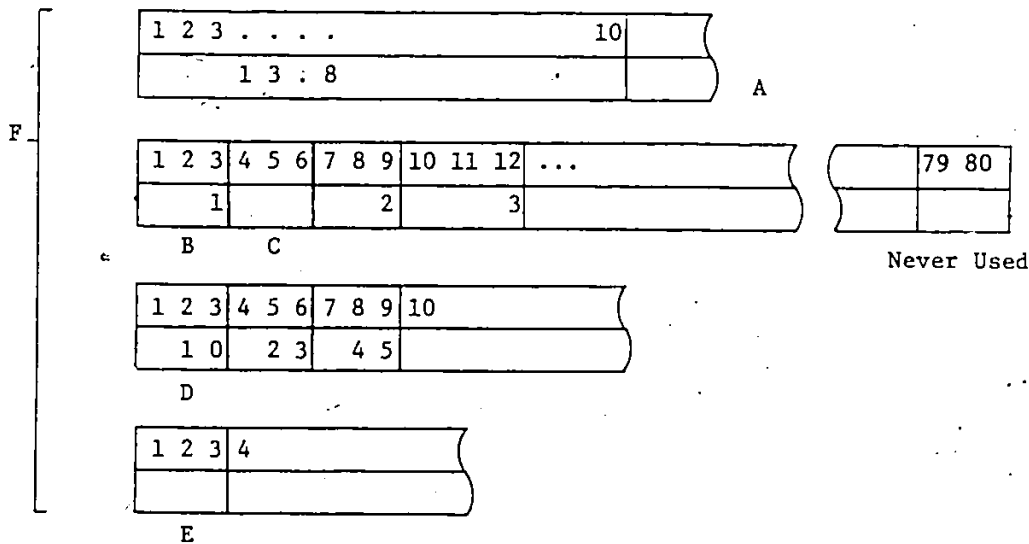
This group consists of as many subgroups as the number of voltage levels.

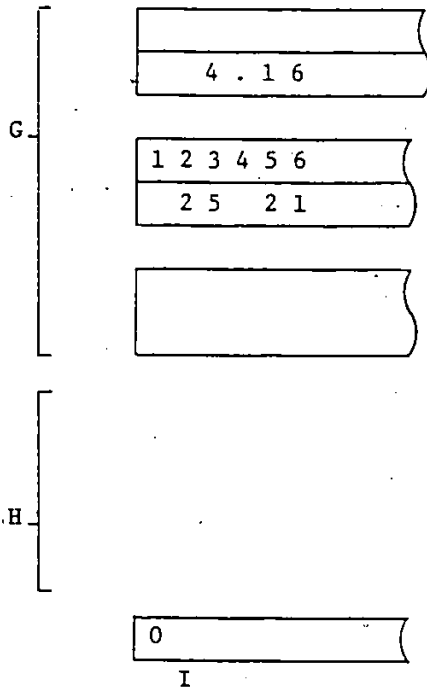
Each subgroup consists of one card for voltage (kV), as many cards as needed for the buses of that voltage level, and one card for flag.

This 5th Card Group should end with a flag which is blank or zero.

An example is given below.

(Example)





Explanation

A : Bus voltage should be put somewhere in the first 10 columns.

It must have decimal point.

B : One card can contain 26 buses. Each bus number occupies 3 columns.

The first 3 columns should contain nonzero bus number.

\*Note: the biggest bus number = 99.

C : Zero bus number is ignored but subsequent nonzero bus numbers are respected.

D : If one card is not enough to accommodate all the buses at this voltage level, use another or more cards as required.

E : This is flag to end the "subgroup" for this voltage (here, 13.8 kV).

F,G,H : Put as many subgroups as the number of voltage levels.

I : This card is flag to end the "BUS-VOLTAGES" section.

6th Group

- Bus pair, R and X, Identification
- As many cards as needed

This group contains network information. The two bus numbers at both ends of the line, line resistance and reactance, line identification code are contained in each card.

No special sequence is required for cards in this group.

If the branch identification codes are properly put in, the consideration of "Impedance Correction Factor" and "Current Correction Factor" is automatically achieved by the program.

The "Impedance Correction Factor" and the identification (or classification) code is tabulized in Table A2.

This group must end with a flag which is a blank (or zero) card.

Table A2 Impedance Correction Factors and Line Identification Codes

\* I.C.F. has been stored in the program.

Iden. Code	Low Voltage Int. Duty (=First Cycle)	High Voltage Int. Duty	High Voltage Mom. Duty (=First Cycle)
1	1.0	1.0	1.0
2	1.0	0.75	0.75
3	1.0	1.5	1.0
4	1.0	1.5	1.0
5	1.0	3.0	1.2
6	1.0	(=100000.0)	(=100000.0)
7	1.0	1.0	1.0
8	1.0	1.0	1.0

Iden. Code

- 1 - - - All turbo-generators, all hydro generators with amortisseur windings, and all condensers.  
Put  $X_d''$  on data card.
- 2 - - - Hydro-generators without amortisseur windings.  
Put  $X_d'$  on data card.
- 3 - - - All synchronous motors  
Put  $X_d''$  on data card.
- 4 - - - Induction motors above 1000 HP at 1800 r/min, above 250HP at 3600 r/min.  
Put  $X_d''$  on data card.
- 5 - - - Induction motors other than the above but equal or greater than 50 HP.  
Put  $X_d''$  on data card.
- 6 - - - Induction motors less than 50 HP  
Put  $X_d''$  on data card.
- 7 - - - Non-rotating equipment (Cable, reactor, transformer, etc.)  
Put X on data card.
- 8 - - - Utility System, Outside Source, etc.  
Put X on data card



Information should be put in the following manner.

1 2	3 4	5 . . . . 14	15 . . . . 24	25	
A	B	C	D	E	

Explanation

A : Bus number

B : Bus number

\* Note

1 2		=	1 2	
3			3 0	

C : Resistance R

Decimal point must always appear and can be put anywhere in the range.

If an R is zero, all resistances are ignored. And for L.V. duty calculations, two results will be shown:

(1) E/X

(2) E/X multiplied by 1.15 as per ANSI C37.13-1973, 9.1.4.3.

If R is zero and H.V. interrupting duty calculation is required, program stops with an error message.

D : Reactance X

Decimal point must always appear and can be put anywhere in the range.

X cannot be zero.

If an X is zero, program stops with an error message.

E : Line identification code

One of eight identification codes defined in Table A1 should be put here.

If it is left empty, that line is assumed to be a non-rotating equipment (Iden. Code = 7).

\* Comment on R and X

R and X can be negative only when a previously existing line is to be eliminated.

It is important that the absolute values of these negative R and X be exactly equal to those of the line to be eliminated. Otherwise program will stop with an error message.

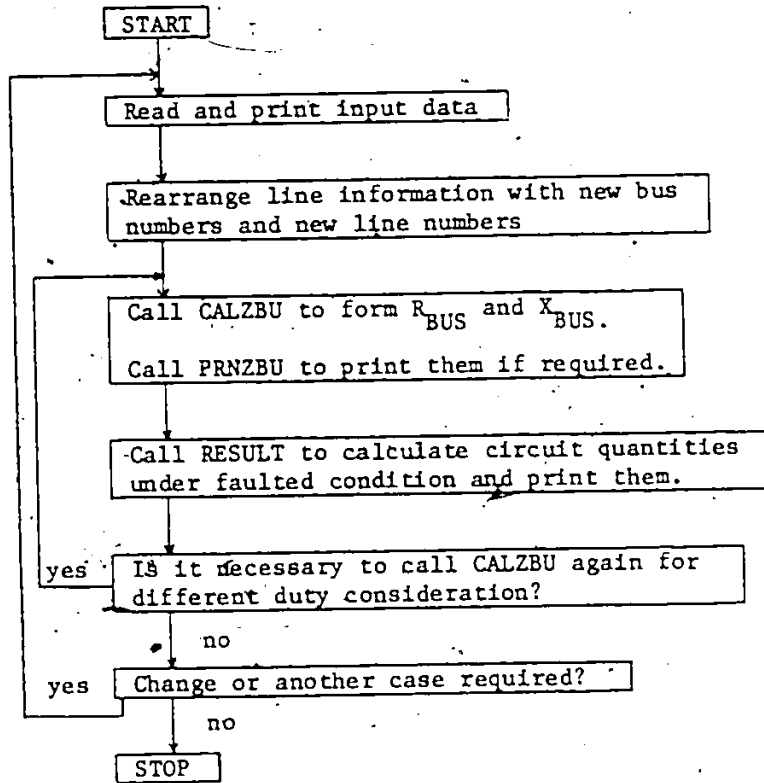
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APPENDIX B

COMPUTER PROGRAMS

1.

FLOW CHART FOR PROGRAM SHCCT



## 2. USAGE OF IMPORTANT VARIABLES

### 2.1 Single variables

The following integers should be defined in DATA statement in SHTCCT.

N9 : Should not be smaller than the maximum number of network buses.

Cannot be bigger than 99.

N30 : Should not be smaller than the total number of network lines.

Cannot be bigger than 999.

N495 : Should not be smaller than  $N9*(N9+1)/2$

N10 :  $N10 = N9+1$

MAXMON : Should not be smaller than the number of remote monitoring cases plus the number of faulted buses appearing in 4th card group in any one case bundle.

### 2.2 Arrays

ENQUIR(---): Dimension should not be smaller than N9.

If ENQUIR(5) = 99920399152., the duty calculation for bus 5 is done in the following manner.

9	99	20	3	99	15	2
A	B	C	D	E	F	G

(1) If bus 5 is H.V.

- G,F --- Do interrupting duty calculation for 2 cycle rated interrupting time and 1.5 cycle contact parting time.
  - E --- Partition
  - D,C --- Do interrupting duty calculation for 3 cycle rated interrupting time and 2.0 cycle contact parting time.
  - B --- Partition
  - A --- Do momentary duty calculation
- \* If A is 0, mom. duty calculation is not done.

(2) If bus 5 is L.V.

- B, - G --- All ignored
  - A --- Do int. duty calculation for bus 5.
- \* If A is 0, no duty calculation is done.

MONTOR(--): Dimension should not be smaller than MAXMON.  
Information related to remote monitoring is stored here.

IOLNWB(--) : Dimension should not be smaller than N9.  
If IOLNWB(5) = 9, 5 is user-given bus number while 9 is program-given bus number.

INCDEN(--): Dimension should not be smaller than N30.  
If INCDEN(5) = 72031008, the 5th line  
information for a given case corresponds to  
the line connecting buses 20 and 31, the  
iden. code is 7, and program given rank is  
008 after new arrangement.

VOLBUS(--): Dimension should not be smaller than N9.  
This is bus voltage.

ROLBRN(--), XOLBRN(--): Dimension should not be smaller  
than N30.

These are line R and X.

RBUS(--), XBUS(--): Dimensions should not be smaller  
than N495.

These are  $R_{BUS}$  and  $X_{BUS}$ .

AUXRBU(--), AUXXBU(--): Dimension should not be smaller  
than N10.

These are used to form  $R_{BUS}$  and  $X_{BUS}$ .

---

3. PROGRAM LISTING







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```

- /IH *DATA CARD SHOULD BE EITHER 3 OR 1*
STOP
35 READ(5,40) (INBUS(1),1,1,26)
40 FORMAT(26I3)
180 IF (INBUS(1)) 111145,180,45
ALLBUS=1
WRITE(6,184)
186 FORMAT(1H *FOR ALL BUSES OF HIGH VOLTAGE CHECKS FOR*
- /IH *2-1.6,3-2.0,5-3.0,8-4.0 BREAKERS INT.*
*DUITY AND CHECKS FOR /IH *FIRST CYCLE DUTY*
*WILL BE DONE.*/IH *FOR ALL BUSES OF LOW
*VOLTAGE, CHECKS FOR FIRST CYCLE DUTY WILL BE DONE.*)
70 GO TO 190
45 ALLBUS=1
WRITE(6,46)
46 FORMAT(///) *DUTY CALCULATIONS TO BE DONE BY THIS STUDY ARE...*
- /IH *(IF H.V. INT. DUTY CAL. IS REQUIRED,*
- /IH *RATED INT. TIME AND CONT. PARTING TIME IN CYCLES*
- /IH *OF THE C.B. TO BE CHECKED ARE AS SHOWN.1*)
50 IF (INBUS(1)) 55,191,55
WRITE(6,51)
51 FORMAT(1H *ERROR IN INPUT...* *THE FIRST BUS IN*
*QUESTION CAN NOT BE ZERO.*)
STOP
55 PRINT 1955
1055 FORMAT(1H //21H...*AT BUSES*)
LIM=0
DO 49 11=1,26
1CHECK=INBUS(11)/100
IF (1CHECK) 70,65,70
WRITE(6,71) INBUS(11)
70 FORMAT(1H *ERROR IN INPUT...* *CHECK BUS IN QUESTION.*
71 *BUS NUMBER CAN NOT BE...*)
STOP
65 IF (INBUS(1)) 167,80,67
67 LIM=LIM+1
95 NORMAL(LIM)=INBUS(11)
CONTINUE
85 READ(5,86) (INBUS(1),1,1,26)
86 FORMAT(26I3)
100 IF (INBUS(1)) 90,120,90
DO 105 12=1,26
105 1CHECK=INBUS(12)/100
IF (1CHECK) 100,93,100
WRITE(6,94) INBUS(12)
93 STOP
94 IF (INBUS(12)) 94,105,94
LIM=LIM+1
NORMAL(LIM)=INBUS(12)
CONTINUE
105 CONTINUE
110 80 TO 85
120 1=1
NUMB=NUMB+LIM
119 IF (MOD(1,10)) 111,122,123,122
123 PRINT 1123,NORMAL(1)
1123 FORMAT(1H *14)

```

FOOR PRINT

-B10-

78705/06. 15.45.54

FM 4.6.666

PROGRAM SHECT 73/172 OPT=1

PAGE

```

115 GO TO 124
      IPLU=1.8
      PRINT 1122,(NORMAL(K),K=:IPLU)
      FORMAT(1H,4X,9(=,14))
      I=IPLU
120 I=1.1
      IF(I-LIMIT)119,119,125
122 IF(I-LIMIT)122,122,123
      IPLU=LIMIT
123 GO TO 124
125 IF(M=9.04
      IPOINT=0
127 READ(5,126)INTIM,(PTIM(I),I=1,10)
126 FORMAT(11,16F3.1)
      IF(INTIM)130,150,130
130 IF(INTIM-9)132,160,132
      DO 133 I=1,10
132 K=1
      IF(PTIM(I))133,131,133
133 CONTINUE
134 IF(INTIM-2)133,133
135 IF(INTIM-3)134,134
136 IF(INTIM-5)135,135
137 IF(INTIM-9)136,136
138 PRINT 19136,INTIM
19136 FORMAT(1H, *ERROR IN INPUT/IM,
      *-RATED INTIME SHOULD BE 2.115 OR 8.17
      *-IM, IT CAN NOT BE 0.13, 0.1)
      STOP
143 DO 28133 I=1,K
      IF(PTIM(I)-1.5)7133,28133
145 7133 IF(PTIM(I)-2.0)6133,28133
      28133 CONTINUE
      GO TO 99131
150 8134 DO 28134 I=1,K
      IF(PTIM(I)-2.0)7134,28134
155 7134 IF(PTIM(I)-3.0)6134,28134
      6134 IF(PTIM(I)-4.0)6133,28134
      28134 CONTINUE
      GO TO 99131
160 8135 DO 28135 I=1,K
      IF(PTIM(I)-3.0)7135,28135
165 7135 IF(PTIM(I)-4.0)6135,28135
      6135 IF(PTIM(I)-5.0)5135,28135
      5135 IF(PTIM(I)-6.0)6132,28135
      28135 CONTINUE
      GO TO 99131
170 8136 DO 28136 I=1,K
      IF(PTIM(I)-4.0)7136,28136
175 7136 IF(PTIM(I)-5.0)6136,28136
      6136 IF(PTIM(I)-6.0)5136,28136
      5136 IF(PTIM(I)-7.0)4136,28136
      4136 IF(PTIM(I)-8.0)6133,28136
      28136 CONTINUE
      GO TO 99131
180 6133 PRINT 16133,PTIM(I),INTIM
16133 FORMAT(1H, *ERROR IN INPUT:1:7

```

-IH, \* CONT.PART.TIME CAN NOT BE,F5.1, \*FOR INT.TIME=,13,\*,\*/  
-IH, \*CHECK \*BUS IN QUESTION,\*)

```

175 STOP
    99131 WRITE(6,13)INTM,(PIIM(1),1,K)
    134 FORMAT(1H,10X,INT.TIME=,13,*, PARTING TIME=,9(F3.1,*, *)
    135 ENFO=EMFO-INTM*10.00*IPOINT
        IPOINT=IPOINT*1
        DO 138 137,K
    138 137,K
    139 ENFO=EMFO*10.00*PIIM(1)*10.00*(2*(13-1)*IPOINT)
    140 IPOINT=IPOINT*2,K
        ENFO=EMFO*99.00*10.00*IPOINT
        IPOINT=IPOINT*2
        GO TO 127
    145 ENFO=EMFO*9.00*10.00*IPOINT
        WRITE(6,141)
    146 FORMAT(1H,10X,*FIRST CYCLE DUTY WANTED*)
        GO TO 152
    150 WRITE(6,131)
    151 FORMAT(1H,10X,*FIRST CYCLE DUTY NOT WANTED*)
    152 DO 155 14=1,LIM
        JE(ERQUIB,NORMAL(14))154,155
    154 PRINT,154,NORMAL(14)
    154 FORMAT(1H, *ERROR IN INPUT,*, BUS NUMBER=,13,
        *DUPLICATED, CHECK *BUS IN QUESTION*,*)
        STOP
    155 ENQUIR(NORMAL(14))=EMFO
        READ(5,40)(INBUS(1),1=1,26)
        IF(INBUS(1))55,190,55
    190 IF(NUMB-N0)2000,2000,9194
    9194 PRINT 19194
    19194 FORMAT(1H, *ERROR,*,M9 MUST NOT BE SMALLER THAN */
        -IH, *TOTAL NUMBER OF BUSSES LISTED IN *BUS IN QUESTION*,*)
        STOP
205 C
C
2000 PRINT 12000
12000 FORMAT(1H)///1H, *REMOTE MONITORING*/1H, *T5,
        *FAULTED BUS//MONITORED BRANCH(FROM BUS/TO BUS)*1
        MOND=9
        MOND=1
        MOND=1
2100 READ(5,2010)(NORMAL(MON),MON=1,25)
2010 FORMAT(25I3)
        DO 2120 JF=1,25
        IF(NORMAL(JF)-N9)2120,2120,2110
2110 PRINT 12110,NORMAL(JF)
12110 FORMAT(1H, *INPUT ERROR,*,CHECK*REMOTE MONITORING*/
        -IH, *BUS NUMBER=,10,*, IS BIGGER THAN N9*)
        STOP
220 CONTINUE
        IF(NORMAL(1))2017,2015
        IF(ENQUIR(NORMAL(1)))2018,2020
2017 IF(ENQUIR(NORMAL(1)))2018,2020
2020 IF(ALLBUS=1)2019,2018
2019 PRINT 12019,NORMAL(1)
12019 FORMAT(1H, *INPUT ERROR,*,*REMOTE MONITORING*,*/1H, *
        *BUS=,14,*,DOES NOT APPEAR IN *BUS IN QUESTION*,*)
        STOP
2018 NE=9

```

PROGRAM SHEET	137172 OPT=1	FIN 8.6.886	78705706. 15.45.54	PAGE 5
230	MONDO=1 MONTO (MONO)=NORMAL (1)= (1,1000) MONO=MONO.1			
235	2200 DO 2040 JMN=2,24,2 IF (NORMAL (JMN)=NORMAL (JMN+1)) 2050,2040 IF (NORMAL (JMN)=NORMAL (JMN+1)) 2170,2060 2060 PRINT 12060,NORMAL (JMN),NORMAL (JMN+1) 12060 FORMAT (1H,*,INPUT ERROR...CHECK REMOTE MONITORING.../ -IH,*,MONITORED BRANCH SHOULD CONNECT TO DIFFERENT BUSES.../ -IH,*,CHECK FROM BUS,*,14,* TO BUS,*,14) STOP			
240	2170 MFB=1 MONTO (MONO)=NORMAL (JMN)=1000,NORMAL (JMN+1) MONO=MONO.1			
245	2040 CONTINUE IF (MFB) 2100,2030 2030 MONTO (MONO)=0 MONO=MONO.1 GO TO 2100			
250	2015 ISUM=0 DO 2250 JADD=2,28 2250 ISUM=ISUM+NORMAL (JADD) 2210 IF (ISUM) 2200,2210 2220 IF (MONDO) 2300,2220 2220 PRINT 12220 12220 FORMAT (1H,*,5,*,NO REMOTE MONITORING*) GO TO 2300			
255	2300 MNP=1 MNP=0			
260	2350 MNP=0 MONTR=MONTO (MONO)=NORMAL (1)= (1,1000) MONFR=MONTO (MNP)=MONTR/1000 IF (MONFR) 2320,2400 2310 IF (MONTR) 2340,2330 2340 PRINT 12340,MONTR 12340 FORMAT (1H,*,15,*,13) MNP=MNP+1 FLAG=1 GO TO 2350			
265	2330 IF (FLAG) 112500,2360 2360 PRINT 12360 12360 FORMAT (1H,*,15,*,ALL BRANCHES*) FLAG=0 MNP=MNP+1 GO TO 2350			
270	2320 IF (FLAG) 112500,2360 2360 PRINT 12360 12360 FORMAT (1H,*,15,*,ALL BRANCHES*) FLAG=0 MNP=MNP+1 GO TO 2350			
275	2320 MNP=MNP+2 INBUS (MNP-1)=MONTR INBUS (MNP)=MONTR IF (MNP-1) 2380,2370 2370 PRINT 12370, (INBUS (K), K=1,10) 12370 FORMAT (1H,*,15,*,14,*,*) MNP=0			
280	2380 MNP=MNP+1 GO TO 2350 2400 IF (MNP) 2410,2310 2410 PRINT 12410, (INBUS (K), K=1,MNP)			

