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Characterization of Traps by Deep Level Transient Spectroscopy
in GaAs Epitaxial Layers Grown by
Close-Spaced Vapor Transport

Sylvain Bourassa

A Thesis

in

The Department

of

Electrical Engineering

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for the Degree of Master of Engineering at
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ABSTRACT

CHARACTERIZATION OF TRAPS BY DEEP LEVEL TRANSIENT SPECTROSCOPY IN GaAs EPITAXIAL LAYERS GROWN BY CLOSE-SPACED VAPOR TRANSPORT

Sylvain Bourassa

Two methods to characterize gallium arsenide (GaAs) Schottky barrier diodes are presented in this thesis. The GaAs epitaxial layers have been grown by the close-spaced vapor transport (CSVST) technique. The first method presented is the capacitance-voltage (C-V) measurement. The second method is the current-voltage (I-V) measurement.

The characterization by the C-V measurement and the I-V measurement are the prerequisite for the deep level transient spectroscopy (DLTS) technique used to characterize deep level traps in a GaAs semiconductor material. It is found that when the characterization of the diode corresponds to the required specification, the DLTS technique can be used.

The DLTS measurement uses the change in capacitance of a Schottky barrier diode under reverse bias. From these various capacitance transients measured, the apparent activation energy, the capture cross section and the concentration of deep levels are found in a GaAs sample. Two particular deep level traps have been found in these

samples; EL2 and ELCS1. For the above methods and technique outlined, theoretical and experimental considerations are presented.

Finally, the results obtained by characterization of GaAs epitaxial layers found by DLTS are presented. The probable causes of error involved in the DLTS measurements are discussed. Then a model for the EL2 trap concentration in GaAs epitaxial layers is proposed. According to this model, it is shown that the EL2 concentration is function of the possible off-stoichiometry variation with the deposition temperature for epitaxial layers grown by CSVT.

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1.0 INTRODUCTION

In the early 1980's, with the advent of new technologies in solid state devices, scientists and industries were turned towards the gallium arsenide (GaAs) semiconductor (SC) devices because of the interesting features presented over silicon (Si) devices.

There are several advantages for using GaAs. For example one of the interesting feature, is that GaAs have a wider band gap than Si allowing operation over a wider temperature range. Furthermore, GaAs provides a semi-insulating substrate which is ideal for planar device technology by ion implantation as a way of introducing dopants (1). The semi-insulating (SI) nature of the GaAs as a substrate ($\rho > 10^8$ ohm-cm) allows for the isolation of adjacent devices on the same substrate and to reduce parasitic capacitance in metal-semiconductor field-effect transistor (MESFET's) (2). Such MESFET devices are suitable for building integrated circuits (IC's) in semiconductors since they are easy to build and relies on reverse biased Schottky diode formed between the gate and the SC (3).

Finally, another interesting feature for using GaAs, is the high speed that it can provide because of the high mobility of GaAs material (1). For example GaAs transistor gates switch faster than Si transistor to transistor logic (TTL) gates since the minority carrier recombination lifetime is in the range of micro second for Si and in the range of pico second for GaAs. Further more, when operating at the same speeds as Si gates, GaAs gates require less power (3)(4).

The past research being made on GaAs and the reasons stated above bring our interests to study the interesting properties of the crystal.

In this thesis we will study the deep level traps on GaAs epitaxial layer grown by closed spaced vapor transport (CSVT) technique on Si GaAs substrate and GaAs substrate doped with Si (5).

The study of deep levels for GaAs samples is made by the deep level transient spectroscopy (DLTS) technique. The DLTS is a measurement technique used to evaluate the apparent activation energies, the concentrations of deep levels in SC's and their capture cross section. This measurement technique requires a computer system and a p^+n junction or a Schottky barrier diode for the measurement. p^+n junctions and Schottky barriers junctions are frequently used as test devices to study basic material properties since they are easy to fabricate and they allow one to see the type of defect easily (majority or minority carriers), depending on the type of semiconductor used (n type or p type).

Schottky barrier diodes are referred to as rectifying contacts. A Schottky barrier is a metal-semiconductor junction. The junction creates a bending of the semiconductor energy bands near the interface. This bending of the bands produces a depletion region which has a certain capacitance. If a bias is applied to the Schottky barrier, the bending of the energy bands will be changed, modifying the depletion layer width thus its capacitance.

The DLTS technique uses the change in capacitance of the biased junction as a basis for the measurement. Capacitance transients are measured as a function of temperature. As the temperature increases, more levels become ionized. These ionized levels modify the aspect of the capacitance transient since more free carriers are generated. From these changing capacitance transients, the concentrations and energy

levels due to impurities or defect structures of the crystal can be calculated (6).

For the study and characterization of GaAs epitaxial layer, this report is divided into four parts. In the first part, some general definitions are given on GaAs crystalline structure, point defects, shallow and deep level states in a semiconductor (SC).