```

290 MNP=0
    GO TO 2310
    CONTINUE
2500 IF (TYPE=1) 2530,2510
2510 IF (MONDO) 2520,2530
2520 PRINT 12520
2520 FORMAT(1H, 'REMOTE MONITORING REQUEST',
-1H, 'IS IGNORED SINCE FAULT TYPE IS IL-0 S.C.').
MONDO=0
2530 CONTINUE
C
9193 WRITE(6,194)
194 FORMAT(1H, '//1H, 'BUS VOLTAGES')
NBUSCH=0
300 195 READ(5,196)VOLT
196 FORMAT(10,2)
IF (VOLT) 198,199,198
199 IF (NBUSCH=408) 215,220,220
19A WRITE(6,197)VOLT
197 FORMAT(1H, '10X, 'BUSES AT',F10.2,'KV')
NUMVOL=0
305 9200 NIREAD=0
200 READ(5,201)(INBUS(I),I=1,26)
201 FORMAT(26I3)
IF (INBUS(1)) 203,204,203
203 DO 208 ICOL=1,26
    ICHECK=INBUS(ICOL)/100
    IF (ICHECK) 203,206,6203
6203 PRINT 16203,INBUS(ICOL)
16203 FORMAT(1H, 'ERROR IN INPUT,.,./
-1H, 'CHECK "BUS VOLTAGES", BUS NUMBER CAN NOT BE',I3)
    STOP
204 IF (INBUS(ICOL)) 205,208,205
205 NUMVOL=NUMVOL+1
    NIREAD=NIREAD+1
    NORMAL(NIREAD)=INBUS(ICOL)
    IF (VOLBUS(INBUS(ICOL))) 6207,6205
6207 PRINT 16207,INBUS(ICOL)
16207 FORMAT(1H, 'ERROR IN INPUT,.,BUS NUMBER',I3,
-60PLICATED, CHECK "BUS VOLTAGES,.,')
    STOP
6205 VOLBUS(INBUS(ICOL))=VOLT
208 CONTINUE
    GO TO 200
320 204 I=1
9210 IF (MOD(I,10) /= 1) 9212,9213,9212
9213 PRINT 19213,NORMAL(I)
19213 FORMAT(1H, '20X,I2)
    GO TO 9214
335 9212 IF (I=8-NIREAD) 9215,9216,9216
9216 I=I+NIREAD
    GO TO 9217
9215 I=I+8
9217 PRINT 19208,(NORMAL(K), K=I,IPLU)
19208 FORMAT(1H, '22X,9(.,.,I2))
I=IPLU
340 9214 I=I+1

```

PROGRAM 'SRICCT' 13/17Z OPT=1

```

335 IF(I-NIREAD)19210,9210,210
    WRITE(6,211)NUMVOL
    FORMAT(1H,20X,'AT LEAST',13,'BUSES AT THIS VOLTAGE',1)
    211 NBUCHK=NBUCHK+NUMVOL
        GO TO 195
350 WRITE(6,216)
    216 FORMAT(1H,'ERROR IN DATA CARD...TOTAL NUMBER OF BUSES=',
        -1H,'LISTED IN "BUS IN QUESTION" ',
        -1H,'CAN NOT BE BIGGER/1H
        -1H,' THAN THAT OF BUSES GIVEN IN "BUS VOLTAGES"SECTION.').
        STOP
355 220 CONTINUE
        J=13K=1
        4227 IF(K-NUMB)4223,4223,4226
        4223 IF(ENQUIR(J))4220,4221
        4221 J=J+1
        4220 IF(J-100)4223,4228,4228
        14228 PRINT 14228
        4220 STOP
        4220 IF(VOLBUS(J))4223,4225
        4224 K=K+13J=J+1
        4225 GO TO 4227
        14225 PRINT 14225,J
        14225 FORMAT(1H,'ERROR IN INPUT: ',
        -1H,'BUS VOLTAGE FOR BUS',13,' SHOULD BE GIVEN.').
        STOP
370 C
        4226 CONTINUE
        C DETERMINATION OF JLV,JHT,JHF
        C IF(ALLBUS-1)270,252,270
        252 DO 258 I=1,MAXBUS
        375 IF(VOLBUS(I))250,258,253
        253 IF(VOLBUS(I)-1.0)254,256,256
        254 JLV=I
        256 JHT=I
        380 JHF=I
        257 IF(JLV:JHT:JHF=3)258,269,289
        258 CONTINUE
        C
        270 DO 285 I=1,100
        270 IF(VOLBUS(I))270,285,270
        385 270 IF(ENQUIR(I))271,285,271
        271 ENFO=ENQUIR(I)
        271 IF(IKK-NUM)516280,6280,289
        6280 IKK=IKK+1
        280 K=1
        276 DENOM=10.0000K
        390 T1H=DHODI(ENFO,DENOM)
        IF(K-1)274,274,279
        274 IF(T1H)272,275,272
        272 IF(T1H-9.1273,273,273
        273 ENFO=(ENFO-T1H)/DENOM
        K=2
        GO TO 276
        ENFO=(ENFO-T1H)/DENOM
        279

```



PROGRAM SHEET 137172 OPT=1

```

400 IF (TIM) 286, 201, 286
    PRINT 1281
    1281 FORMAT(1H, 'INPUT ERROR...CHECK INITIATION AND PARTING TIME.')
```

```

405 CONTINUE
    IF (TIM-99) 1276, 280, 276
    IF (VOLBUS(1)-1.0) 205, 283, 283
    JNF=1
    283 IF (JLY-JHI) JNF=312851282, 282
    288 IF (VOLBUS(1)-1.0) 282, 284, 284
    277 JLV=1
    282 GO TO 288
    284 JNF=1
    284 GO TO 283
    285 CONTINUE
    289 CONTINUE
    C
    BRANCH IMPEDANCES
    PRINT 7227
    7227 FORMAT(1H, 'IDENTIFICATION CODE FOR BRANCH IMPEDANCES:///')
    -1H ** ID CODE1=A 1/8, H/8 WITH AMOR, WINDING, OR CONDENSER.*/
    -1H ** ID CODE2=AN H/8 WITHOUT AMOR, WINDING.*/
    -1H ** ID CODE3=A SYNCH. MOTOR.*/
    -1H ** ID CODE4=AN 1ND, MTR, ABV 1000HP AT 1800RPM, OR*/
    -1H ** ID CODE5=ABV 250HP AT 3600RPM.*/
    -1H ** ID CODE6=AN 1ND, MTR, 50HP AND ABV...NOT BIGGER THAN*/
    -1H ** ID CODE7=AN 1ND, MTR, 50HP OR 250HP AT 3600RPM.*/
    -1H ** ID CODE8=AN 1ND, MTR, SMALLER THAN 50HP.*/
    -1H ** ID CODE9=A STATIC ELEMENT...CABLE, BUSDUCT, TRF, RXTR, ETC.*/
    -1H ** ID CODE0=UTILITY SYSTEM, OFFSITE SOURCE, ETC.*/
    LINE=0
    WRITE(6, 221)
    221 FORMAT(1H, 'IMPEDANCES/1H, 5X, 9FROM BUS=120,
    *TO BUS=133, 99, 143, *X=150, *IDEN, CODE=1
```

```

435 IF (IFCHAN-2) 530, 500
    DO 510 K30=1, N30
    500 ROLBRN(K30)=XOLBRN(K30)=INCOEN(K30)=0
    CONTINUE
    510 GO TO 520
    530 IF (IFCHAN-1) 535, 223
    535 PRINT 1535
    1535 FORMAT(1H, 'INPUT ERROR...CHECK THE FLAG CARD FOR*/
    ** CHANGE OR NEW CASES.*/
    ** THE FIRST COLUMN OF THAT CARD SHOULD BE 0, 1, OR 2.')
```

```

445 STOP
    18RN=0
    520 MOOR=1
    READ(15, 224) IFROMB, ITOB, BRANR, BRANX, ICODMG
    223 FORMAT(2I2, 2F10.5, 11)
    224 IF (IFFROMB-1) 1081222, 250, 222
    222 IBRN=IBRN+1
    450 IF (IFFROMB(108) 8226, 8227
    8227 IF (ICODMG(1) 8229, 8228
    8229 IF (ICODMG-7) 8226, 8228
    8228 IF (ITYPE-1) 8230, 8226
    8230 PRINT 18228, IFROMB, ITOB
    18228 FORMAT(1H, 'INPUT ERROR...*/1H,

```





PROGRAM	SHTCCT	737172	OPT=1	PTN 3.85446	78705706. 1544554	PAGE 11
575	4238	STOP				
	C	CONTINUE				
	C	NEW BRANCH NUMBERS AND NEW BUS NUMBERS				
		NEWBRN=0				
		NEWBUS=0				
		LMBRN=0				
580	7300	1=0				
	7244	1=1				
		IF (MOD(INCDEM(I),1000))=7240,7242				
	7342	INTERM=INCDEM(I)/1000				
	7242	ITOB=MOD(INTERM,100)				
		INTERM=INTERM/100				
585		IFROM=MOD(INCDEM(I),100)				
		IF (ITOB=IFROM)7240,7241				
7244		PRINT 17244				
17244		FORMAT(IH,'ERR IN BRANCH IMPEDANCES...'/IH,				
		'-SOURCE BRANCH SHOULD CONTAIN ZERO BUS, '				
590		-IH,'-ALSO EACH SUBNETWORK SHOULD CONTAIN ZERO BUS.')				
		STOP				
7241		INCDEM(I)=INCDEM(I)+NEWBRN+1				
		NEWBRN=1+NEWBRN				
		NEWBUS=1+NEWBUS				
595		IF (IFROM=1)9241,9240,9241				
	9240	IOLNMB(I,TOB)=NEWBUS				
		GO TO 9247				
9241		IOLNMB(IFROM)=NEWBUS				
		INCDEM(I)=INCDEM(I)-((IFROM=100)*(TOB)=1000*((TOB=100)*(FROMB)=1000				
9247		CONTINUE				
600	00	9200 I=1,1BRN				
		IF (MOD(INCDEM(I),1000))=9200,9250,9200				
	9250	INTERM=INCDEM(I)/1000				
		ITOB=MOD(INTERM,100)				
		INTERM=INTERM/100				
		IFROM=MOD(INTERM,100)				
		IF (ITOB=1)9251,9259				
9250		IF (IOLNMB(IFROM)=1)9262,9200				
9250		INCDEM(I)=INCDEM(I)-((IFROM=100)*(TOB)=1000*((TOB=100)*(FROMB)=1000				
		GO TO 7277				
610	9251	IF (IOLNMB(ITOB)=1)9252,9253,9252				
	9253	IF (IFROM=1)9255,9200				
	9255	IF (IOLNMB(IFROM)=1)9256,9200,9256				
	9256	NEWBUS=NEWBUS+1				
		NEWBRN=NEWBRN+1				
		IOLNMB(ITOB)=NEWBUS				
		INCDEM(I)=NEWBRN+INCDEM(I)				
		GO TO 9200				
620	9252	IF (IFROM=1)9258,9200,9258				
	9250	IF (IOLNMB(IFROM)=1)9270,9264,9270				
	9284	NEWBUS=NEWBUS+1				
	9284	NEWBRN=NEWBRN+1				
		INCDEM(I)=INCDEM(I)-((IFROM=100)*(TOB)=1000*((TOB=100)*(FROMB)=1000				
		IOLNMB(IFROM)=NEWBUS				
		INCDEM(I)=NEWBRN+INCDEM(I)				
		GO TO 9200				
625	9200	GO TO 7272				

PROGRAM SHEETS	73/172 OPTC1	FIN 456446	78/05786. 15.06.34	PAGE 12
630	9276	IF (IOLNWB(IJOB) - IOLNWB(IFROMB)) / 7276.7272.7272		
	9276	INCDEN(I) = INCDEN(I) - (IFROMB(100.110B) * 1000. (IJOB * 100. IFROMB) * 1000		
	7273	M8188 = IOLNWB(IFROMB)		
		60 TO 7275		
	7272	M8188 = IOLNWB(IJOB)		
	7275	DO 7298 J=1,NEWBRN		
		K=NEWBRN-J		
		DO 7286 L=1,IBRN		
		LL=MOD(IINCDEN(L),1000)		
		IF LL		
		-K17288.7279.7280		
	7279	JOLBRN=L		
		60 TO 7282		
	7280	CONTINUE		
	7282	INTERM=INCDEN(JOLBRN)/1000		
		ITBCHK=MOD(INTERM,100)		
		MIBCHK=IOLNWB(ITBCHK)		
		IF (MIBCHK - M8188) / 7292.7292.7295		
	7295	INCDEN(JOLBRN) = K + INCDEN(JOLBRN) / 1000 * 1000		
	7296	CONTINUE		
	17290	FORMAT('H', 'SOMETHING WRONG NEAR STATEMENT LABEL 17290')		
		PRINT 17290		
		STOP		
	7292	INCDEN(I) = K + INCDEN(I)		
		NEWBRN = NEWBRN + 1		
		60 TO 9280		
	9280	CONTINUE		
	7307	LNBRN = NEWBRN		
		60 TO 9288		
	7308	PRINT 97308		
	97308	FORMAT('H', '97308...IN SHTCCT,')		
		STOP		
	7305	IF (NEWBRN - IBRN) / 7309.9281.9282		
	9282	PRINT 19282, NEWBRN, IBRN		
	19282	FORMAT('H', 'NEWBRN(=,14,0) CAN NOT BE BIGGER THAN IBRN(=,14,0)')		
		STOP		
	9281	MTTLRU = NEWBUS		
	C	DUTY CALCULATION		
		PRINT 1300		
	1300	FORMAT('H', 'H', 'SHORT CIRCUIT DUTIES=H', '-----		
		-1-----0)		
		IF (JULY - 11495, 400, 405		
	405	IF (JUN - 11415, 410, 415		
	415	JCDVIF=3		
		60 TO 402		
	400	JCDVIF=1		
		60 TO 402		
	410	JCDVIF=2		
	402	CONTINUE		
		CALL CALZNU1		
		(IBRN, INCDEN, IOLNWB, RBUS, XBUS, AUXRBU,		
		-BUS, JCDVIF, INTLBU, FACTOR, INCR, BULBRN, BULBRN,		
		-BUS, M9, M8, M3, M95, N10)		
		IF (IFZBU1422, 423		
	422	CALL PRNZMARRBUS, XBUS, INTLBU, JCDVIF, MOOR, M9, MAXBUS, IOLNWB)		
	423	CALL RESULTALLBUS, MAXBUS, IOLNWB, VOLBUS, RBUS, XBUS, JCDVIF,		
		-INCDEN, ITYPE,		
		-MONTOR, MAXMON, MONDO,		



SUBROUTINE	MGRP	73172	OPT=1	FTN 4.6446	78705706.13.45.34	PAGE
1						
5						
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SUBROUTINE MGRP (ICODMG)
1  IF (ICODMG-1) 1,19
2  IF (ICODMG-2) 2,19
3  IF (ICODMG-3) 3,19
4  IF (ICODMG-4) 4,19
5  IF (ICODMG-5) 5,19
6  IF (ICODMG-6) 6,19
7  IF (ICODMG-7) 7,19
8  IF (ICODMG-8) 8,19
9  IF (ICODMG-9) 9,19
10 WRITE (1,179)
11 FORMAT (1H,150,*,CODE ERROR AT THIS BRANCH,*)
12 STOP
13 RETURN
14 END

```

SUBROUTINE LOCATN 73717Z 0PT61 78/05/86. 15.45.34 P100 1

1 SUBROUTINE LOCATNIKROV,KCOL,(CTM)  
IF IKROV=KCOL,1,2,2  
KBIG=KCOL  
KSMALL=KROV  
GO TO 3  
KBIG=KROV  
KSMALL=KCOL  
LCN=KBIG+KBIG-11/2+KSMALL  
RETURN  
END





LINE	TEXT	PTN	PAGE
68	SUBROUTINE CALZBU 73/172 OPT=1	70705/06.15.45.55	2
50	IF (NTOB=KRCOL) 54,52,60		
52	LTYPE=3		
54	GO TO 399		
55	LTYPE=4		
60	CONTINUE		
65	PRINT 1960		
1060	FORMAT(1H, 'SOMETHING WRONG NE AR STAT LABEL 60 IN CALZBU')		
106	STOP		
108	KROW=KCOL+NTOB		
109	CALL LOCATN(KROW,KCOL,LC1N)		
110	XBUS(ILC1N)=BRANR*FACTOR(ICODMG,JCOVIF)		
111	RBUS(ILC1N)=PHOR*BRANR*FACTOR(ICODMG,JCOVIF)		
112	GO TO 588		
188	KRCOL=KRCOL+1		
189	DO 428 I=58,NTWK8,KRCOL		
190	KCOL=ITMS8		
191	IF (NFROM) 405,410		
192	KROW=NFROM		
193	CALL LOCATN(KROW,KCOL,LC1N)		
194	RPMROW=RBUS(ILC1N)		
195	RFMROW=XBUS(ILC1N)		
196	GO TO 415		
197	RPMROW=0.		
198	RFMROW=0.		
199	KROW=NTOB		
200	CALL LOCATN(KROW,KCOL,LC1N)		
201	RTOROW=RBUS(ILC1N)		
202	RTOROW=XBUS(ILC1N)		
203	AUXRBU(ITMS8)=RPMROW+RTOROW		
204	AUXRBU(ITMS8)=RFMROW+RTOROW		
205	CONTINUE		
206	IF (NFROM) 125,430		
207	KROW=NFROM		
208	KCOL=NFROM		
209	CALL LOCATN(KROW,KCOL,LC1N)		
210	RFMDGL=RBUS(ILC1N)		
211	RFMDGL=XBUS(ILC1N)		
212	GO TO 435		
213	RFMDGL=0.		
214	RFMDGL=0.		
215	KROW=NTOB		
216	KCOL=NTOB		
217	CALL LOCATN(KROW,KCOL,LC1N)		
218	RTODGL=RBUS(ILC1N)		
219	RTODGL=XBUS(ILC1N)		
220	IF (NFROM) 436,437		
221	KROW=NTOB		
222	KCOL=NFROM		
223	CALL LOCATN(KROW,KCOL,LC1N)		
224	RMUTUL=RBUS(ILC1N)		
225	RMUTUL=XBUS(ILC1N)		
226	GO TO 439		
227	RMUTUL=0.		
228	RMUTUL=0.		
229	AUXRBU(KRCOL+1)=RFMDGL+RTODGL+2*RMUTUL+ROR*BRANR*FACTOR		
230	-(ICODMG,JCOVIF)		

LINE	CODE	TEXT
115		AUXBU(KRACOL*1)=XFMOBL*XTODOL*2*XMUTUL*BRANK*FACTOR -(ICODMB,JCOVIF) DO 448 KRQ=NTKRB,KRMCOL
120	443	CALL LOCATN(KRQV,KCOL,LCIN)
	444	IF(MOOR)443,445
	445	RBUS(ILCTN)=RBUS(LCTN)-AUXBU(KRQV)*AUXBU(KCOL)/AUXBU(KRACOL*1)
	448	CONTINUE
125	300	DO 340 KCOL=NTKRB,LIMIT
		KRQV=NRQMB
		CALL LOCATN(KRQV,KCOL,LCIN)
		RFMRQV=RBUS(ILCTN)*RFMRQV*RBUS(LCTN)
130		KRQV=NTOR
		CALL LOCATN(KRQV,KCOL,LCIN)
		RBUS(ILCTN)=RFMRQV*RBUS(LCTN)+XFMRQV
		CONTINUE
135	340	CALL LOCATN(KRQV,KCOL,LCIN)
		RFMOBL=RBUS(ILCTN)*RFMOBL+RBUS(LCTN)
		KRQV=KCOL=NRQMB
		CALL LOCATN(KRQV,KCOL,LCIN)
		RBUS(ILCTN)=RFMOBL*NOOR*BRANK*FACTOR(ICODMB,JCOVIF)
140		RBUS(ILCTN)=XFMOBL*BRANK*FACTOR(ICODMB,JCOVIF)
		GO TO 500
145	500	RBUS(LCTN)=RFMOBL
	999	CONTINUE
		IF(KRACOL-NITLBU-1)1605,600
	605	PRINT 1605,KRACOL,NITLBU
	1605	FORMAT(1H,SOMETHING WRONG NEAR 605 IN CALZBU*)
		IN,KRACOL=1,1,5X,NITLBU=1,1,5X,KRMCOL=1,1
		--SHOULD BE EQUAL TO NITLBU.*
		STOP
150	600	CONTINUE
		NOOR=NRQLO
		RETURN
		END

SUBROUTINE CALZBU 73717Z 08Y-1 PTH 4.6446 78705706. 15.46.34 PAGE 3

SUBROUTINE	PARZBU	73/172 OPT=1	FIN 4.6.446	78/05/86. 15.45.54	PAGE
1					
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SUBROUTINE PARZBU(RBUS,IRBUS,MITLBU,ICOVIF,MOORI,NO,MRBUS,IOLNMB)
DIMENSION RBUS(19),XBUS(19),XBUS(19),IOLNMB(19)
PRINT 1000
FORMAT(1H) ,RBUS AND XBUS MATRICES FOR*
IF(ICOVIF=2) ,1,1,12
PRINT 1011
FORMAT(1H) ,L,Y, ,MI:DUITY STUDY*
GO TO 20
PRINT 1012
FORMAT(1H) ,H,V,NOM.(FIRST CYCLE) OUTY STUDY*
GO TO 20
PRINT 1013
FORMAT(1H) ,H,Y, ,MI:DUITY STUDY*
GO TO 20
IF(MOORI=50) 40
PRINT 1040
FORMAT(1H) //1H ,FOR RBUS MATRIX ,FOR THIS CASE, //1H ,
-ALL ELEMENTS ARE ZERO,*
MAX(CN=MITLBU*(MITLBU.1)/2
DO 45 ICHK=1,MAXLCL
IF(RBUS(ICHK)) 44,45
CONTINUE
GO TO 46
PRINT 1045
FORMAT(1H) ,SOMETHING WRONG,THE ABOVE STATEMENT IS INCORRECT.*
CONTINUE
LINE=7
PRINT 1050
PRINT 1052
FORMAT(1H) //1H ,RBUS AND XBUS MATRICES ... (BUS,BUS)*
LINE=5
DO 40 KRW=1,MRBUS
IF(IOLNMB(KRW)) 1053,60
DO 61 KCL=1,KRRW
IF(IOLNMB(KCL)) 1054,61
KRW=IOLNMB(KRW)
KCL=IOLNMB(KCL)
NPRNTO=NPRNTO+1
CALL LOCATN(KRW,KCL,LCTN)
PRINT 1055,KRW,KCL,RBUS(LCTN),KRW,KCL,XBUS(LCTN)
-13.,.13.,.F20.10)
LINE=LIME+1
IF(NPRNTO=MITLBU) 53,61,61
IF(LIME=45) 61,56,56
PRINT 1056
FORMAT(1H) ,RBUS AND XBUS MATRICES,...CONT'D*
LINE=1
CONTINUE
RETURN
END

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SUBROUTINE NAME	DATE	TIME	PAGE
1	7/7/72	OPT=1	78705706.15445.56
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SUBROUTINE HVMF (RNACD, XOV, ITYPE, CBITIM, CPTIM, RHVMF)
  DIMENSION IMPE(12)
  X=XOVR
  CPTIM=1
  DO 500 I=1,2
    IDCN=ITYPE+10+IRNCL
    IF (IDCN-12) I1=2, I1=1
    IF (IDCN-10) I1=1, I1=2
    IF (IDCN-11) I1=1, I1=2
    IF (IDCN-12) I1=1, I1=2
    IF (IDCN-13) I1=1, I1=2
    IF (IDCN-14) I1=1, I1=2
    IF (IDCN-15) I1=1, I1=2
    IF (IDCN-16) I1=1, I1=2
    IF (IDCN-17) I1=1, I1=2
    IF (IDCN-18) I1=1, I1=2
    IF (IDCN-19) I1=1, I1=2
    IF (IDCN-20) I1=1, I1=2
    IF (IDCN-21) I1=1, I1=2
    IF (IDCN-22) I1=1, I1=2
    IF (IDCN-23) I1=1, I1=2
    IF (IDCN-24) I1=1, I1=2
    IF (IDCN-25) I1=1, I1=2
    IF (IDCN-26) I1=1, I1=2
    IF (IDCN-27) I1=1, I1=2
    IF (IDCN-28) I1=1, I1=2
    IF (IDCN-29) I1=1, I1=2
    IF (IDCN-30) I1=1, I1=2
    IF (IDCN-31) I1=1, I1=2
    IF (IDCN-32) I1=1, I1=2
    IF (IDCN-33) I1=1, I1=2
    IF (IDCN-34) I1=1, I1=2
    IF (IDCN-35) I1=1, I1=2
    IF (IDCN-36) I1=1, I1=2
    IF (IDCN-37) I1=1, I1=2
    IF (IDCN-38) I1=1, I1=2
    IF (IDCN-39) I1=1, I1=2
    IF (IDCN-40) I1=1, I1=2
    IF (IDCN-41) I1=1, I1=2
    IF (IDCN-42) I1=1, I1=2
    IF (IDCN-43) I1=1, I1=2
    IF (IDCN-44) I1=1, I1=2
    IF (IDCN-45) I1=1, I1=2
    IF (IDCN-46) I1=1, I1=2
    IF (IDCN-47) I1=1, I1=2
    IF (IDCN-48) I1=1, I1=2
    IF (IDCN-49) I1=1, I1=2
    IF (IDCN-50) I1=1, I1=2
  
```

PRINT 4400  
 FORMAT(IH, ' INPUT ERROR.../IH '  
 --IF H.V.INT.DUTY REQUIRED, C.R. INT.TIME AND CONT.PARTY.TIME %/

POOR PRINT

-B28-

SUBROUTINE KUNF 777172 OPT=1 PIN 4.6.466 7/87/05/86. 15.45.55 PAGE 2

```

-IM *SHOULD BE GIVEN.*
STOP
1121 P1=.74997182073254099518
P2=.0180885642303773584
P3=.0003247469213282149
P4=.0000324667023680314
P5=.0000001495086261596
P6=.0000000003540022869
GO TO 499

1122 P1=.6488143323262523578
P2=.02182043786065190693
P3=.0004286129006366254
P4=.0000046917616794589
P5=.0000002632381266872
P6=.000000000581818021
GO TO 499

1123 P1=.76201473267869118099
P2=.0214724674034030071
P3=.0003682718277368935
P4=.000036278748764389
P5=.0000000001731315871
P6=.0000000004122847318
GO TO 499

1133 P1=.52941407023906200080
P2=.0274276578626977658
P3=.0005245960024251831
P4=.0000000001890000372
P5=.00000000011800095816
P6=.0000000006583265997
GO TO 499

1134 P1=.32311439274242942577
P2=.03277830162101158531
P3=.00058585117633764351
P4=.00000000009710520117
P5=.0000000005504915307
GO TO 499

1153 P1=.07316162742219916026
P2=.00583543725163163107
P3=.0001312095007507520
P4=.0000031086606926253
P5=.0000002332852774303
P6=.000000000576393927
GO TO 499

1154 P1=.66719188744730217877
P2=.0162801154278630199
P3=.00014495288970764501
P4=.00000057637094887258
P5=.00000000169222019358
P6=.0000000012514137
GO TO 499

1155 P1=.2284228304013282167
P2=.04314825576378060183
P3=.000810750683233244
P4=.000000970212252225664
P5=.00000005420703694613
P6=.0000000011966760365
GO TO 499

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FOOT PRINT

1156 P1=.2542284399267717979  
 P2=.6336296513247660833  
 P3=.00555051328097590183  
 P4=.00009145138870420478  
 P5=.00000001602402601866  
 P6=.00000000002149966137  
 GO TO 499

1164 P1=.8024602093439257257  
 P2=.007645305478952821  
 P3=.8885835350117318  
 P4=.00000180964479063385  
 P5=.00000001420260586807  
 GO TO 499

1185 P1=.95785163557439850550  
 P2=.00000000937573543  
 P3=.005800009681055208  
 P4=.009997164876915469  
 P5=.00000102110077036918  
 P6=.0000001121321750898  
 P8=.000000002205612669  
 GO TO 499

1186 P1=.29892531730963955203  
 P2=.84953142862355855660  
 P3=.00119460829000148684  
 P4=.0000151393591302157  
 P5=.000000947176801537  
 P6=.00000000223716197  
 GO TO 499

1187 P1=.87197078376624759244  
 P2=.001513407915608552  
 P3=.0003249919245624527  
 P4=.0000057386651549321  
 P5=.0000000027508154639  
 P6=.00000000010112803788  
 GO TO 499

1188 P1=.56784695443144528326  
 P2=.010384272286329839  
 P3=.0002054113687508256  
 P4=.888087184175035632  
 P5=.000000025301844556  
 P6=.000000001077647847  
 GO TO 499

3121 P1=.7097093087876106644  
 P2=.0198779571032122217  
 P3=.0003892687610941545  
 P4=.0000011267826709091  
 P5=.0000002260015633085  
 P6=.0000000005032655252  
 GO TO 499

3122 P1=.407826462342308099722  
 P2=.0215740611915097320  
 P3=.00072701087658772617  
 P4=.00000873249084654134  
 P5=.000000521260087677  
 P6=.0000000012151865937  
 GO TO 499

3132 P1=.3578452833780003985

FOOR PRINT

SUBROUTINE XVMF 73/172 DMTBI FTM 606466 78/05/06. 15:45:54 PAGE

```

P2=-.03221778263479979443
P3=-.0007238483148990339
P4=-.828888228755529282
P5=-.00000004971649767039
P6=-.0000000011451110954
GO TO 499
P1=.736347354275875431995
P2=.07766315154862590030
P3=-.00173957041181136840
P4=-.000200476275217948
P5=-.0000011546341646100
P6=-.000000026240549214
GO TO 499
P1=-5.6632995702054314671
P2=-3285628237631756211
P3=-.00644169487983012323
P4=-.0004282596809320725
P5=-.000003031775031538
P6=-.0000000057904625251
GO TO 499
P1=-.6321893834439618753
P2=-.0237996550425208671
P3=-.005077910055317084
P4=-.0000665684003228355
P5=-.0000000499852203173
P6=-.000000011531254742
GO TO 499
P1=-2.0720137450764573259
P2=-.0024640417175560158
P3=-.0022798321746071089
P4=-.0000283107356531633
P5=-.0000016538966358699
P6=-.000000003705089850
GO TO 499
P1=-1.6933027247380306918
P2=-.08924362275063461649
P3=-.00101309672522030063
P4=-.0002148263134311794
P5=-.0000012107074643669
P6=-.000000002642080092
GO TO 499
P1=-55.71193707240948179090
P2=-2.4786852402175932730
P3=-.04308349167241432021
P4=-.00037242154031755574
P5=-.00000159901152719503
P6=-.00000000272689572303
GO TO 499
P1=-95114945901132505959
P2=-.00190281368473351
P3=-.0001169034647973125
P4=-.0000049916222154440
P5=-.0000003211953450034
P6=-.0000000007605440135
GO TO 499
P1=-70417959452043632496
P2=-.0106629034540474179

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FOOR PRINT |

230 P3--.000045103397986524  
P4-.000000365722135781  
P5--.000000047683521066  
P6--.4288880137815302  
GO TO 499

235 3184 P1-.2955212018937195579  
P2-.030398225252921095  
P3--.0405739855645473566  
P4-.09088119928118398596  
P5--.098800129470509721  
P6--.090900000741485675  
GO TO 499

240 3187 P1-.9123951258454863573  
P2-.316891962592189809  
P3--.8098645354053914238  
P4-.888823286778298409  
P5--.088884597316675577  
P6--.8098000989346885982  
GO TO 499

245 3188 P1-.9648922897765471833  
P2-.274882448910745756  
P3--.0744693794639030272  
P4-.0888684168473485  
P5--.8888888883069825897  
P6--.8088888883252921621  
GO TO 499

250 3221 P1-.4310866892675510686  
P2-.227173291272064237  
P3--.00054778194605772  
P4-.00000393573595041797  
P5--.0000003269948220358  
P6--.000000007106151226  
GO TO 499

255 3222 P1-.822078037308112427  
P2-.0241916283065845028  
P3--.000470138899671796  
P4-.000053298720533201  
P5--.0000003100926075167  
P6--.000000007228475151  
GO TO 499

260 3212 P1-.66519557768500447992  
P2-.02906046224930658450  
P3--.0006736127391201183  
P4-.0000008943505192074  
P5--.0000000427518992358  
P6--.0000000102529252409  
GO TO 499

270 3233 P1-.5653904076325954403  
P2-.0252947914619480946  
P3--.0003736837492451744  
P4-.0000073252746725476  
P5--.000000087820245350  
P6--.00000000745740793  
GO TO 499

275 3234 P1-.4703435823392045982  
P2-.0265728914543670140  
P3--.00041809639817123878  
P4-.000000167015428109377

FOOR PRINT

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SUBROUTINE HVHF 73/17Z OPT=1 78/05/86. 15.46.54 PAGE 6

290 3253 P5--.00000001695331205125  
P6--.00000000003191649124  
GO TO 499  
P1--.07924456344900703675  
P2--.00619409057261458007  
P3--.00017176689203266056  
P4--.00000336086163303725  
P5--.0000003415868610413  
P6--.00000000009934521259  
GO TO 499  
3295 P1--.67305246552711750496  
P2--.0206451142472015700  
P3--.000311086035899240  
P4--.00000313879459867543  
P5--.000000170319787822  
P6--.000000004291202502  
GO TO 499  
3305 P1--.49006993964200249565  
P2--.02115152674391730159  
P3--.0006495189146997931  
P4--.0000096645954321394  
P5--.0000004977248593639  
P6--.00000001215712964  
GO TO 499  
3310 P1--.6070103508000747058  
P2--.0153036578442723215  
P3--.000110143713454599  
P4--.0000030294241563449  
P5--.0000000907094423561  
P6--.0000000000353300755  
GO TO 499  
3320 P1--.9554567625657170928  
P2--.0027842729036937965  
P3--.0002906152502728041  
P4--.0000062359206147096  
P5--.00000004780464079655  
P6--.000000001295252736  
GO TO 499  
3325 P1--.9016870627115511811  
P2--.0000200692843011748  
P3--.00034125246249002913  
P4--.00000610426738662150  
P5--.00000004381534500693  
P6--.0000000011430052737  
GO TO 499  
3330 P1--.026377620023390909  
P2--.00634015473843496657  
P3--.00043760114666942983  
P4--.0000076867798750305  
P5--.0000004522015954114  
P6--.0000000011283936594  
GO TO 499  
3340 P1--.0250322193890763947  
P2--.00602395019969201306  
P3--.0003921196096439891  
P4--.00000592456463345459  
P5--.00000001917877316929



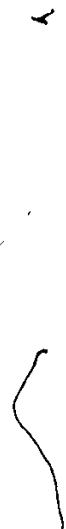
SUBROUTINE LVMP 737172 DRY=1 78/05/06. 15.45.54 PAGE 1

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SUBROUTINE LVMP(XOVR,RLVMP)
  IF(XOVR-28.9)20,10,10
  IF(XOVR-14.25)40,30,30
  IF(XOVR-11.72)60,50,50
  IF(XOVR-9.95)80,70,70
  IF(XOVR-8.27)100,90,90
  IF(XOVR-6.6)120,110,110
  RLVMP=1.15
  RETURN
  30 RLVMP=1.11*(1.15-1.11)*(XOVR-14.25)/(20.0-14.25)
  RETURN
  50 RLVMP=1.09*(1.11-1.09)*(XOVR-11.72)/(14.25-11.72)
  RETURN
  70 RLVMP=1.07*(1.09-1.07)*(XOVR-9.95)/(11.72-9.95)
  RETURN
  90 RLVMP=1.04*(1.07-1.04)*(XOVR-8.27)/(9.95-8.27)
  RETURN
  110 RLVMP=1.0*(1.04-1.0)*(XOVR-6.6)/(8.27-6.6)
  RETURN
  120 RLVMP=1.0
  RETURN
  END

```

21



POOR PRINT

-B35-

PAGE 1

76705706. 15.48.54

FTN 4.6.446

SUBROUTINE DTL 73/172 OPT=1

SUBROUTINE DTL(JCDVIF)  
IF(JCDVIF#2111,13,12

11 PRINT 1011  
GO TO 30  
12 PRINT 1012  
FORMAT(1H)LOW VOLTAGE INT,DUTY(=FIRST CYCLE DUTY)\*  
GO TO 30  
13 PRINT 1013  
FORMAT(1H)HIGH VOLTAGE MOM,DUTY(=FIRST CYCLE DUTY)\*  
GO TO 30  
1013 FORMAT(1H)HIGH VOLTAGE INT,DUTY\*  
GO TO 30  
30 RETURN  
END



FOOR PRINT

-B37-

```

490 IF (LINE-40) 101, 102, 102
402 LINE=0
60 CALL DTL(JCOVIF)
PRINT 1403
1403 FORMAT(IH, 'A3X', 'CONT'D')
401 PRINT 1400, I0BQ
1400 FORMAT(IH, //IH, '10, PAT BUS', I4)
PRINT 1426, VOLBUS(I0BQ)
1428 FORMAT(IH, I20, 'BUS VOLTAGE=', F12.4, '(KV)')
BASCUR=BKVA/VOLBUS(I0BQ), SORT(3,1)
KROW=KCOL=4480-10LNWB(I0BQ)
CALL LOCATN(KROW, KCOL, LCTN)
BUX=BUSILCTN(SUR=RBUSILCTN)
IF (TYPE-1) 1425, 1422
1422 IF (SEQR(I0BQ), PHSEOR(I0BQ)) 1423, 1424
1423 BUX=(BUX*2, PHSEOR(I0BQ))/3.
BUX=(BUX*2, PHSEOR(I0BQ))/3.
60 TO 1425
1424 PRINT 1424
1424 FORMAT(' INPUT ERROR...PHASE DUTY CALCULATION./
-- SHOULD BE DONE BEFORE L-LB DUTY CALCULATION.2)
STOP
1425 EOVPU=1, 0/BUX
EOVMP=BASCUR/BUX
PRINT 1438, EOVMP, EOVPU
1430 FORMAT(IH, I20, 'CALCULATED E', F12.4, '(SYN, KA), (P.U.)')
IF (TYPE-1) 1425, 110
1435 PRINT 140
1440 FORMAT(IH, I25, 'CONTRIBUTIONS FROM ADJACENT BUSES')
LINE=LINE+6
DO 400 NRQU=1, IBRN
BRANX=OLARM(NRBU)
BRANB=OLBR(NRBU)
INTERM=INCDEMINRBU/1000
I1OR=MOD(I1TERM, 100)
I1ERAM=INTERM/100
IF (RMB=MONIINTERM, 100)
TCODMG=I1TERM/100
IF (IFRMB-I0BQ) 445, 450, 445
IF (I1OR-I0BQ) 445, 460, 460
445 NEAR=ITON500 TO 465
450 NEAR=IFRMB
460 NEAR=IFRMB
465 CURADB=1, 0/BRANX*BASCUR
468 CRABPU=CURADB/MA3EOR
GO TO 469
105 KROW=10LNWB(NEARB)
KCOL=NWB
CALL LOCATN(KROW, KCOL, LCTN)
BMEAR=BUSILCTN)
CURANBE(1, 0=BMEARX/BUXI1BASCUR/(BRANX*FACTORI(CODMG, JCOVIF))
CRABPU=CURADB/BASCUR
110 IF (LINE-50) 471, 472, 472
LINE=0
CALL DTL(JCOVIF)
PRINT 1407
PRINT 1400, I0BQ

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115 PRINT 1472
1172 FORMAT('...',22X,'CONT'D=')
1173 LINE LINEAL
1174 PRINT 1474,HEAR8,CURAB8,CRABPU
1179 FORMAT('H',I25,'FROM BUS ',I4,'...',I15,5,'(SYM,KAI)',F10.5,
1180 '(P,U,I)')
1181 CONTINUE
1182 C
1183 IF (MONDO) 905,1180
1184 IF (T08Q) 1186
1185 DO 910 MAX1,MAXMON
1186 IF (MONDOR(MN)-IOTO) 910,915
1187 CONTINUE
1188 GO TO 1188
1189 PRINT 1915
1195 FORMAT('H',I25,'--REMOTE MONITORING--')
1196 IF (MONTOR(MN),I25,'CURRENT',*,I55,'*/BUS VOLT/*')
1197 IF (MONDOR(MN),I11988,920
1198 DO 920 (B9),I0RM
1199 INTER=INCEN(I1B1)/1000
1200 I108=MOD(INTER,100)
1201 INTER=INTER/100
1202 IFROM=MOD(INTER,100)
1203 ICODMG=INTER/100
1204 IF (I108-I08Q) 921,970
1205 IF (IFROM-I0BQ) 922,970
1206 IF (IFROM) 945,925
1207 KOL=IOLN8(I108)
1208 KCOL=NB80
1209 CALL LOCATN(KROW,KCOL,LCTN)
1210 XTQ=XBUS(LCTN)
1211 IF (XTQ) 930,970
1212 CMNPU=XTQ/BOX/KOLRM(I1B1)/FACTOR(I1CODMG,JCDVIF)
1213 VOLFB=0
1214 VOLTB=IBUX=XTQ/BOX
1215 GO TO 940
1216 KROW=IOLN8(IFROM)
1217 KCOL=NB80
1218 CALL LOCATN(KROW,KCOL,LCTN)
1219 XTQ=XBUS(LCTN)
1220 IF (XTQ) 947,970
1221 VOLFR=IBUX=XTQ/BOX
1222 KROW=IOLN8(I108)
1223 KCOL=NB80
1224 CALL LOCATN(KROW,KCOL,LCTN)
1225 XTQ=XBUS(LCTN)
1226 IF (XTQ) 950,948
1227 PRINT 1948
1228 FORMAT('H',*,WRONG,...,I948 IN RESULT*)
1229 STOP
1230 VOLTB=IBUX=XTQ/BOX
1231 CMNPU=VOLFB=VOLTB)/KOLRM(I1B1)/FACTOR(I1CODMG,JCDVIF)
1232 IF (LINE-50) 960,962,962
1233 LINE=0
1234 CALL DILL(JCDVIF)
1235 PRINT 1403
1236 PRINT 1400,INRO

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958 PRINT 147Z
LINE=LINE+2
PRNT 1969,IFROMB,ITOB,CHNPU,VOLFB,XOLIB
FORMAT 1H,125,9FROM BUS,14, TO BUS,14,
-//,155,9FROM BUS,176, TO BUS,
-1H,130, //,15,5,(P,U,1//,155,17,3,(P,U,1,170,17,3,(P,U,1)
175
180 CONTINUE
970 GO TO 1100
980 MN=MH+1
IMOVES=0
IF (MH-MAXMH) GT 984,989
KT0B=MOD(IMONFORIMN),10001
KFROMB=(IMONFOR(MH)-KT0B)/1000
984 IF (KT0B-KFROMB) 981,1109
981 IF (KT0B) 985,982
982 KROW=IOLNMB(KFROMB)
KCOL=MNBQ
CALL LOCATN(KROW,KCOL,LCTN)
XFO=XBUS(LCTN)
IF (XFO) 1810,985
185 PRINT 1995,KFROMB,KTOR
1995 FORMAT 1H,130, INPUT ERROR, CHECK REMOTE MONITORING,
-1H,130, FAULT BUS IS NOT CONNECTED TO THE NETWORK,
-//, WHICH CONTAINS F-BUS,14, AND/OR T-BUS,14, //,
GO TO 980
985 X80=IOLNMB(ITOB)
KCOL=MNBQ
CALL LOCATN(KROW,KCOL,LCTN)
XTO=XBUS(LCTN)
IF (XTO) 987,995
987 IF (KFROMB) 990,1030
990 KROW=IOLNMB(KFROMB)
KCOL=MNBQ
CALL LOCATN(KROW,KCOL,LCTN)
XFG=XBUS(LCTN)
IF (XFG) 1050,995
1010 IF (KFROMB-1080) 1011,960
1011 KPIB=KFROMB
DO 1016 KZ=1,IBRN
INTERM=INCDEM(KF)/1000
IF (B=MOD(INTERM,1000))
ICODMG=INTERM/1000
IF (IFB-KPIB) 1014,1016
CHNPU=XEO/8UX/XOLB(KF)/FACTOR(ICODMG,JCDFIF)
VOLFB=(BUX-XFG)/8UX
VOLTFR=0
IMOVES=1
IF (LTC-50) 1020,1016,1016
1018 LINE=1-1
CALL DIF(JCDFIF)
PRINT 1403
PRINT 1400,1080
PRINT 147Z
1020 LNF=LINE+2
PRINT 1969,KFROMB,KT0B,CHNPU,VOLFB,VOLT8
1014 CONTINUE