The second part considers the Schottky barrier capacitance since the variation of the capacitance with voltages under reverse bias will allow the determination of the concentration of shallow donors or acceptors. These will be used to evaluate the concentration of deep levels as it is discussed in the following chapter. Furthermore, in that chapter the characteristics of the diode is examined in order to verify if it can be used for further experiments. The characteristics of the diode is found by the current-voltage measurements. In both cases, the theoretical basis are given and the experimental descriptions follow.

Then in the third part, the characterization of deep levels is studied followed by the experimental descriptions. This third chapter presents first some general definitions on capture rates and emission rates of carriers. Then the theory on capacitive measurements method is described which leads to the DLTS measurement method used in practice. The DLTS measurement on a GaAs sample will allow to find the apparent activation energies by using the Arrhenius plot, and the total trap concentration.

Finally, in the last part, the results obtained by characterization of the GaAs samples found by DLTS measurements are analyzed, discussed and compared with published data. At first, the

probable causes of error involved in the DLTS measurements are evaluated. Then a proposed model for EL2 trap is described and it will be shown that its concentration is function of the possible off-stoichiometry variation with the deposition temperature for epitaxial layers grown by CSVT. Then the report is terminated by a brief conclusion.

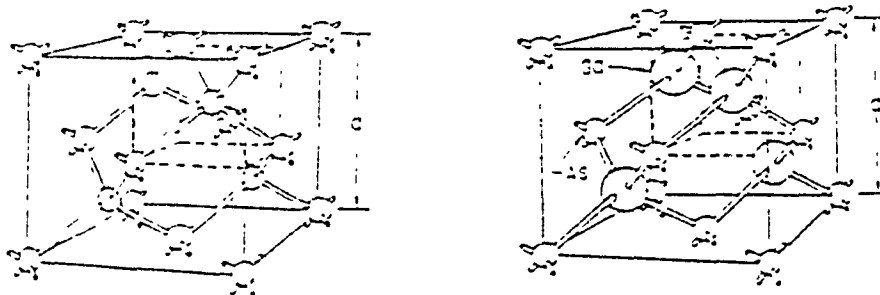
2.0 BASIC DEFINITIONS ON CRYSTALLINE STRUCTURE FOR GaAs

2.1 Crystal lattice and point defect

2.1.1 The crystal lattice

The three dimensional periodic arrangement of atoms in a crystal is called the lattice (7). Some important SC such Si and GaAs have *diamond* and *zincblende* lattice structures as shown in figure 2.1 respectively. These lattice structures are characterized by tetrahedral coordination. As it can be seen in the figure, each atom is surrounded by four equidistant nearest neighbors which lie at the corner of a tetrahedron (8).

The diamond and the zincblende lattices can be considered as two interpenetrating face-centered cubic lattices. For diamond lattice, such as Si, all the atoms are Si. In a zincblende lattice, such as GaAs, the cation sub lattice is gallium (Ga) and the anion sub lattice is arsenic (As) (5).



a) Diamond (C, Ge, Si, etc) b) Zincblende (GaAs, GaP, etc)

Fig. 2.1 Important lattice structures

2.1.2 Point defects

We have seen in section 2.1.1 an example of perfect GaAs crystal lattice, but in reality all crystals deviate from perfection. These imperfections or defects of the crystal have important consequences in material properties. They might give rise to localized energy states (9)(10).

The crystallographic defects that give rise to localized energy states in the crystal are called point defects. Point defects in a crystal are lattice flaws that cause interruptions in the lattice periodicity (11)(12). A schematic representation of simple point defects in a binary AB compound crystal semiconductor such as GaAs is shown in figure 2.2 (13) where the cation sub lattice is represented by A and the anion sublattice is represented by B. The different types of point defects are described below. Clearly, vacancies V_A and V_B of sub lattice A and B respectively are shown by rectangles numbered by 1 and 2 respectively. An anti site B_A is an atom of sub lattice B taking the place of an atom of the regular sub lattice A (rectangle #3). An anti site A_B is the contrary of B_A (rectangle #4). The substitutional impurity I_B is a foreign atom I taking the place of an atom of the regular sub lattice B (rectangle #5). A complex $I_A + V_B$ is an impurity I_A with a vacancy V_B (rectangle #6). Finally a complex $V_B + B_A$ is a vacancy V_B and anti site B_A (rectangle #7).

In a semiconductor there are two basic types of lattice disorder, the Frenkel defect and the Schottky defect. The Frenkel defect is a vacancy created by the removal of an atom from a lattice site and it is subsequently positioned interstitially (14)(15). The Schottky defect is the same as the Frenkel defect except that the atom is a missing one

instead being placed interstitially.