```

230 GO TO 1066  
 1030 IF (KT08-1080) 1031, 980  
 1031 KTB=KT08

DO 1034 KT=1, 1BRN  
 INTER=INCOEN(KT)/1000  
 IFTB=MOD(INTER, 10000)  
 ICD04G=INTER/10000  
 IF (IFTB-KFTB) 1034, 1036  
 1036 CHMPU=I02/8UX/K0LBRN(KT)/LACT08(IIC004G, JCOVIF)  
 VOLFR=0

VOLTR=(BUS-XTO)/8UX  
 INOYES=1  
 IF (LINE-50) 1039, 1038, 1038  
 1038 LINE=0

CALL DILLJCOVIF  
 PRINT 1400, 1080  
 PRINT 1472

1039 LINE=LINE+2  
 PRINT 1969, KFR0MB, KT08, CHMPU, VOLFR, VOLTR  
 1034 CONTINUE  
 GO TO 1066

1050 IF (KT08-1080) 1051, 980  
 1051 IF (KFR0MB-1080) 1052, 980  
 1052 IF (KT08-KFR0MB) 1054, 1090  
 1054 KFTB=KT08-100-KFR0MB  
 KFTB=KFR0MB+100-KT08

DO 1060 KFI=1, 1BRN  
 INTER=INCOEN(KFI)/1000  
 IF (MOD(INTER, 10000))  
 ICD04G=INTER/10000  
 IF (IFTB-KFTB) 1063, 1062  
 1063 IF (IFTB-KFTB) 1060, 1062  
 VOLFR=(BUS-XTO)/8UX  
 1062 VOLTR=(BUS-XTO)/8UX

CHMPU=I02/8UX/K0LBRN(KFI)/FACTOR(IIC004G, JCOVIF)  
 INOYES=1  
 1060 IF (LINE-50) 1065, 1062, 1062  
 1062 LINE=0  
 CALL DILLJCOVIF

PRINT 1400  
 PRINT 1400, 1080  
 PRINT 1472

1065 LINE=LINE+2  
 PRINT 1969, KFR0MB, KT08, CHMPU, VOLFR, VOLTR  
 CONTINUE

1066 IF (INOYES) 980, 1065  
 1065 PRINT 1061, KFR0MB, KT08  
 1061 FORMAT(1H, '3J1, INPUT ERROR, NO BRANCH/  
 - CONNECTS BUS, 14, AND BUS, 14)

GO TO 980  
 1090 PRINT 11090  
 11090 FORMAT(1H, 'WRONG 11090 IN RESULT')  
 STOP

C  
 C  
 1100 IF (JCOVIF-2) 1500, 700, 600

```

500 IF (NDR) 502, 550
502 XVR=BXZ/BUR
    CALL LVF(AVR, HLMVF)
    DUTY=EDVXPRCVF
290 PRINT 1505, XVR, RLVF, DUTY
    FORMAT(IH, T20, X/R, F10, 4/1H, T20, X, F, 0,
    -F10, X, ANSI C 37, 13-1973, 9, 1, 4, 3) 1H, T20,
    -INT, DUTY, F15, 5, (SYM, KA)
    LINE=LINE+3
    GO TO 30
295 DUTY=LOVXMP+1, 15
    PRINT 1555, EDVXMP, DUTY
305 FORMAT(IH, T20, X/R, ROUNKNOM)
    -IH, T20, INT, DUTY, F15, 5, IF NO M, F, 15,
    -APPLIC, 1H, T20, 8, F15, 5, IF M, F, 15, 15,
    -APPLIC, AS PER ANSI C 37, 13-1973, 9, 1, 4, 3)
    LINE=LINE+3
    GO TO 30
300 DUTY=EDVXMP+1, 6
    PRINT 1600, DUTY
305 FORMAT(IH, T20, X/M, DUTY(FIRST CYCLE DUTY), F15, 5, (ASTH, KA))
    LINE=LINE+1
    GO TO 30
310 XVR=BXZ/BUR
    IF (LINE=45) 701, 702, 702
315 LINE=0
    CALL DIL(JCVIF)
    PRINT 1403
    PRINT 1400, 1000
    PRINT 1472
    PRINT 1700, XVR
320 FORMAT(IH, T20, X/R, F10, 4)
    C ***** sep sep
    C SECTION FOR ANAD
    ALLCUR=0
    MTCUR=0
    DO 799 NDBM=1, 18RN
    BRAN=OLBRM(NDBM)
    BRAN=ROLBRM(NDBM)
    INTER=INCDEN(NDBM)/1000
    ITOB=MOD(INTER, 100)
    INTER=INTER/100
    IF (AOR=MOD(INTER, 100))
    ICDMG=INTER/100
    IF (ICDMG=0) 710, 730
    IF (IFROM) 799, 7155
325 710 IF (ICDMG=2) 713, 713, 799
    715 MIOB=IOLNMB(IITOB)
    713 IF (MIOB=0) 715, 715
    714 GEMHT=0
    ALLCUR=ALLCUR+1/(BRAN*FACTOR(ICDMG, JCVIF))
    GO TO 716
    KROM=KCOLANTOB
    CALL LOCATN(KROV, KCOL, LCIN)
    XJ=ABUS(LCIN)
    GEMCUR=1/(BRAN*FACTOR(ICDMG, JCVIF)+BUX)
    ALLCUR=ALLCUR+GEMCUR

```



FOOR PRINT

-B43-

SUBROUTINE RESULT 73/172 OPT=1  
 400  
 END  
 FIN 4100450 78/00/00 8103027 PAGE 8

POOR PRINT

APPENDIX C

SAMPLE RUNNINGS

# FOOR PRINT |

## 1. SAMPLE 1

The first sample calculates solutions for the same sample system that Stagg<sup>(1)</sup> used, with some modifications and additions. A "change case" demonstration has been included.

The validity of this program concerning the formation of  $R_{BUS}$  and  $X_{BUS}$  can be checked by comparing  $X_{BUS}$  for "L.V. int. duty calculation" of this sample running with the same given in<sup>(1)</sup>.

Note that lines R and X are corrected by correction factors before they are used to form  $R_{BUS}$  and  $X_{BUS}$  in the cases of H.V. int. and mom. duty calculations. So  $X_{BUS}$  for H.V. duty calculations cannot be compared with that of (1).

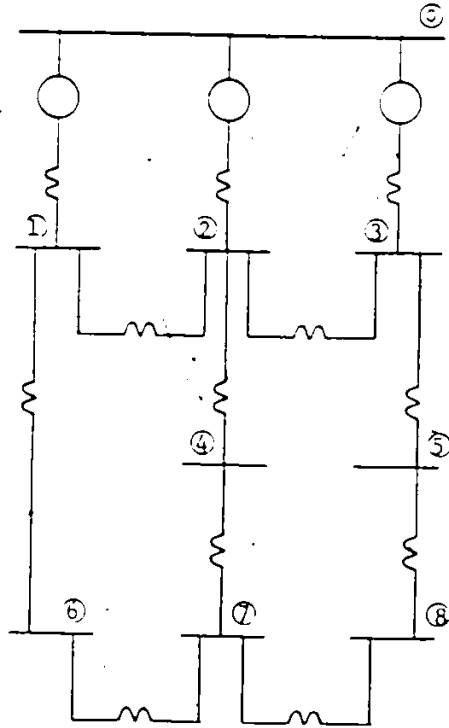
In this sample, the base MVA is 100 MVA and type of fault is a 3 phase short circuit.

### 1.1 System Description

Fig. C1 shows the initial case which is identical to Stagg<sup>(1)</sup> in its topology. Bus voltages are assigned to system buses arbitrarily as shown in Fig. C1. Line information is tabulized in Table C1.

# FOOR PRINT |

-C3-



Bus Voltages

Bus	Voltage (kV)
1	4.16
2	4.16
3	0.48
4	4.16
5	0.48
6	0.48
7	0.48
8	0.48

Fig. C1 Sample running 1  
- initial case

Table C1: Line Information - sample running 1

Line	R	X	Identification
0 1	0.001	0.01	Utility
0 2	0.0005	0.015	Turbogenerator
1 2	0.002	0.084	Cable
0 3	0.0002	0.005	Induction motor 500 hp 1800 rpm
2 3	0.008	0.122	Cable, Transformer, etc.
2 4	0.002	0.084	
3 5	0.001	0.037	
1 6	0.007	0.126	
6 7	0.01	0.168	
4 7	0.0015	0.084	
5 8	0.0008	0.037	
7 8	0.008	0.14	



Fig. C2 shows change case. In addition to several changes in the original system, a separate system is included together with new bus voltages as shown in the figure. Additional information to get Fig. C2 from Fig. C1 is tabulized in Tables C2 and C3.

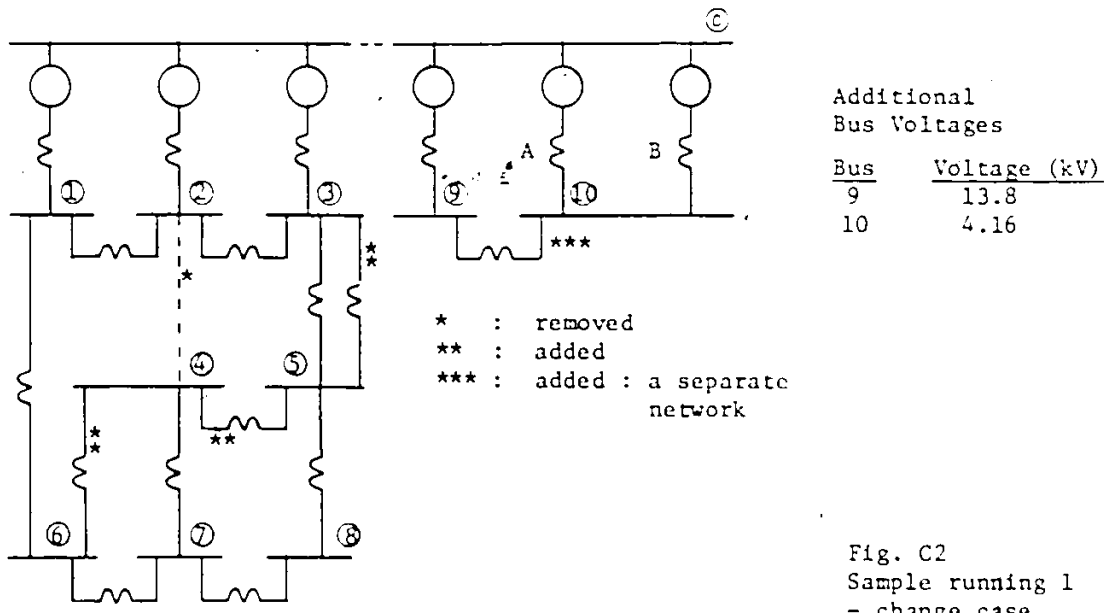


Fig. C2  
Sample running 1  
- change case

Table C2: Added Information - sample running 1

Line	R	X	Identification
3 5	0.001	0.06	Transformer
4 5	0.002	0.04	Transformer
4 6	0.003	0.05	Transformer
0 9	0.0002	0.004	Turbogenerator
0 10(A)	0.001	0.5	Synch. motor
0 10(B)	0.002	0.7	700 hp 1800 rpm Ind. motor

Table C3: Removed Information - sample running 1

Line	R	X	Identification
2 4	0.002	0.084	Cable



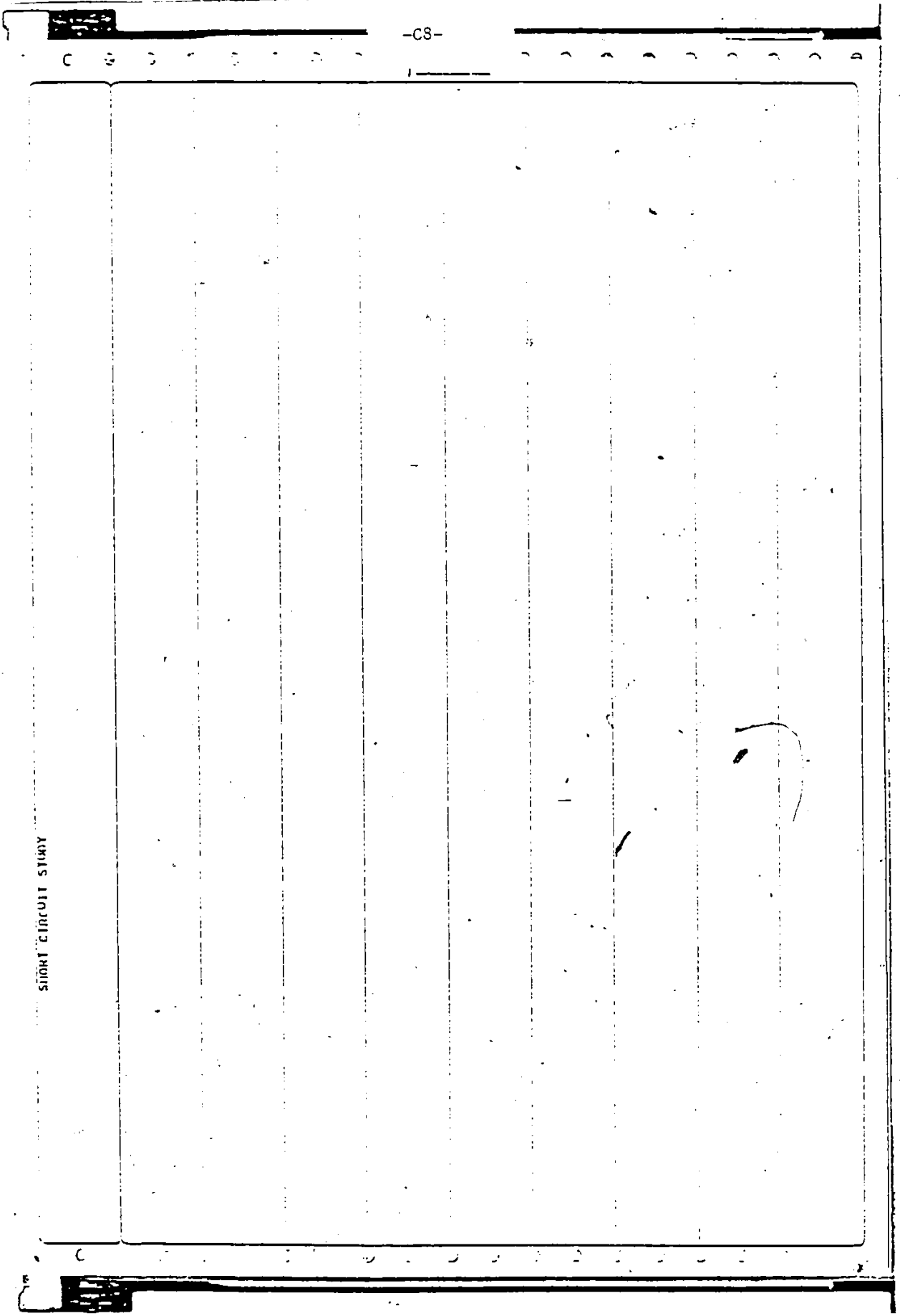


1.3 Result of computer running

FOOR PRINT I

-CS-

SIGHT CIRCUIT STAMP



JOB NAME=EXAMPLE...G.W.STAGG

DESCRIPTION=NONE BY HWANG

BASE PAY= 100.00

TYPE OF FAULT=3PHASE SHORT CIRCUIT

DUTY CALCULATIONS TO BE DONE BY THIS STUDY ARE...  
(IF H.V. INT.DUTY CAL. IS REQUIRED)  
RATED INT.TIME AND CONT.PARTING TIME IN CYCLES  
OF THE C.B. TO BE CHECKED ARE AS SHOWN.)

AT BUSES

- 1, 3, 8.
- INT.TIME= 2; PARTING TIME=1.5;
- INT.TIME= 3; PARTING TIME=2.0;
- FIRST CYCLE DUTY WANTED

AT BUSES

- 2, 4, 5.
- INT.TIME= 5; PARTING TIME=3.0; 4.0;
- INT.TIME= 8; PARTING TIME=4.0; 5.0;
- FIRST CYCLE DUTY WANTED

AT BUSES

- 6, 7.
- FIRST CYCLE DUTY WANTED

REMOTE MONITORING  
FAULTED BUS//MONITORED BRANCH FROM BUS/TO BUS

3	27	31	37	51
8	57	81	67	71
2	47	71	17	21
4	07	11	07	31
5	17	21	27	31
6	17	21	17	61
7	17	21	27	31
	17	21	27	31

Handwritten mark resembling a stylized 'L' or '7'.

BUS VOLTAGES  
 BUSES AT 4.16KV  
 1, 2, 4,  
 AT LEAST 3BUSES AT THIS VOLTAGE.  
 BUSES AT 7.48KV

3, 5, 6, 7, 8,  
 AT LEAST 5BUSES AT THIS VOLTAGE.  
 IDENTIFICATION CODE FOR BRANCH IMPEDANCES

- ID CODE1=A T/G,H/G WITH AHOR,WINDING,OR CONDENSER.
- ID CODE2=AN H/G WITHOUT AHOR,WINDING.
- ID CODE3=A SYNCH-MOTOR.
- ID CODE4=AN IND.-MTR. ARV 1000HP AT 1800RPM,OR ADV 250HP AT 3600RPM.
- ID CODE5=AN IND.-MTR.50HP AND ADV...NOT BIGGER THAN 1000HP AT 1800 RPM OR 250HP AT 3600RPM.
- ID CODE6=AN IND.-MTR. SMALLER THAN 50HP.
- ID CODE7=A STATIC ELEMENT...CABLE(BUSDUCT,TRF,RTTR,ETC.
- ID CODE8=UTILITY SYSTEM/OFFSITE SOURCE,ETC.



# FOOR PRINT I

-C12-

IMPEDANCES FROM RUS	TO RUS	H	X	IDEN. CODE
7	B	.0080	.1400	7
5	B	.0009	.0370	7
4	7	.0015	.0840	7
6	7	.0100	.1680	7
1	6	.0070	.1260	7
3	5	.0010	.0370	7
2	4	.0020	.0840	7
2	3	.0080	.1220	7
0	3	.0002	.0050	5
1	2	.0020	.0840	7
0	2	.0005	.0150	1
0	1	.0010	.0100	A

POOR PRINT

-C13-

SHORT CIRCUIT DUTIES

2

COMPUTER CENTER

CONCORDIA UNIVERSITY



LOW VOLTAGE INT-DUTY(FIRST CYCLE DUTY)

AT BUS 3  
 BUS VOLTAGE = 4800(KV)  
 CALCULATED E/X = 25271.3442(SYM,KAI) = 210.1020(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 5 = 343.6680(SYM,KAI) = 2.8587(P.U.)  
 FROM BUS 2 = 871.21490(SYM,KAI) = 7.24314(P.U.)  
 FROM BUS 0 = 24056.26122(SYM,KAI) = 200.00000(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 5 TO BUS 8// FROM BUS 5 TO BUS 6  
 -2.85887(P.U.)// .106(P.U.) .212(P.U.)  
 FROM BUS 6 TO BUS 7// FROM BUS 6 TO BUS 5  
 1.27061(P.U.)// .820(P.U.) .612(P.U.)  
 X/R = 24.6959  
 M.F. = 1.1500(ANSI C 37.13-1973...9.1.4.J)  
 INT.DUTY = 29062.04581(SYM,KAI)

AT BUS 5  
 BUS VOLTAGE = 4800(KV)  
 CALCULATED E/X = 32841875(SYM,KAI) = 27.3042(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 = 411.12348(SYM,KAI) = 3.41802(P.U.)  
 FROM BUS 3 = 2873.06403(SYM,KAI) = 23.88621(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS 1 TO BUS 5  
 .26297(P.U.)// .984(P.U.) .962(P.U.)  
 FROM BUS 1 TO BUS 6// FROM BUS 1 TO BUS 5  
 1.29073(P.U.)// .984(P.U.) .822(P.U.)  
 X/R = 33.6360  
 M.F. = 1.1500(ANSI C 37.13-1973...9.1.4.J)  
 INT.DUTY = 3776.81564(SYM,KAI)

AT BUS 6  
 BUS VOLTAGE = 4800(KV)  
 CALCULATED E/X = 13364769(SYM,KAI) = 11.1113(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 1 = 448.20569(SYM,KAI) = 3.7424(P.U.)  
 FROM BUS 7 = 888.19121(SYM,KAI) = 7.38428(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS 1 TO BUS 5  
 -4.2625(P.U.)// .930(P.U.) .966(P.U.)  
 FROM BUS 2 TO BUS 3// FROM BUS 2 TO BUS 5  
 -1.9892(P.U.)// .966(P.U.) .990(P.U.)  
 X/R = 18.5102  
 M.F. = 1.1397(ANSI C 37.13-1973...9.1.4.J)  
 INT.DUTY = 1523.17136(SYM,KAI)

LOW VOLTAGE INT. DUTY + FIRST CYCLE DUTY (CONT'D)

AT BUS 7 BUS VOLTAGE = 4800 (KV)  
 CALCULATED E/X = 1607.2813 (SYN, KAI) = 13.3627 (P.U.)  
 CONTRIBUTIONS FROM ADJACENT BUSES -  
 FROM BUS 4 = 548.1843 (SYN, KAI) = 4.55752 (P.U.)  
 FROM BUS 5 = 685.04642 (SYN, KAI) = 5.52911 (P.U.)  
 FROM BUS 6 = 398.04801 (SYN, KAI) = 3.27605 (P.U.)  
 REMOTE MONITORING -  
 /CURRENT /BUS VOLT/  
 FROM BUS 1 TO BUS 2 // FROM BUS 1 TO BUS 2  
 4797 (P.U.) // .963 (P.U.) .929 (P.U.)  
 FROM BUS 2 TO BUS 3 // FROM BUS 2 TO BUS 3  
 38049 (P.U.) // .929 (P.U.) .975 (P.U.)  
 X/R = 30.5370  
 M.F. = 1.1500 (ANST C 37.13-1973...9.1.4.3)  
 INT. DUTY = 148.3734 (SYN, KAI)

AT BUS 8 BUS VOLTAGE = 4800 (KV)  
 CALCULATED E/X = 1996.9485 (SYN, KAI) = 16.6023 (P.U.)  
 CONTRIBUTIONS FROM ADJACENT BUSES -  
 FROM BUS 4 = 422.79429 (SYN, KAI) = 3.93074 (P.U.)  
 FROM BUS 5 = 1524.15423 (SYN, KAI) = 12.67158 (P.U.)  
 REMOTE MONITORING -  
 /CURRENT /BUS VOLT/  
 FROM BUS 4 TO BUS 7 // FROM BUS 4 TO BUS 7  
 235912 (P.U.) // .757 (P.U.) .550 (P.U.)  
 FROM BUS 1 TO BUS 2 // FROM BUS 1 TO BUS 2  
 22243 (P.U.) // .983 (P.U.) .963 (P.U.)  
 X/R = 35.4976  
 M.F. = 1.1500 (ANST C 37.13-1973...9.1.4.3)  
 INT. DUTY = 229.49080 (SYN, KAI)

RHUS AND XHUS MATRICES FOR REV. INT. DUTY STUDY

RHUS	XHUS	MATRICES	...	(RHUS, XHUS)
RHUS1 1, 1	XHUS1 1, 1	.000626562		.000895591
RHUS1 2, 1	XHUS1 2, 1	.001378382		.001350909
RHUS1 3, 1	XHUS1 3, 1	.000366296		.011558114
RHUS1 4, 1	XHUS1 4, 1	.000019005		.000305626
RHUS1 5, 1	XHUS1 5, 1	.000413416		.001515413
RHUS1 6, 1	XHUS1 6, 1	.000538989		.013026146
RHUS1 7, 1	XHUS1 7, 1	.001640822		.002091616
RHUS1 8, 1	XHUS1 8, 1	.000330761		.000576482
RHUS1 9, 1	XHUS1 9, 1	.000104671		.003281001
RHUS1 10, 1	XHUS1 10, 1	.001870165		.066732215
RHUS1 11, 1	XHUS1 11, 1	.000358132		.000742712
RHUS1 12, 1	XHUS1 12, 1	.000065833		.002238027
RHUS1 13, 1	XHUS1 13, 1	.000499512		.011644261
RHUS1 14, 1	XHUS1 14, 1	.000250368		.009787356
RHUS1 15, 1	XHUS1 15, 1	.001386242		.043234586
RHUS1 16, 1	XHUS1 16, 1	.000483129		.066297015
RHUS1 17, 1	XHUS1 17, 1	.000196935		.003212639
RHUS1 18, 1	XHUS1 18, 1	.000073098		.002341837
RHUS1 19, 1	XHUS1 19, 1	.000729281		.018718611
RHUS1 20, 1	XHUS1 20, 1	.000101433		.007854250
RHUS1 21, 1	XHUS1 21, 1	.004867524		.090265973
RHUS1 22, 1	XHUS1 22, 1	.000103765		.002832242
RHUS1 23, 1	XHUS1 23, 1	.000281360		.005694850
RHUS1 24, 1	XHUS1 24, 1	.000152188		.005056786
RHUS1 25, 1	XHUS1 25, 1	.001536788		.040887945
RHUS1 26, 1	XHUS1 26, 1	.000389469		.017336801
RHUS1 27, 1	XHUS1 27, 1	.001128543		.034224583
RHUS1 28, 1	XHUS1 28, 1	.002478218		.076001038
RHUS1 29, 1	XHUS1 29, 1	.000492634		.001179316
RHUS1 30, 1	XHUS1 30, 1	.000864266		.002960639
RHUS1 31, 1	XHUS1 31, 1	.000467930		.010270386
RHUS1 32, 1	XHUS1 32, 1	.000367670		.016286807
RHUS1 33, 1	XHUS1 33, 1	.001295626		.037820895
RHUS1 34, 1	XHUS1 34, 1	.000267535		.013366712
RHUS1 35, 1	XHUS1 35, 1	.000579353		.029616574
RHUS1 36, 1	XHUS1 36, 1	.001957783		.065371404

HIGH VOLTAGE INT-DUTY

1 AT BUS  
 VOLTAGE = 4.1600 (KV)  
 CALCULATED E/X = 1560.168 (SYM.KA) = 112.4152 (P.U.)  
 - CONTRIBUTIONS FROM ADJACENT BUSES -  
 FROM BUS 6 = 32.1763 (SYM.KA) = 2.3184 (P.U.)  
 FROM BUS 2 = 140.12925 (SYM.KA) = 10.09678 (P.U.)  
 FROM BUS 4 = 1387.86122 (SYM.KA) = 100.00000 (P.U.)  
 - REMOTE MONITORING -  
 /CURRENT /BUS VOLT /  
 FROM BUS 2 TO BUS 3 // FROM BUS TO BUS  
 FROM BUS 3 TO BUS 5 // .848 (P.U.) .966 (P.U.)  
 FROM BUS 5 // FROM BUS TO BUS  
 1.32724 (P.U.) // .966 (P.U.) .917 (P.U.)  
 X/R = 12.8427  
 M/C/D RATIO = .90604  
 INT-DUTY  
 C.B. INT-TIME/CONT-PRING TIME / M.F. / DUTY (SYM.KA)  
 2.0 1.5 1.00 1560.16680  
 3.0 2.0 1.00 1560.16680

2 AT BUS  
 VOLTAGE = 4.1600 (KV)  
 CALCULATED E/X = 1211.2475 (SYM.KA) = 87.2744 (P.U.)  
 - CONTRIBUTIONS FROM ADJACENT BUSES -  
 FROM BUS 4 = 41.55202 (SYM.KA) = 2.99394 (P.U.)  
 FROM BUS 3 = 98.71369 (SYM.KA) = 7.11265 (P.U.)  
 FROM BUS 1 = 145.74095 (SYM.KA) = 10.50112 (P.U.)  
 FROM BUS 6 = 925.24082 (SYM.KA) = 66.66667 (P.U.)  
 - REMOTE MONITORING -  
 /CURRENT /BUS VOLT /  
 FROM BUS 0 TO BUS 1 // FROM BUS TO BUS  
 FROM BUS 1 TO BUS 3 // 0.000 (P.U.) .842 (P.U.)  
 FROM BUS 3 // FROM BUS TO BUS  
 8.81712 (P.U.) // 0.000 (P.U.) .068 (P.U.)  
 X/R = .28.8887  
 M/C/D RATIO = .15028  
 INT-DUTY  
 C.B. INT-TIME/CONT-PRING TIME / M.F. / DUTY (SYM.KA)  
 5.0 3.0 1.04 1256.73321  
 5.0 4.0 1.00 1242.04344  
 8.0 4.0 1.05 1266.09055  
 8.0 5.0 1.02 1233.22151





HBUS AND XBUS MATRICES FOR  
H.V.M.M. (FIRST CYCLE) DUTY STUDY

HBUS AND XBUS MATRICES ... (HUS+BUS)							
HBUS 1, 1	1	1	0.000000000	XBUS 1, 1	1	1	.008915306
HBUS 1, 2	1	2	0.000000000	XBUS 1, 2	1	2	.001330867
HBUS 1, 3	1	3	0.000000000	XBUS 1, 3	1	3	.011358308
HBUS 1, 4	1	4	0.000000000	XBUS 1, 4	1	4	.0001327302
HBUS 1, 5	1	5	0.000000000	XBUS 1, 5	1	5	.0006561276
HBUS 1, 6	1	6	0.000000000	XBUS 1, 6	1	6	.0056571100
HBUS 1, 7	1	7	0.000000000	XBUS 1, 7	1	7	.0020479951
HBUS 1, 8	1	8	0.000000000	XBUS 1, 8	1	8	.0083602151
HBUS 2, 1	2	1	0.000000000	XBUS 2, 1	2	1	.0014271169
HBUS 2, 2	2	2	0.000000000	XBUS 2, 2	2	2	.0662032486
HBUS 2, 3	2	3	0.000000000	XBUS 2, 3	2	3	.0005870636
HBUS 2, 4	2	4	0.000000000	XBUS 2, 4	2	4	.0014714225
HBUS 2, 5	2	5	0.000000000	XBUS 2, 5	2	5	.0050587128
HBUS 2, 6	2	6	0.000000000	XBUS 2, 6	2	6	.0081250099
HBUS 2, 7	2	7	0.000000000	XBUS 2, 7	2	7	.0373420573
HBUS 2, 8	2	8	0.000000000	XBUS 2, 8	2	8	.0062659321
HBUS 3, 1	3	1	0.000000000	XBUS 3, 1	3	1	.0030585165
HBUS 3, 2	3	2	0.000000000	XBUS 3, 2	3	2	.0010170361
HBUS 3, 3	3	3	0.000000000	XBUS 3, 3	3	3	.0183044038
HBUS 3, 4	3	4	0.000000000	XBUS 3, 4	3	4	.0066659606
HBUS 3, 5	3	5	0.000000000	XBUS 3, 5	3	5	.0900278003
HBUS 3, 6	3	6	0.000000000	XBUS 3, 6	3	6	.0027651235
HBUS 3, 7	3	7	0.000000000	XBUS 3, 7	3	7	.0053620494
HBUS 3, 8	3	8	0.000000000	XBUS 3, 8	3	8	.0021961661
HBUS 4, 1	4	1	0.000000000	XBUS 4, 1	4	1	.0401662820
HBUS 4, 2	4	2	0.000000000	XBUS 4, 2	4	2	.0147785973
HBUS 4, 3	4	3	0.000000000	XBUS 4, 3	4	3	.0337102911
HBUS 4, 4	4	4	0.000000000	XBUS 4, 4	4	4	.0749705146
HBUS 4, 5	4	5	0.000000000	XBUS 4, 5	4	5	.0010429070
HBUS 4, 6	4	6	0.000000000	XBUS 4, 6	4	6	.0022847174
HBUS 4, 7	4	7	0.000000000	XBUS 4, 7	4	7	.0044603148
HBUS 4, 8	4	8	0.000000000	XBUS 4, 8	4	8	.014829029
HBUS 5, 1	5	1	0.000000000	XBUS 5, 1	5	1	.0326254019
HBUS 5, 2	5	2	0.000000000	XBUS 5, 2	5	2	.0123221791
HBUS 5, 3	5	3	0.000000000	XBUS 5, 3	5	3	.0273610805
HBUS 5, 4	5	4	0.000000000	XBUS 5, 4	5	4	.0607904889
HBUS 5, 5	5	5	0.000000000				
HBUS 5, 6	5	6	0.000000000				
HBUS 5, 7	5	7	0.000000000				
HBUS 5, 8	5	8	0.000000000				
HBUS 6, 1	6	1	0.000000000				
HBUS 6, 2	6	2	0.000000000				
HBUS 6, 3	6	3	0.000000000				
HBUS 6, 4	6	4	0.000000000				
HBUS 6, 5	6	5	0.000000000				
HBUS 6, 6	6	6	0.000000000				
HBUS 6, 7	6	7	0.000000000				
HBUS 6, 8	6	8	0.000000000				
HBUS 7, 1	7	1	0.000000000				
HBUS 7, 2	7	2	0.000000000				
HBUS 7, 3	7	3	0.000000000				
HBUS 7, 4	7	4	0.000000000				
HBUS 7, 5	7	5	0.000000000				
HBUS 7, 6	7	6	0.000000000				
HBUS 7, 7	7	7	0.000000000				
HBUS 7, 8	7	8	0.000000000				
HBUS 8, 1	8	1	0.000000000				
HBUS 8, 2	8	2	0.000000000				
HBUS 8, 3	8	3	0.000000000				
HBUS 8, 4	8	4	0.000000000				
HBUS 8, 5	8	5	0.000000000				
HBUS 8, 6	8	6	0.000000000				
HBUS 8, 7	8	7	0.000000000				
HBUS 8, 8	8	8	0.000000000				

HIGH VOLTAGE MON. DUTY (FIRST CYCLE DUTY)

AT BUS 1 BUS VOLTAGE = 4.1600 (KV)  
 CALCULATED E/A = 1560.8786 (SYM,KA) = 112.4665 (P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 6 = 32.52582 (SYM,KA) = 2.34359 (P.U.)  
 FROM BUS 2 = 140.49156 (SYM,KA) = 10.12288 (P.U.)  
 FROM BUS 0 = 1387.66122 (SYM,KA) = 100.00000 (P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 -1.19451 (P.U.)// .850 (P.U.) .985 (P.U.)  
 FROM BUS 3 TO BUS 5// FROM BUS TO BUS  
 1.38344 (P.U.)// .985 (P.U.) .934 (P.U.)  
 MON. DUTY (FIRST CYCLE DUTY) = 2497.40576 (ASYM,KA)

AT BUS 2 BUS VOLTAGE = 4.1600 (KV)  
 CALCULATED E/A = 1221.8870 (SYM,KA) = 88.0407 (P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 4 = 43.61200 (SYM,KA) = 3.14239 (P.U.)  
 FROM BUS 3 = 107.16768 (SYM,KA) = 7.72179 (P.U.)  
 FROM BUS 1 = 145.86249 (SYM,KA) = 10.50988 (P.U.)  
 FROM BUS 0 = 925.24082 (SYM,KA) = 66.66667 (P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 0 TO BUS 1// FROM BUS TO BUS  
 1.17105 (P.U.)// 0.000 (P.U.) .883 (P.U.)  
 FROM BUS 0 TO BUS 3// FROM BUS TO BUS  
 9.62700 (P.U.)// 0.000 (P.U.) .942 (P.U.)  
 MON. DUTY (FIRST CYCLE DUTY) = 1955.01277 (ASYM,KA)

AT BUS 4 BUS VOLTAGE = 4.1600 (KV)  
 CALCULATED E/A = 209.4466 (SYM,KA) = 15.0913 (P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 7 = 65.07049 (SYM,KA) = 4.68854 (P.U.)  
 FROM BUS 2 = 144.37611 (SYM,KA) = 10.40278 (P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 1.13404 (P.U.)// .969 (P.U.) .874 (P.U.)  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 -.85762 (P.U.)// .874 (P.U.) .978 (P.U.)  
 MON. DUTY (FIRST CYCLE DUTY) = 335.11456 (ASYM,KA)

JOB NAME=CHANGE CASF 1...

DESCRIPTION= .....

BASE HVA= 100.00

TYPE OF FAULT=3PHASE SHORT CIRCUIT

DUTY CALCULATIONS TO BE DONE BY THIS STUDY ARE...  
(IF H.V. INT.DUTY CAL. IS REQUIRED)  
RATED INT.TIME AND CONT.PARTING TIME IN CYCLES  
OF THE C.B. TO BE CHECKED ARE AS SHOWN.)

AT BUSES

1, 0, 9,

INT.TIME= 2, PARTING TIME=1.5,

INT.TIME= 3, PARTING TIME=2.0,

FIRST CYCLE DUTY WANTED

AT BUSES

2, 4, 5, 10,

INT.TIME= 5, PARTING TIME=3.0, 4.0,

INT.TIME= 8, PARTING TIME=4.0, 5.0,

FIRST CYCLE DUTY WANTED

AT BUSES

6, 7,

FIRST CYCLE DUTY WANTED

POOR PRINT

-C23-

RENOTE MONITORING  
FAULTED BUS//MONITORED BRANCH(FROM BUS/TO BUS)

3	2/	3/	3/	5/
5	5/	8/	6/	7/
8	4/	7/	1/	2/
2	0/	1/	0/	3/
4	1/	2/	2/	3/
5	1/	2/	1/	6/
6	1/	2/	2/	3/
7	1/	2/	2/	3/

BUS VOLTAGES  
BUSES AT 13.80KV  
AT LEAST 1BUSES AT THIS VOLTAGE.

BUSES AT 4.16KV  
1, 2, 4, 10,  
AT LEAST 4BUSES AT THIS VOLTAGE.

BUSES AT 3, 5, 6, 7, 8,  
AT LEAST 5BUSES AT THIS VOLTAGE.  
IDENTIFICATION CODE FOR BRANCH IMPEDANCES

ID CODE1=A T/G+H/G WITH AMOR WINDING OR CONDENSER

ID CODE2=AN H/G WITHOUT AMOR WINDING

ID CODE3=A SYNCH. MOTOR

ID CODE4=AN IND. MTR. ABV 1000HP AT 1800RPH OR  
ABV 250HP AT 3600RPH

ID CODE5=AN IND. MTR. 50HP AND ABV... NOT BIGGER THAN  
1000HP AT 1800 RPH OR 250HP AT 3600RPH.

ID CODE6=AN IND. MTR. SMALLER THAN 50HP.

ID CODE7=A STATIC ELEMENT... CABLE, BUSDUCT, TRF, XTR, ETC.

ID CODE8=UTILITY SYSTEM OFF SITE SOURCE ETC.

IMPEDANCES FROM BUS	TO BUS	R	X	IDEN. CODE
2	4	.0020	.0840	7
4	6	.0030	.0500	7
4	5	.0020	.0400	7
3	5	.0010	.0600	7
0	9	.0002	.0040	1
9	10	.0020	.0500	7
10	0	.0010	.5000	5
0	10	.0020	.7000	3

FOOR PRINT-1

-C26-

SHORT CIRCUIT BUTIFS

RBUS AND XBUS MATRICES FOR  
L.V. INT. DUTY STUDY

RBUS AND XBUS MATRICES  
.....(RBUS,XBUS)

RBUS( 1, 1)	.0006712311	XBUS( 1, 1)	.0087212532
RBUS( 2, 1)	.0001283264	XBUS( 2, 1)	.0012186004
RBUS( 3, 1)	.0004060018	XBUS( 3, 1)	.0117373398
RBUS( 3, 2)	.0000143392	XBUS( 3, 2)	.0002331733
RBUS( 3, 3)	.0000119920	XBUS( 3, 3)	.0004748532
RBUS( 4, 1)	.0001923753	XBUS( 4, 1)	.0047239956
RBUS( 4, 2)	.0001384643	XBUS( 4, 2)	.0023584552
RBUS( 4, 3)	.0000335035	XBUS( 4, 3)	.0006636245
RBUS( 4, 4)	.0001593893	XBUS( 4, 4)	.0035995642
RBUS( 5, 1)	.0019330049	XBUS( 5, 1)	.0466112849
RBUS( 5, 2)	.0004305000	XBUS( 5, 2)	.0011156205
RBUS( 5, 3)	.0000149902	XBUS( 5, 3)	.0005552220
RBUS( 5, 4)	.0001845936	XBUS( 5, 4)	.0042571157
RBUS( 5, 5)	.0005657305	XBUS( 5, 5)	.0206266800
RBUS( 6, 1)	.0006565539	XBUS( 6, 1)	.0244377520
RBUS( 6, 2)	.0002692800	XBUS( 6, 2)	.0038630235
RBUS( 6, 3)	.0000571619	XBUS( 6, 3)	.0007948559
RBUS( 6, 4)	.001232793	XBUS( 6, 4)	.0028035363
RBUS( 6, 5)	.0014472698	XBUS( 6, 5)	.0346172361
RBUS( 6, 6)	.0004356097	XBUS( 6, 6)	.0160130364
RBUS( 6, 7)	.0028966533	XBUS( 6, 7)	.0571393703
RBUS( 7, 1)	.0001917666	XBUS( 7, 1)	.0024407332
RBUS( 7, 2)	.00003640594	XBUS( 7, 2)	.0006700010
RBUS( 7, 3)	.000185409	XBUS( 7, 3)	.0035560331
RBUS( 7, 4)	.0017013283	XBUS( 7, 4)	.0373289402
RBUS( 7, 5)	.0005426734	XBUS( 7, 5)	.0203743882
RBUS( 7, 6)	.0014613227	XBUS( 7, 6)	.0358468701
RBUS( 7, 7)	.0026653223	XBUS( 7, 7)	.0754200173
RBUS( 8, 1)	.0000517888	XBUS( 8, 1)	.0013924215
RBUS( 8, 2)	.0000185419	XBUS( 8, 2)	.0005793826
RBUS( 8, 3)	.0001822255	XBUS( 8, 3)	.0041105617
RBUS( 8, 4)	.0006489667	XBUS( 8, 4)	.0241181192
RBUS( 8, 5)	.0006480193	XBUS( 8, 5)	.0235833403
RBUS( 8, 6)	.0005306745	XBUS( 8, 6)	.0001595101
RBUS( 8, 7)	.0007538233	XBUS( 8, 7)	.0318811016
RBUS( 8, 8)	.0013849106	XBUS( 8, 8)	.0545873984
RBUS( 9, 1)	0.0000000000	XBUS( 9, 1)	0.0000000000
RBUS( 9, 2)	0.0000000000	XBUS( 9, 2)	0.0000000000
RBUS( 9, 3)	0.0000000000	XBUS( 9, 3)	0.0000000000
RBUS( 9, 4)	0.0000000000	XBUS( 9, 4)	0.0000000000
RBUS( 9, 5)	0.0000000000	XBUS( 9, 5)	0.0000000000
RBUS( 9, 6)	0.0000000000	XBUS( 9, 6)	0.0000000000
RBUS( 9, 7)	0.0000000000	XBUS( 9, 7)	0.0000000000
RBUS( 9, 8)	0.0000000000	XBUS( 9, 8)	0.0000000000
RBUS( 9, 9)	0.001864665	XBUS( 9, 9)	.0039537126
RBUS( 10, 1)	0.0000000000	XBUS( 10, 1)	0.0000000000
RBUS( 10, 2)	0.0000000000	XBUS( 10, 2)	0.0000000000
RBUS( 10, 3)	0.0000000000	XBUS( 10, 3)	0.0000000000
RBUS( 10, 4)	0.0000000000	XBUS( 10, 4)	0.0000000000
RBUS( 10, 5)	0.0000000000	XBUS( 10, 5)	0.0000000000
RBUS( 10, 6)	0.0000000000	XBUS( 10, 6)	0.0000000000
RBUS( 10, 7)	0.0000000000	XBUS( 10, 7)	0.0000000000
RBUS( 10, 8)	0.0000000000	XBUS( 10, 8)	0.0000000000
RBUS( 10, 9)	.0000451116	XBUS( 10, 9)	.0003751205
RBUS( 10, 10)	.0005116279	XBUS( 10, 10)	.0455664273



LOW VOLTAGE INT. DUTY (FIRST CYCLE DUTY)

AT BUS 3 BUS VOLTAGE = .4800(KV)  
 CALCULATED E/X = 254617734(SYM.KA) = 211.6852(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 5 = 821.28621(SYM.KA) = 2.67112(P.U.)  
 FROM BUS 2 = 886.09943(SYM.KA) = 7.26689(P.U.)  
 FROM BUS 0 = 24056.26122(SYM.KA) = 200.80000(P.U.)  
 FROM BUS 5 = 198.12650(SYM.KA) = 1.64719(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 5 TO BUS 8// FROM BUS TO BUS  
 FROM BUS 6 TO BUS 7// FROM BUS TO BUS  
 FROM BUS 6 TO BUS 7// FROM BUS TO BUS  
 FROM BUS 6 TO BUS 7// FROM BUS TO BUS  
 X/R = 24.5561  
 M.F. = 1.1500(ANSI C 37.13-1973...9.1.4.3)  
 INT. DUTY = 29281.03936(SYM.KA)

AT BUS 5 BUS VOLTAGE = .4800(KV)  
 CALCULATED E/X = 4921.9464(SYM.KA) = 40.9203(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 8 = 112.99243(SYM.KA) = .93940(P.U.)  
 FROM BUS 3 = 2684.54082(SYM.KA) = 22.31805(P.U.)  
 FROM BUS 4 = 468.94633(SYM.KA) = 3.89875(P.U.)  
 FROM BUS 3 = 1655.46684(SYM.KA) = 13.76329(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 X/R = 37.2212  
 M.F. = 1.1500(ANSI C 37.13-1973...9.1.4.3)  
 INT. DUTY = 5660.23038(SYM.KA)

AT BUS 6 BUS VOLTAGE = .4800(KV)  
 CALCULATED E/X = 210540513(SYM.KA) = 17.5011(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 1 = 266.77140(SYM.KA) = 2.21790(P.U.)  
 FROM BUS 1 = 890.07495(SYM.KA) = 7.39994(P.U.)  
 FROM BUS 4 = 948.20496(SYM.KA) = 7.88323(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 X/R = 19.7260  
 M.F. = 1.1481(ANSI C 37.13-1973...9.1.4.3)  
 INT. DUTY = 2410.79653(SYM.KA)

LOW VOLTAGE INT. DUTY (FIRST CYCLE DUTY) CONT'D

AT BUS 7 VOLTAGE= 4800(KV)  
 CALCULATED EX= 1594.8194(SYM.KA) = 13.2591(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 8 = 495.9784(SYM.KA) = 4.12347(P.U.)  
 FROM BUS 4 = 723.19510(SYM.KA) = 6.01253(P.U.)  
 FROM BUS 6 = 375.64781(SYM.KA) = 3.12308(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLTS/  
 FROM BUS 1 TO BUS 2// FROM BUS 1 TO BUS 2  
 FROM BUS 2 TO BUS 3// FROM BUS 2 TO BUS 3  
 FROM BUS 3 TO BUS 4// FROM BUS 3 TO BUS 4  
 FROM BUS 4 TO BUS 5// FROM BUS 4 TO BUS 5  
 FROM BUS 5 TO BUS 6// FROM BUS 5 TO BUS 6  
 FROM BUS 6 TO BUS 7// FROM BUS 6 TO BUS 7  
 FROM BUS 7 TO BUS 8// FROM BUS 7 TO BUS 8  
 X/R= 28.2968  
 M.F.= 1.1500(IANSI C 37.13-1973...9.1.4.3)  
 INT. DUTY= 1834.04230(SYM.KA)

AT BUS 8 VOLTAGE= 4800(KV)  
 CALCULATED EX= 2203.4629(SYM.KA) = 18.3192(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 7 = 357.37487(SYM.KA) = 2.97116(P.U.)  
 FROM BUS 5 = 1846.08801(SYM.KA) = 15.34809(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLTS/  
 FROM BUS 4 TO BUS 7// FROM BUS 4 TO BUS 7  
 FROM BUS 7 TO BUS 8// FROM BUS 7 TO BUS 8  
 FROM BUS 1 TO BUS 2// FROM BUS 1 TO BUS 2  
 FROM BUS 2 TO BUS 3// FROM BUS 2 TO BUS 3  
 FROM BUS 3 TO BUS 4// FROM BUS 3 TO BUS 4  
 FROM BUS 5 TO BUS 6// FROM BUS 5 TO BUS 6  
 FROM BUS 6 TO BUS 7// FROM BUS 6 TO BUS 7  
 FROM BUS 7 TO BUS 8// FROM BUS 7 TO BUS 8  
 X/R= 39.4158  
 M.F.= 1.1500(IANSI C 37.13-1973...9.1.4.3)  
 INT. DUTY= 2533.98231(SYM.KA)

HHUS AND XHUS MATRICES FOR  
H.V. INT. DUTY STUDY

HHUS AND XHUS MATRICES ... (HHUS, XHUS)

HHUS1 1	1	1	.0006731415	XHUS1 1	1	1	.0087408389
HHUS1 2	1	2	.0007101208	XHUS1 2	1	2	.0012587717
HHUS1 3	1	3	.0004873158	XHUS1 3	1	3	.0118197338
HHUS1 4	1	4	.0000399701	XHUS1 4	1	4	.0006299700
HHUS1 5	1	5	.0000331486	XHUS1 5	1	5	.0012921086
HHUS1 6	1	6	.0005362396	XHUS1 6	1	6	.0127629384
HHUS1 7	1	7	.0001578223	XHUS1 7	1	7	.0026608041
HHUS1 8	1	8	.0000511151	XHUS1 8	1	8	.0012837616
HHUS1 9	1	9	.0004442922	XHUS1 9	1	9	.0097250322
HHUS1 10	1	10	.0021699564	XHUS1 10	1	10	.0512787353
HHUS1 11	1	11	.0000676442	XHUS1 11	1	11	.0014732912
HHUS1 12	1	12	.0000373869	XHUS1 12	1	12	.0012886428
HHUS1 13	1	13	.0005145491	XHUS1 13	1	13	.0115015554
HHUS1 14	1	14	.0008391093	XHUS1 14	1	14	.0261467463
HHUS1 15	1	15	.0009731627	XHUS1 15	1	15	.0109662124
HHUS1 16	1	16	.0002857050	XHUS1 16	1	16	.0040985097
HHUS1 17	1	17	.0000707836	XHUS1 17	1	17	.0012778524
HHUS1 18	1	18	.0003436367	XHUS1 18	1	18	.0075743837
HHUS1 19	1	19	.0016298430	XHUS1 19	1	19	.0382525002
HHUS1 20	1	20	.0008479519	XHUS1 20	1	20	.0203123734
HHUS1 21	1	21	.0003037842	XHUS1 21	1	21	.0599707115
HHUS1 22	1	22	.0001602996	XHUS1 22	1	22	.0027394258
HHUS1 23	1	23	.0000515774	XHUS1 23	1	23	.0012834364
HHUS1 24	1	24	.0004419274	XHUS1 24	1	24	.0096074229
HHUS1 25	1	25	.0010161233	XHUS1 25	1	25	.0419399450
HHUS1 26	1	26	.0008345974	XHUS1 26	1	26	.0258277097
HHUS1 27	1	27	.0016629243	XHUS1 27	1	27	.0394401713
HHUS1 28	1	28	.0020988675	XHUS1 28	1	28	.0799752591
HHUS1 29	1	29	.0000760674	XHUS1 29	1	29	.001778922
HHUS1 30	1	30	.0000386770	XHUS1 30	1	30	.0012875549
HHUS1 31	1	31	.0005074742	XHUS1 31	1	31	.011056068
HHUS1 32	1	32	.0009388179	XHUS1 32	1	32	.029441657
HHUS1 33	1	33	.0009602659	XHUS1 33	1	33	.0294920621
HHUS1 34	1	34	.0010222580	XHUS1 34	1	34	.0243108397
HHUS1 35	1	35	.0016934470	XHUS1 35	1	35	.0371466889
HHUS1 36	1	36	.0000000000	XHUS1 36	1	36	.0606741027
HHUS1 37	1	37	.0000000000	XHUS1 37	1	37	.0000000000
HHUS1 38	1	38	.0000000000	XHUS1 38	1	38	.0000000000
HHUS1 39	1	39	.0000000000	XHUS1 39	1	39	.0000000000
HHUS1 40	1	40	.0000000000	XHUS1 40	1	40	.0000000000
HHUS1 41	1	41	.0000000000	XHUS1 41	1	41	.0000000000
HHUS1 42	1	42	.0000000000	XHUS1 42	1	42	.0000000000
HHUS1 43	1	43	.0000000000	XHUS1 43	1	43	.0000000000
HHUS1 44	1	44	.0000000000	XHUS1 44	1	44	.0000000000
HHUS1 45	1	45	.0000000000	XHUS1 45	1	45	.0000000000
HHUS1 46	1	46	.0000000000	XHUS1 46	1	46	.0000000000
HHUS1 47	1	47	.0000000000	XHUS1 47	1	47	.0000000000
HHUS1 48	1	48	.0000000000	XHUS1 48	1	48	.0000000000
HHUS1 49	1	49	.0000000000	XHUS1 49	1	49	.0000000000
HHUS1 50	1	50	.0000000000	XHUS1 50	1	50	.0000000000
HHUS1 51	1	51	.0000000000	XHUS1 51	1	51	.0000000000
HHUS1 52	1	52	.0000000000	XHUS1 52	1	52	.0000000000
HHUS1 53	1	53	.0000000000	XHUS1 53	1	53	.0000000000
HHUS1 54	1	54	.0000000000	XHUS1 54	1	54	.0000000000
HHUS1 55	1	55	.0000000000	XHUS1 55	1	55	.0000000000
HHUS1 56	1	56	.0000000000	XHUS1 56	1	56	.0000000000
HHUS1 57	1	57	.0000000000	XHUS1 57	1	57	.0000000000
HHUS1 58	1	58	.0000000000	XHUS1 58	1	58	.0000000000
HHUS1 59	1	59	.0000000000	XHUS1 59	1	59	.0000000000
HHUS1 60	1	60	.0000000000	XHUS1 60	1	60	.0000000000
HHUS1 61	1	61	.0000000000	XHUS1 61	1	61	.0000000000
HHUS1 62	1	62	.0000000000	XHUS1 62	1	62	.0000000000
HHUS1 63	1	63	.0000000000	XHUS1 63	1	63	.0000000000
HHUS1 64	1	64	.0000000000	XHUS1 64	1	64	.0000000000
HHUS1 65	1	65	.0000000000	XHUS1 65	1	65	.0000000000
HHUS1 66	1	66	.0000000000	XHUS1 66	1	66	.0000000000
HHUS1 67	1	67	.0000000000	XHUS1 67	1	67	.0000000000
HHUS1 68	1	68	.0000000000	XHUS1 68	1	68	.0000000000
HHUS1 69	1	69	.0000000000	XHUS1 69	1	69	.0000000000
HHUS1 70	1	70	.0000000000	XHUS1 70	1	70	.0000000000
HHUS1 71	1	71	.0000000000	XHUS1 71	1	71	.0000000000
HHUS1 72	1	72	.0000000000	XHUS1 72	1	72	.0000000000
HHUS1 73	1	73	.0000000000	XHUS1 73	1	73	.0000000000
HHUS1 74	1	74	.0000000000	XHUS1 74	1	74	.0000000000
HHUS1 75	1	75	.0000000000	XHUS1 75	1	75	.0000000000
HHUS1 76	1	76	.0000000000	XHUS1 76	1	76	.0000000000
HHUS1 77	1	77	.0000000000	XHUS1 77	1	77	.0000000000
HHUS1 78	1	78	.0000000000	XHUS1 78	1	78	.0000000000
HHUS1 79	1	79	.0000000000	XHUS1 79	1	79	.0000000000
HHUS1 80	1	80	.0000000000	XHUS1 80	1	80	.0000000000
HHUS1 81	1	81	.0000000000	XHUS1 81	1	81	.0000000000
HHUS1 82	1	82	.0000000000	XHUS1 82	1	82	.0000000000
HHUS1 83	1	83	.0000000000	XHUS1 83	1	83	.0000000000
HHUS1 84	1	84	.0000000000	XHUS1 84	1	84	.0000000000
HHUS1 85	1	85	.0000000000	XHUS1 85	1	85	.0000000000
HHUS1 86	1	86	.0000000000	XHUS1 86	1	86	.0000000000
HHUS1 87	1	87	.0000000000	XHUS1 87	1	87	.0000000000
HHUS1 88	1	88	.0000000000	XHUS1 88	1	88	.0000000000
HHUS1 89	1	89	.0000000000	XHUS1 89	1	89	.0000000000
HHUS1 90	1	90	.0000000000	XHUS1 90	1	90	.0000000000
HHUS1 91	1	91	.0000000000	XHUS1 91	1	91	.0000000000
HHUS1 92	1	92	.0000000000	XHUS1 92	1	92	.0000000000
HHUS1 93	1	93	.0000000000	XHUS1 93	1	93	.0000000000
HHUS1 94	1	94	.0000000000	XHUS1 94	1	94	.0000000000
HHUS1 95	1	95	.0000000000	XHUS1 95	1	95	.0000000000
HHUS1 96	1	96	.0000000000	XHUS1 96	1	96	.0000000000
HHUS1 97	1	97	.0000000000	XHUS1 97	1	97	.0000000000
HHUS1 98	1	98	.0000000000	XHUS1 98	1	98	.0000000000
HHUS1 99	1	99	.0000000000	XHUS1 99	1	99	.0000000000
HHUS1 100	1	100	.0000000000	XHUS1 100	1	100	.0000000000
HHUS1 101	1	101	.0000000000	XHUS1 101	1	101	.0000000000
HHUS1 102	1	102	.0000000000	XHUS1 102	1	102	.0000000000
HHUS1 103	1	103	.0000000000	XHUS1 103	1	103	.0000000000
HHUS1 104	1	104	.0000000000	XHUS1 104	1	104	.0000000000
HHUS1 105	1	105	.0000000000	XHUS1 105	1	105	.0000000000
HHUS1 106	1	106	.0000000000	XHUS1 106	1	106	.0000000000
HHUS1 107	1	107	.0000000000	XHUS1 107	1	107	.0000000000
HHUS1 108	1	108	.0000000000	XHUS1 108	1	108	.0000000000
HHUS1 109	1	109	.0000000000	XHUS1 109	1	109	.0000000000
HHUS1 110	1	110	.0000000000	XHUS1 110	1	110	.0000000000
HHUS1 111	1	111	.0000000000	XHUS1 111	1	111	.0000000000
HHUS1 112	1	112	.0000000000	XHUS1 112	1	112	.0000000000
HHUS1 113	1	113	.0000000000	XHUS1 113	1	113	.0000000000
HHUS1 114	1	114	.0000000000	XHUS1 114	1	114	.0000000000
HHUS1 115	1	115	.0000000000	XHUS1 115	1	115	.0000000000
HHUS1 116	1	116	.0000000000	XHUS1 116	1	116	.0000000000
HHUS1 117	1	117	.0000000000	XHUS1 117	1	117	.0000000000
HHUS1 118	1	118	.0000000000	XHUS1 118	1	118	.0000000000
HHUS1 119	1	119	.0000000000	XHUS1 119	1	119	.0000000000
HHUS1 120	1	120	.0000000000	XHUS1 120	1	120	.0000000000
HHUS1 121	1	121	.0000000000	XHUS1 121	1	121	.0000000000
HHUS1 122	1	122	.0000000000	XHUS1 122	1	122	.0000000000
HHUS1 123	1	123	.0000000000	XHUS1 123	1	123	.0000000000
HHUS1 124	1	124	.0000000000	XHUS1 124	1	124	.0000000000
HHUS1 125	1	125	.0000000000	XHUS1 125	1	125	.0000000000
HHUS1 126	1	126	.0000000000	XHUS1 126	1	126	.0000000000
HHUS1 127	1	127	.0000000000	XHUS1 127	1	127	.0000000000
HHUS1 128	1	128	.0000000000	XHUS1 128	1	128	.0000000000
HHUS1 129	1	129	.0000000000	XHUS1 129	1	129	.0000000000
HHUS1 130	1	130	.0000000000	XHUS1 130	1	130	.0000000000
HHUS1 131	1	131	.0000000000	XHUS1 131	1	131	.0000000000
HHUS1 132	1	132	.0000000000	XHUS1 132	1	132	.0000000000
HHUS1 133	1	133	.0000000000	XHUS1 133	1	133	.0000000000
HHUS1 134	1	134	.0000000000	XHUS1 134	1	134	.0000000000
HHUS1 135	1	135	.0000000000	XHUS1 135	1	135	.0000000000
HHUS1 136	1	136	.0000000000	XHUS1 136	1	136	.0000000000
HHUS1 137	1	137	.0000000000	XHUS1 137	1	137	.0000000000
HHUS1 138	1	138	.0000000000	XHUS1 138	1	138	.0000000000
HHUS1 139	1	139	.0000000000	XHUS1 139	1	139	.0000000000
HHUS1 140	1	140	.0000000000	XHUS1 140	1	140	.0000000000
HHUS1 141	1	141	.0000000000	XHUS1 141	1	141	.0000000000
HHUS1 142	1	142	.0000000000	XHUS1 142	1	142	.0000000000
HHUS1 143	1	143	.0000000000	XHUS1 143	1	143	.0000000000
HHUS1 144	1	144	.0000000000	XHUS1 144	1	144	.0000000000
HHUS1 145	1	145	.0000000000	XHUS1 145	1	145	

HIGH VOLTAGE INT-DUTY

AT BUS 1 BUS VOLTAGE= 4.1600(KV)  
 CALCULATED E/X= 1587.7895(SYM.KA)= 114.4055(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 6= 58.5003(SYM.KA)= 4.2151(P.U.)  
 FROM BUS 2= 141.42795(SYM.KA)= 10.19035(P.U.)  
 FROM BUS 0= 1387.86122(SYM.KA)= 100.00000(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 2 TO BUS 3// FROM BUS 10 BUS .928(P.U.)  
 FROM BUS 3 TO BUS 5// FROM BUS .856(P.U.) TO BUS  
 FROM BUS 2.60730(P.U.)// .928(P.U.) TO BUS .831(P.U.)  
 FROM BUS 1.60784(P.U.)// .928(P.U.) TO BUS .831(P.U.)  
 X/R = 12.9851  
 MAGD RATIO= .98739  
 INT-DUTY  
 C.B. INT-TIME/CONT-PRING TIME/ M.F. / DUTY(SYM.KA)  
 2.0 1.00 1587.7895  
 3.0 1.00 1587.7895

AT BUS 2 BUS VOLTAGE= 4.1600(KV)  
 CALCULATED E/X= 1174.1899(SYM.KA)= 84.8043(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 3= 101.3221(SYM.KA)= 7.30067(P.U.)  
 FROM BUS 1= 147.62569(SYM.KA)= 10.63693(P.U.)  
 FROM BUS 0= 925.24082(SYM.KA)= 66.66667(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ /BUS VOLT/  
 FROM BUS 0 TO BUS 1// FROM BUS TO BUS  
 FROM BUS 10.64975(P.U.)// 0.000(P.U.) TO BUS .894(P.U.)  
 FROM BUS 3// FROM BUS TO BUS .891(P.U.)  
 FROM BUS 7.28786(P.U.)// 0.000(P.U.)  
 X/R = 29.0186  
 MAGD RATIO= .13774  
 INT-DUTY  
 C.B. INT-TIME/CONT-PRING TIME/ M.F. / DUTY(SYM.KA)  
 5.0 3.0 1.04 1217.88610  
 5.0 4.0 1.02 1202.56300  
 8.0 4.0 1.04 1226.15749  
 8.0 5.0 1.02 1193.86849

CONT'D

HIGH VOLTAGE INT-DUTY

AT BUS 4  
 VOLTAGE = 4.1600(KV)  
 CALCULATED E/X = 270.6504(ISHM-KA) = 19.5013(P.U.)  
 -CONTRIBUT (ONS) FROM ADJACENT BUSES-  
 FROM BUS 7 = 30.08985(ISHM-KA) = 2.16807(P.U.)  
 FROM BUS 6 = 70.51113(ISHM-KA) = 5.08056(P.U.)  
 FROM BUS 5 = 170.04946(ISHM-KA) = 12.25263(P.U.)  
 -REMOTE MONITORING-  
 /CURRENT/ ( /BUS VOLT/  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 -31969(P.U.1// .948(P.U.) .975(P.U.)  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 1.33931(P.U.1// .975(P.U.) .810(P.U.)  
 X/R = 23.6410  
 MAFD RATIO = .99391  
 INT-DUTY C.B. INT-TIME/CONT-PRING TIME/ M.F. / DUTY(ISHM-KA)  
 5.0 3.0 1.00 291.47533  
 5.0 4.0 1.02 276.17008  
 0.0 4.0 1.12 303.01378  
 0.0 5.0 1.08 292.88587

AT BUS 9  
 VOLTAGE = 13.8000(KV)  
 CALCULATED E/X = 1052.1907(ISHM-KA) = 251.4978(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 = 1045.92440(ISHM-KA) = 250.00000(P.U.)  
 FROM BUS 10 = 0.26633(ISHM-KA) = 1.49780(P.U.)  
 X/R = 21.0169  
 MAFD RATIO = 0.00000  
 INT-DUTY C.B. INT-TIME/CONT-PRING TIME/ M.F. / DUTY(ISHM-KA)  
 2.0 1.5 1.00 1052.19071  
 3.0 2.0 1.00 1052.19073

AT BUS 10  
 VOLTAGE = 4.1600(KV)  
 CALCULATED E/X = 279.6815(ISHM-KA) = 20.1376(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 9 = 257.01134(ISHM-KA) = 18.51852(P.U.)  
 FROM BUS 0 = 27.75722(ISHM-KA) = 2.00000(P.U.)  
 FROM BUS 0 = 19.82659(ISHM-KA) = 1.42857(P.U.)  
 X/R = 55.6716  
 MAFD RATIO = .92593  
 INT-DUTY C.B. INT-TIME/CONT-PRING TIME/ M.F. / DUTY(ISHM-KA)  
 5.0 3.0 1.29 360.53229  
 5.0 4.0 1.22 340.80452  
 0.0 4.0 1.36 374.20533

# FOOR PRINT |

-C33-

HIGH VOLTAGE INT. DUTY

CONT'D

AT BUS 10 CONJ'D

5.0

1.20

357.16692

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99







(HIGH VOLTAGE MOM.DUTY)=FIRST CYCLE DUTY) CONT'D

AT BUS 9  
 HUS VOLTAGE= 13.8000(KV)  
 CALCULATED E/X= 1057.1384(SYH,KAI)= 252.6804(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0= 1045.9240(SYH,KAI)= 250.00000(P.U.)  
 FROM BUS 10= 11.21403(SYH,KAI)= 2.68041(P.U.)  
 MOM.DUTY(FIRST CYCLE DUTY)= 1691.42150(ASYH,KAI)

AT BUS 10  
 HUS VOLTAGE= 4.1600(KV)  
 CALCULATED E/X= 299.9689(SYH,KAI)= 21.6138(P.U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 9= 257.01134(SYH,KAI)= 18.51852(P.U.)  
 FROM BUS 0= 27.75722(SYH,KAI)= 2.00000(P.U.)  
 FROM BUS 0= 19.82659(SYH,KAI)= 1.42857(P.U.)  
 MOM.DUTY(FIRST CYCLE DUTY)= 479.95032(ASYH,KAI)

**FOOR PRINT I**

-C37-

THANK YOU-BYE-BYE.

FOOR PRINT I

-C38-

HMANALV. 70/06/10. CONCORDIA UNIVERSITY - CYBER 172/2.

12.23.11.HWANGJ.T100.  
 12.23.11.ACCOUNT.K755161..  
 12.23.12.FIN.  
 12.23.38. 17.087 CP SECONDS COMPLETION TIME  
 12.23.38.L60. STOP  
 12.23.42. 2.576 CP SECONDS EXECUTION TIME  
 12.23.42.UFAD. 0.001KUNS.  
 12.23.42.UEMS. 2.016KUNS.  
 12.23.42.UECP. 20.9755SECS.  
 12.23.42.AESH. 24.980UNTS.

# FOOR PRINT I

## 2. SAMPLE 2

This sample demonstrates the option feature, 3 phase and 1L-G fault calculations -- with one running.

Note that, in the result for 1L-G fault, no "CONTRIBUTION FROM ADJACENT BUSES" is printed.

### 2.1 System Description

The system to be studied is shown in Fig. C3, which is a part of a real system for a nuclear power plant.

Fig. C4 and Fig. C5 show positive and negative sequence networks of the system, respectively.

In this sample running, the base MVA is 10000 MVA.

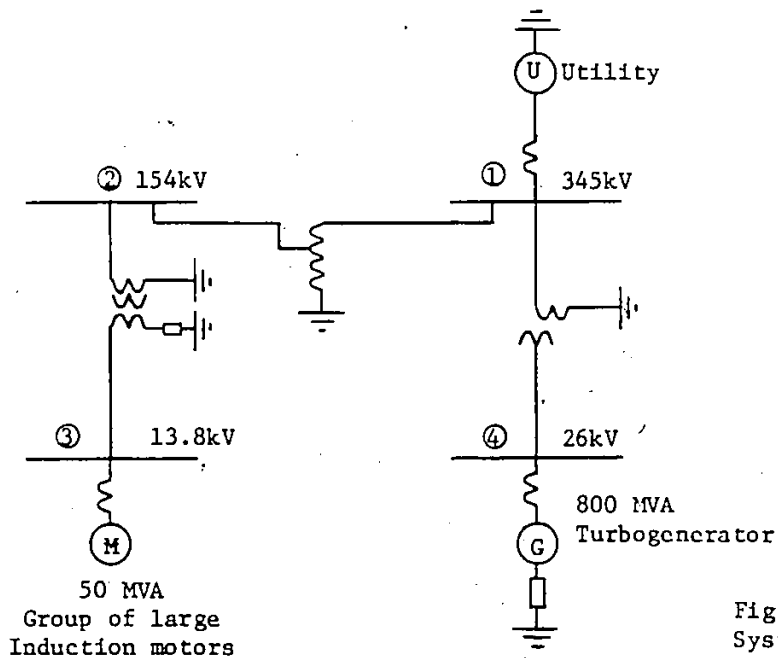


Fig. C3 Sample running 2  
System Single line diagram

# FOOT PRINT 1

-C40-

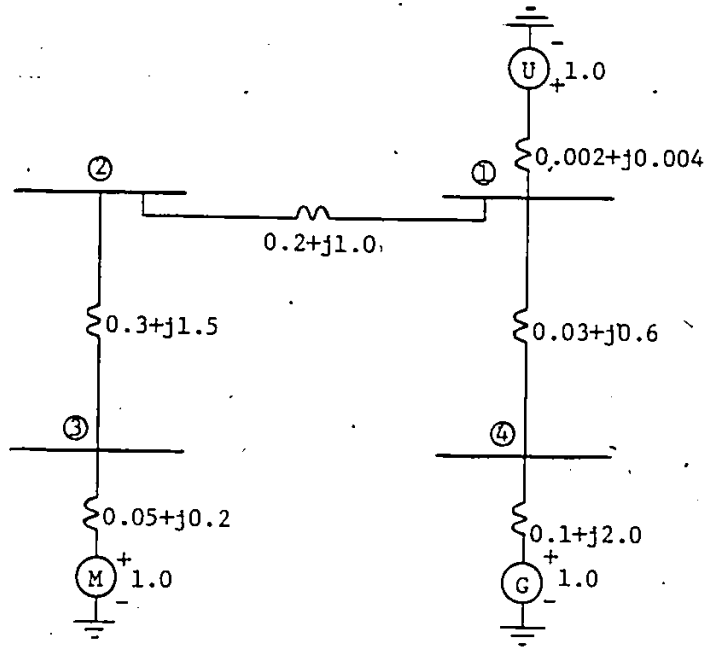


Fig. C4 Sample running 2  
- Positive sequence

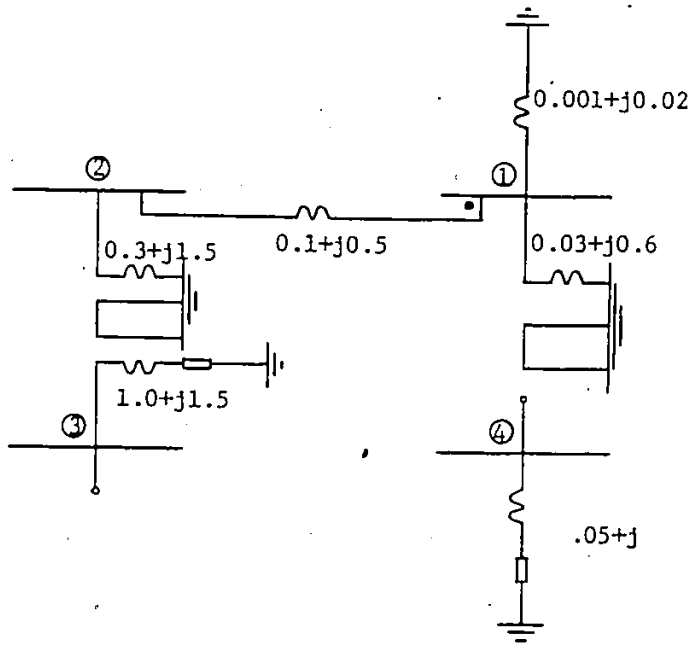


Fig. C5 Sample running 2  
- Zero sequence

# FOOR PRINT I

-C41-

2.2     - Input Data

CARD NO.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25
1	S	A	M	P	L	E	2	.	.	.	3	P	H	A	S	E		F	A	U	L	T			
2	1	0	0	0	0	.					3	1													
3	1	1	1																						
4			1																						
5	.		2																						
6			3																						
7			4																						
8	0																								
9	3	4	5	.																					
10			1																						
11	0																								
12	1	5	4	.																					
13			2																						
14	0																								
15	2	6	.																						
16			4																						
17	0	.																							
18	1	3	.	8																					
19			3																						
20	0																								
21	0																								
22	0		1			0	.	0	0	2								0	.	0	4				8
23	0		4			0	.	1											2	.	0				1
24	0		3			0	.	0	5									0	.	2					4
25	1		2			0	.	2											1	.	0				
26	2		3			0	.	3											1	.	5				
27	1		4			0	.	0	3									0	.	6					
28	0																								
29	2																								

Cont'd



# FOOR PRINT |

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-C43-

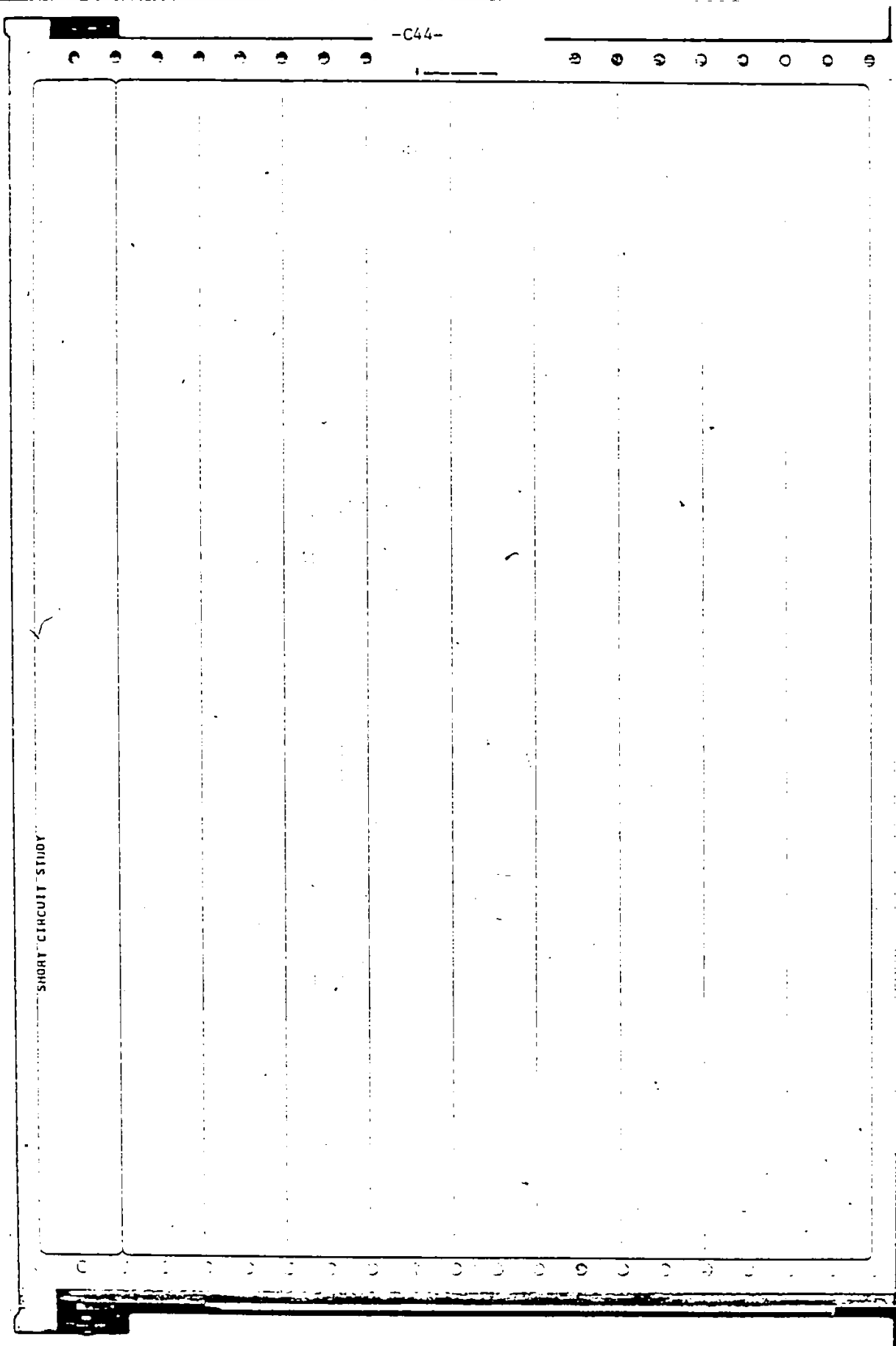
2.3 Result of computer running



**FOOR PRINT |**

-C44-

SHORT CIRCUIT STUDY



# FOOR PRINT |

-C45-

JOB NAME=SAMPLE2...3PHASE FAULT

DESCRIPTION=

BASE MVA= 10000.00

TYPE OF FAULT=3PHASE SHORT CIRCUIT

FOR ALL BUSES OF HIGH VOLTAGE,CHECKS FOR

2-1-5,3-2,0-5-3,0-8-9,0 BREAKER'S INT,DUTY AND CHECKS FOR

FIRST CYCLE DUTY WILL BE DONE.

FOR ALL BUSES OF LOWVOLTAGE CHECKS FOR FIRST CYCLE DUTY WILL BE DONE.

# FOOR PRINT I

-046-

REMOTE MONITORING  
FAULTED BUS//MONITORED BRANCH(FROM BUS/TO BUS)

- 1 ALL BRANCHES
- 2 ALL BRANCHES
- 3 ALL BRANCHES
- 4 ALL BRANCHES

BUS VOLTAGES

BUSES AT 345.00KV

BUSES AT 1 AT LEAST 1BUSES AT THIS VOLTAGE.

BUSES AT 151.00KV

BUSES AT 2 AT LEAST 1BUSES AT THIS VOLTAGE.

BUSES AT 26.00KV

BUSES AT 4 AT LEAST 1BUSES AT THIS VOLTAGE.

BUSES AT 13.00KV

BUSES AT 3 AT LEAST 1BUSES AT THIS VOLTAGE.

IDENTIFICATION CODE FOR BRANCH IMPEDANCES

ID CODE1=TA T/U,H/G WITH AMOR,WINDING,OR CONDENSER,

ID CODE2=AM H/G WITHOUT AMOR,WINDING.

ID CODE3=TA SYNCH, MOTOR.

ID CODE4=AN IND,MTR,ABV 1000HP AT 1800RPM,OR

ABV 250HP AT 3600RPM.

ID CODE5=AM IND,MTR,50HP AND ABV, NOT BIGGER THAN

1000HP AT 1800 RPM OR 250HP AT 3600RPM.

ID CODE6=AN IND,MTR, SMALLER THAN 50HP.

ID CODE7=TA STATIC ELEMENTS, CABLE,BUSDUCT,TRF,ARKTR,ETC.

ID CODE8=UTILITY SYSTEM,OFFSITE SOURCE,ETC.

IMPEDANCES FROM BUS	TO BUS	R	X	IDEN*CODE
0	1	.0020	.0400	8
0	4	.1000	2.0000	1
0	3	.0500	.2000	4
1	2	.2000	1.0000	7
2	3	.3000	1.5000	7
1	4	.0300	.6000	7



RBUS AND XBUS MATRICES FOR  
H.V. INT. DUTY STUDY

RBUS AND XBUS MATRICES ... (LUS, BUS)			
RBUS( 1, 1)	.0019629727	XBUS( 1, 1)	.0380473851
RBUS( 2, 1)	.0012801996	XBUS( 2, 1)	.0249733191
RBUS( 2, 2)	.1312696956	XBUS( 2, 2)	.6599114194
RBUS( 3, 1)	.0002560399	XBUS( 3, 1)	.0041622199
RBUS( 3, 2)	.0242530391	XBUS( 3, 2)	.1098185609
RBUS( 3, 3)	.0632507874	XBUS( 3, 3)	.2683030950
RBUS( 4, 1)	.0015997790	XBUS( 4, 1)	.0298826644
RBUS( 4, 2)	.0009847689	XBUS( 4, 2)	.0192102455
RBUS( 4, 3)	.0001969538	XBUS( 4, 3)	.0032017076
RBUS( 4, 4)	.0242304454	XBUS( 4, 4)	.4845250800

HIGHT VOLTAGE INT.DUTY

AT BUS 1  
 BUS VOLTAGE= 345.0000 (KV)  
 CALCULATED E/X= 430.7829 (SYN.KA) 25.7418 (P.U.)  
 CONTRIBUTIONS FROM ADJACENT BUSES=  
 FROM BUS 0= 18.36976 (SYN.KA) 25.0000 (P.U.)  
 FROM BUS 2= 5.97871 (SYN.KA) .35714 (P.U.)  
 FROM BUS 4= 6.43646 (SYN.KA) .38462 (P.U.)  
 -REMOTE MONITORING=  
 /CURRENT /BUS VOLT /  
 FROM BUS 0 TO BUS 4// FROM BUS 10 TO BUS 10//  
 .38462 (P.U.)// 0.000 (P.U.) .231 (P.U.)  
 FROM BUS 0 TO BUS 3// FROM BUS 10 TO BUS 10//  
 .35714 (P.U.)// 0.000 (P.U.) .893 (P.U.)  
 FROM BUS 2 TO BUS 3// FROM BUS 10 TO BUS 10//  
 .35714 (P.U.)// .357 (P.U.) .893 (P.U.)  
 K/R = 19.7901  
 MAGD RATIO = .98834  
 INT.DUTY  
 C.B. INT.TIME/CONF.PRINTG TIME/ H.F. / DUTY (SYN.KA)  
 2.0 1.5 1.00 430.78293  
 3.0 1.05 1.00 452.55427  
 5.0 1.04 1.00 448.92461  
 8.0 1.09 1.00 467.61496

AT BUS 2  
 BUS VOLTAGE= 154.0000 (KV)  
 CALCULATED E/X= 56.8973 (SYN.KA) 1.5177 (P.U.)  
 CONTRIBUTIONS FROM ADJACENT BUSES=  
 FROM BUS 1= 36.06936 (SYN.KA) .96210 (P.U.)  
 FROM BUS 3= 20.82793 (SYN.KA) .55556 (P.U.)  
 -REMOTE MONITORING=  
 /CURRENT /BUS VOLT /  
 FROM BUS 0 TO BUS 1// FROM BUS 10 TO BUS 10//  
 .94752 (P.U.)// 0.000 (P.U.) .962 (P.U.)  
 FROM BUS 0 TO BUS 4// FROM BUS 10 TO BUS 10//  
 .01458 (P.U.)// 0.000 (P.U.) .971 (P.U.)  
 FROM BUS 0 TO BUS 3// FROM BUS 10 TO BUS 10//  
 .55556 (P.U.)// 0.000 (P.U.) .833 (P.U.)  
 FROM BUS 1 TO BUS 4// FROM BUS 10 TO BUS 10//  
 .01458 (P.U.)// .962 (P.U.) .971 (P.U.)  
 K/R = 5.0195  
 MAGD RATIO = .99956  
 INT.DUTY  
 C.B. INT.TIME/CONF.PRINTG TIME/ H.F. / DUTY (SYN.KA)  
 2.0 1.5 1.00 56.89729  
 3.0 2.0 1.00 56.89729  
 5.0 3.0 1.00 56.89729  
 8.0 4.0 1.00 56.89729



HIGH VOLTAGE INT: DUTY

CONT'D

AT BUS 3  
 BUS VOLTAGE= 13.8000(KV)  
 CALCULATED E/R= 1559.3177(SYM,KA) = 7.7271(P,U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 = 2091.8480(SYM,KA) = 5.0000(P,U.)  
 FROM BUS 2 = 164.75181(SYM,KA) = .39379(P,U.)  
 -REMOTE MONITORING-  
 /CURRENT /BUS VOLT /FROM BUS TO BUS  
 FROM BUS 0 TO BUS 1// 38783(P,U.)/ 0.000(P,U.) .984(P,U.)  
 FROM BUS 0 TO BUS 4// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 2// 0.000(P,U.) .988(P,U.)  
 FROM BUS 1 TO BUS 3// .39379(P,U.)/ .984(P,U.) .591(P,U.)  
 FROM BUS 1 TO BUS 4// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 5// -.00597(P,U.)/ .984(P,U.) .986(P,U.)  
 A/R = 1.119  
 MAGD RATIO = .9982  
 INT: DUTY  
 C.B. INT. TIME/CONT. PRING TIME/ M.F. / DUTY(SYM,KA)  
 2.0 1.00 1559.31768  
 3.0 1.00 1559.31768  
 5.0 1.00 1559.31768  
 8.0 1.00 1559.31768

AT BUS 4  
 BUS VOLTAGE= 26.0000(KV)  
 CALCULATED E/R= 458.2999(SYM,KA) = 2.0639(P,U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 = 111.02890(SYM,KA) = .50000(P,U.)  
 FROM BUS 1 = 347.27100(SYM,KA) = 1.56388(P,U.)  
 -REMOTE MONITORING-  
 /CURRENT /BUS VOLT /FROM BUS TO BUS  
 FROM BUS 0 TO BUS 1// FROM BUS TO BUS  
 FROM BUS 0 TO BUS 3// 1.54185(P,U.)/ 0.000(P,U.) .938(P,U.)  
 FROM BUS 1 TO BUS 2// 0.2203(P,U.)/ 0.000(P,U.) .993(P,U.)  
 FROM BUS 1 TO BUS 3// FROM BUS TO BUS  
 FROM BUS 1 TO BUS 4// -.82203(P,U.)/ .938(P,U.) .960(P,U.)  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 FROM BUS 2 TO BUS 4// -.02203(P,U.)/ .960(P,U.) .993(P,U.)  
 A/R = 14.9899  
 MAGD RATIO = .75512  
 INT: DUTY  
 C.B. INT. TIME/CONT. PRING TIME/ M.F. / DUTY(SYM,KA)  
 2.0 1.00 458.29990  
 3.0 1.04 476.82969  
 5.0 1.03 473.67811  
 8.0 1.07 488.84028

RBUS AND XBUS MATRICES FOR  
H.V.MOM. (FIRST CYCLE) DUTY STUDY

RBUS AND XBUS MATRICES ... (HUS, BUS)	RBUS	XBUS
RBUS( 1, 1) =	0.0000000000	XBUS( 1, 1) =
RBUS( 2, 1) =	0.0000000000	XBUS( 2, 1) =
RBUS( 3, 1) =	0.0000000000	XBUS( 3, 1) =
RBUS( 4, 1) =	0.0000000000	XBUS( 4, 1) =
RBUS( 1, 2) =	0.0000000000	XBUS( 1, 2) =
RBUS( 2, 2) =	0.0000000000	XBUS( 2, 2) =
RBUS( 3, 2) =	0.0000000000	XBUS( 3, 2) =
RBUS( 4, 2) =	0.0000000000	XBUS( 4, 2) =
RBUS( 1, 3) =	0.0000000000	XBUS( 1, 3) =
RBUS( 2, 3) =	0.0000000000	XBUS( 2, 3) =
RBUS( 3, 3) =	0.0000000000	XBUS( 3, 3) =
RBUS( 4, 3) =	0.0000000000	XBUS( 4, 3) =
RBUS( 1, 4) =	0.0000000000	XBUS( 1, 4) =
RBUS( 2, 4) =	0.0000000000	XBUS( 2, 4) =
RBUS( 3, 4) =	0.0000000000	XBUS( 3, 4) =
RBUS( 4, 4) =	0.0000000000	XBUS( 4, 4) =

.0388274336  
 .0244169027  
 .6458221239  
 .0028761662  
 .0758849558  
 .1651982301  
 .0298872566  
 .0188053097  
 .0022123894  
 .4845132743

HIGH VOLTAGE MOM. DUTY (FIRST CYCLE DUTY)

AT BUS 1  
 BUS VOLTAGE= 345.0000(KV)  
 CALCULATED E/X= 431.0043(SYM,KA) = 25.7550(P,U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 418.36976(SYM,KA) = 25.00000(P,U.)  
 FROM BUS 2 6.19807(SYM,KA) = .37037(P,U.)  
 FROM BUS 4 6.43646(SYM,KA) = .38462(P,U.)  
 -REMOTE MONITORING-  
 /CURRENT/  
 FROM BUS 0 TO BUS 4// /BUS VOLT// FROM BUS TO BUS  
 .38462(P,U.)// 0.000(P,U.) .231(P,U.)  
 FROM BUS 0 TO BUS 3// FROM BUS TO BUS  
 .37037(P,U.)// 0.000(P,U.) .926(P,U.)  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 .37037(P,U.)// .370(P,U.) .926(P,U.)  
 MOM. DUTY (FIRST CYCLE DUTY) = 689.6286(ASYM,KA)

AT BUS 2  
 BUS VOLTAGE= 154.0000(KV)  
 CALCULATED E/X= 58.1225(SYM,KA) = 1.5501(P,U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 1 36.06936(SYM,KA) = .96210(P,U.)  
 FROM BUS 3 22.05310(SYM,KA) = .58824(P,U.)  
 -REMOTE MONITORING-  
 /CURRENT/  
 FROM BUS 0 TO BUS 1// /BUS VOLT// FROM BUS TO BUS  
 .96210(P,U.)// 0.000(P,U.) .962(P,U.)  
 FROM BUS 0 TO BUS 4// FROM BUS TO BUS  
 .81458(P,U.)// 0.000(P,U.) .971(P,U.)  
 FROM BUS 0 TO BUS 3// FROM BUS TO BUS  
 .58824(P,U.)// 0.000(P,U.) .882(P,U.)  
 FROM BUS 1 TO BUS 4// FROM BUS TO BUS  
 .01458(P,U.)// .962(P,U.) .971(P,U.)  
 MOM. DUTY (FIRST CYCLE DUTY) = 92.99595(ASYM,KA)

AT BUS 3  
 BUS VOLTAGE= 13.8000(KV)  
 CALCULATED E/X= 2256.6006(SYM,KA) = 5.3938(P,U.)  
 -CONTRIBUTIONS FROM ADJACENT BUSES-  
 FROM BUS 0 2091.84880(SYM,KA) = 5.00000(P,U.)  
 FROM BUS 2 164.75181(SYM,KA) = .39379(P,U.)  
 -REMOTE MONITORING-  
 /CURRENT/  
 FROM BUS 0 TO BUS 1// /BUS VOLT// FROM BUS TO BUS  
 .39379(P,U.)// 0.000(P,U.) .984(P,U.)  
 FROM BUS 0 TO BUS 4// FROM BUS TO BUS  
 .00597(P,U.)// 0.000(P,U.) .980(P,U.)  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 .39379(P,U.)// .904(P,U.) .591(P,U.)  
 FROM BUS 1 TO BUS 4// FROM BUS TO BUS  
 .00597(P,U.)// .904(P,U.) .980(P,U.)  
 MOM. DUTY (FIRST CYCLE DUTY) = 3610.56099(ASYM,KA)

HIGH VOLTAGE NOM. DUTY (FIRST CYCLE DUTY) CONT'D

AT BUS 4 BUS VOLTAGE= 26.000(KV)  
 CALCULATED EXR= 458.3111(SYM,KAI) 2.0639(P.U.)  
 -CORRECTED FROM ADJACENT BUSES-  
 FROM BUS 0 111.0200(SYM,KAI) 50000(P.U.)  
 FROM BUS 1 347.2821(SYM,KAI) 1.56393(P.U.)  
 -REMOTE MONITORING-  
 FROM BUS 0 TO BUS 1// /BUS VOLT/ FROM BUS TO BUS  
 FROM BUS 1.54110(P.U.)// 0.000(P.U.)// .938(P.U.)  
 FROM BUS 4 TO BUS 3// FROM BUS TO BUS  
 FROM BUS .02283(P.U.)// 0.000(P.U.) .995(P.U.)  
 FROM BUS 1 TO BUS 2// FROM BUS TO BUS  
 FROM BUS -.02283(P.U.)// .938(P.U.) .961(P.U.)  
 FROM BUS 2 TO BUS 3// FROM BUS TO BUS  
 FROM BUS -.02283(P.U.)// .961(P.U.) .995(P.U.)  
 NOM. DUTY (FIRST CYCLE DUTY)= 733.29771(SYM,KAI)

POOR PRINT

-C56-

JOB NAME= SAMPLER...IL-O FAULT

DESCRIPTION=  
BASE VVA 1900.00  
TYPE OF FAULT=LIME TO GROUND SHORT CIRCUIT.  
FOR ALL BUSES OF HIGH VOLTAGE,CHECKS FOR  
2-1,6,7-2,8,9-3,0,8-1,0 BREAKERS INT.DUTY AND CHECKS FOR  
FIRST CYCLE DUTY WILL BE DONE.  
FOR ALL BUSES OF LOWVOLTAGE, CHECKS FOR FIRST CYCLE DUTY WILL BE DONE.

POOR PRINT

-C57-

REMOTE MONITORING  
FAULTED BUS//MONITORED BRANCH(FROM BUS/TO BUS)  
NO REMOTE MONITORING

BUS VOLTAGES

BUSES AT 345.00KV

1 AT LEAST 1 BUSES AT THIS VOLTAGE.

BUSES AT 154.00KV

2 AT LEAST 1 BUSES AT THIS VOLTAGE.

BUSES AT 26.00KV

4 AT LEAST 1 BUSES AT THIS VOLTAGE.

BUSES AT 13.80KV

3 AT LEAST 1 BUSES AT THIS VOLTAGE.

IDENTIFICATION CODE FOR BRANCH IMPEDANCES

ID CODE 1=A T/G, H/G WITH AMOR, WINDING, OR CONDENSER.

ID CODE 2=AN H/G WITHOUT AMOR, WINDING.

ID CODE 3=A SYNCH. MOTOR.

ID CODE 4=AN IND. MTR. ADV 1000HP AT 1800RPM, OR

ADV 250HP AT 3600RPM.

ID CODE 5=AN IND. MTR. 50HP AND ADV... NOT BIGGER THAN

1000HP AT 1800 RPM OR 250HP AT 3600RPM.

ID CODE 6=AN IND. MTR. SMALLER THAN 50HP.

ID CODE 7=A STATIC ELEMENT... CABLE, BUSDUCT, TRF, HT, TR, ETC.

ID CODE 8=UTILITY SYSTEM, OFFSITE SOURCE, ETC.

POOR PRINT

-C59-

IMPEDANCES	TO BUS	R	X	IDEN+CODE
0	1	.0210	.0200	0
0	4	.0500	1.0000	1
0	3	1.0000	1.5000	7
0	1	.0300	.5000	7
0	2	.3000	1.5000	7
1	2	.1000	.5000	7



POOR PRINT

-C60-

SHORT CIRCUIT DUES

RBUS AND XBUS MATRICES FOR  
H.V. INT-DUTY STUDY

RBUS AND RBUS MATRICES ... (BUS, RBUS)			
RBUS1 1, 1	.0009653063	XBUS1 1, 1	.0191693291
RBUS1 2, 1	.0007240547	XBUS1 2, 1	.0143769960
RBUS1 3, 1	.0755430410	XBUS1 3, 1	.3857027476
RBUS1 4, 1	0.0000000000	XBUS1 4, 1	0.0000000000
RBUS1 5, 1	0.0000000000	XBUS1 5, 1	0.0000000000
RBUS1 6, 1	1.0000000000	XBUS1 6, 1	0.5000000000
RBUS1 7, 1	0.0000000000	XBUS1 7, 1	0.0000000000
RBUS1 8, 1	0.0000000000	XBUS1 8, 1	0.0000000000
RBUS1 9, 1	0.0000000000	XBUS1 9, 1	0.0000000000
RBUS1 10, 1	0.0000000000	XBUS1 10, 1	0.0000000000
RBUS1 11, 1	.0500000000	XBUS1 11, 1	0.0000000000

HIGH VOLTAGE INF. DUTY

AT BUS 1  
 BUS VOLTAGE= 345.000(KV)  
 CALCULATED E/X= 518.5106(SYM,KAI)= 30.9840(P.U.)  
 A/R = 180.2937  
 MADO RATIO= 1.00000  
 INF. DUTY  
 C.B. INT. TIME/CONT. PRNG TIME/ M.F. / DUTY(SYM,KAI)  
 2.0 1.5 1.26 652.81491  
 3.0 2.0 1.34 693.41660  
 5.0 3.0 1.41 729.68220  
 8.0 4.0 1.48 767.38056

AT BUS 2  
 BUS VOLTAGE= 154.000(KV)  
 CALCULATED E/X= 67.1136(SYM,KAI)= 1.7902(P.U.)  
 A/R = 25.1837  
 MADO RATIO= 1.00000  
 INF. DUTY  
 C.B. INT. TIME/CONT. PRNG TIME/ M.F. / DUTY(SYM,KAI)  
 2.0 1.5 1.02 48.76666  
 3.0 2.0 1.08 72.38637  
 5.0 3.0 1.06 71.43018  
 8.0 4.0 1.11 74.32584

AT BUS 3  
 BUS VOLTAGE= 13.800(KV)  
 CALCULATED E/X= 670.6957(SYM,KAI)= 1.6036(P.U.)  
 A/R = 1.8708  
 MADO RATIO= .50000  
 INF. DUTY  
 C.B. INT. TIME/CONT. PRNG TIME/ M.F. / DUTY(SYM,KAI)  
 2.0 1.5 1.00 670.89569  
 3.0 2.0 1.00 670.89569  
 5.0 3.0 1.00 670.89569  
 8.0 4.0 1.00 670.89569

AT BUS 4  
 BUS VOLTAGE= 26.000(KV)  
 CALCULATED E/X= 338.3263(SYM,KAI)= 1.5236(P.U.)  
 A/R = 39.3805  
 MADO RATIO= 0.00000  
 INF. DUTY  
 C.B. INT. TIME/CONT. PRNG TIME/ M.F. / DUTY(SYM,KAI)  
 2.0 1.5 1.12 378.80941  
 3.0 2.0 1.15 387.73162  
 5.0 3.0 1.16 393.79956  
 8.0 4.0 1.18 400.81471

RBUS AND XBUS MATRICES FOR  
H.V. MOM. (FIRST CYCLE) DUTY STUDY

RBUS	1	1	...	IBUS	IBUS
RBUS( 1, 1)	0.0000000000			0.0191693291	
RBUS( 2, 1)	0.0000000000			0.0191693291	
RBUS( 2, 2)	0.0000000000			0.3857827475	
RBUS( 3, 1)	0.0000000000			0.0000000000	
RBUS( 3, 2)	0.0000000000			0.0000000000	
RBUS( 3, 3)	0.0000000000			0.5000000000	
RBUS( 4, 1)	0.0000000000			0.0000000000	
RBUS( 4, 2)	0.0000000000			0.0000000000	
RBUS( 4, 3)	0.0000000000			0.0000000000	
RBUS( 4, 4)	0.0000000000			0.0000000000	

1 2 3 4 5 6 7 8 9 10 11 12

1 2 3 4 5 6 7 8 9 10 11 12

HIGH VOLTAGE MOM.DUTY(FIRST CYCLE DUTY)

AT BUS 1	BUS VOLTAGE=	345,000(KV)
	CALCULATED E/X=	518.5106(SYM,KAI)= 40.9040(P,U,I)
	MOM.DUTY(FIRST CYCLE DUTY)=	829.616951(SYM,KAI)
AT BUS 2	BUS VOLTAGE=	154,000(KV)
	CALCULATED E/X=	67.1136(SYM,KAI)= 1.7902(P,U,I)
	MOM.DUTY(FIRST CYCLE DUTY)=	107.381011(SYM,KAI)
AT BUS 3	BUS VOLTAGE=	13,000(KV)
	CALCULATED E/X=	670.0957(SYM,KAI)= 1.6036(P,U,I)
	MOM.DUTY(FIRST CYCLE DUTY)=	1073.433101(SYM,KAI)
AT BUS 4	BUS VOLTAGE=	26,000(KV)
	CALCULATED E/X=	338.3263(SYM,KAI)= 1.5236(P,U,I)
	MOM.DUTY(FIRST CYCLE DUTY)=	541.322021(SYM,KAI)

POOR PRINT

-C65-

THANK YOU, BYE-BYE.

HWANGH, 78/06/29, CONCORDIA UNIVERSITY, CYBER 17272.

21:58:27.HWANGH.T100.  
 21:58:27.ACCOUNT.BAKSK29.  
 21:58:27.FIN. 17:228 CP SECONDS COMPIATION TIME  
 21:58:58. LGU.  
 21:59:01. STOP  
 21:59:01. .954 CP SECONDS EXECUTION TIME  
 21:59:01.UEAD. 0.001KUNS;  
 21:59:01.UEMS. 1.958KUNS;  
 21:59:01.UECP. 19.494SECS;  
 21:59:01.AESR. 23.345UNITS;