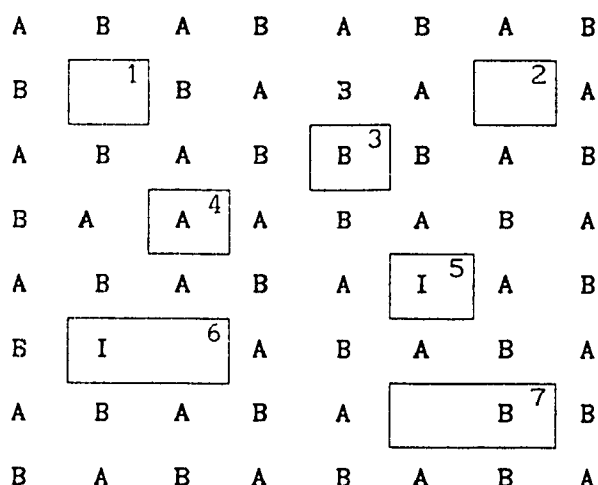


Figure 2.2 Point defects in a binary AB compound semiconductor

- 1) vacancy V_A 2) vacancy V_B 3) anti site B_A 4) anti site A_B
 5) substitutional impurity I_B 6) $I_A + V_B$ complex 7) $V_A + B_A$ complex.

2.2 Shallow and Deep Level States in Semiconductors

It has been mentioned above that defects in a crystal might give rise to localized energy states. Besides the imperfections of the crystal, lattice defects can be created voluntarily by adding foreign atoms to the host lattice (16). This will introduce electronic energy states into the forbidden gap of an SC. These are the so called *defect states* (17).

This section introduces two categories of defect state: the shallow level impurities and the deep level impurities. The deep level state will be studied extensively in a subsequent chapter.

2.2.1 Shallow levels

In general, shallow states are located near their related band edges: near the valence band (VB) for acceptor impurities and near the conduction band (CB) for donor impurities. In fact a shallow state is defined by kT greater than the ionization energy level E_i for a donor in an n-type SC. Here k is the Boltzmann constant and T is the absolute temperature. Thus at room temperature ($T=300K$), $kT=26meV$ where we have a shallow level if E_i is less than $26meV$. The ionization energy of shallow state can be described by the effective mass approximation theory (16)(17) or by the modified hydrogenic model that can be found in reference (18). Shallow impurities are widely used in SC technology for modifying the amount and type of electrical conductivity of an extrinsic SC material. This is the basis of device fabrication such as diodes, transistors and integrated circuits.

2.2.2 Deep levels

As opposed to shallow levels, deep levels states are located at considerable distances from a band edge: in this case kT should be less than the energy level E_i . It would require a higher energy for an electron to go from the deep level to the conduction band. Thus at room temperature we have a deep level for E_i greater than $26meV$. For GaAs references (19)(20) show a table giving the doping impurities that will cause shallow or deep levels in this material. For example, Si is an amphoteric impurity in GaAs, but it has been shown experimentally that Si would be a shallow donor in this material with an activation energy equal to $0.002eV$ (21). On the other hand chromium (Cr) is a deep acceptor in GaAs with an activation energy equal to $0.63eV$ (19).

3.0 GENERAL CONSIDERATIONS AND EXPERIMENTAL DESCRIPTIONS

OF SCHOTTKY BARRIERS

3.0.0 Introduction

This chapter is divided into three main sections. The first section deals with the capacitance of a Schottky barrier (SKB). The second section is involved in finding the characteristics of the SKB and the last one gives some practical considerations for SKB fabrication.

The capacitance of an SKB is of fundamental importance in the characterization of a GaAs sample for two reasons. The first reason is that the variation of the junction capacitance of an SKB with reverse bias voltage applied to the junction, usually denoted by $C(V)$, will allow one to find the shallow donor concentration N_D of an n-type GaAs SC sample under investigation.¹ The shallow donor concentration will be used in turn for the calculation of the deep level trap concentration. Furthermore, $C(V)$ might be used to calculate the barrier height V_b that gives some additional information on the quality of SKBs as it will be explained in the following. The second reason is that the junction capacitance of an SKB is used since the DLTS technique is based on the change in capacitance of the biased junction.

The characteristics of an SKB is determined by using the current as function of voltage measurements of the junction. This is denoted by $I(V)$. With this measurement method several information on the diode

¹ The shallow acceptor concentration N_A for an p-type SC can be found also, if the case may be.

can be found such as the barrier height ϕ_b , the ideality factor n , the reverse saturation current I_o , the series resistance R_s and the shunt resistance R_{sh} .

The knowledge of ϕ_b is required to determine if the DLTS measurements should be performed. As an example, the EL2 DLTS signal peak is strongly dependent on the SKB ϕ_b between 0.62eV to 0.82eV (22). For ϕ_b less than 0.62eV the DLTS measurements fail to show the EL2 signal. For ϕ_b greater than 0.82eV, the EL2 DLTS signal is measured with confidence since it is not altered anymore.

The ideality factor n indicates the current conduction mode of an SKB (23). n is usually between one and two. If n is close to one for low free carrier concentration, the current conduction mode is done by thermionic emission for which an SKB is in good condition for DLTS measurements.

The reverse saturation current I_o indicates the current of the diode under reverse bias before the breakdown voltage occurs. If the reverse current under reverse bias voltage is maintained fairly constant until breakdown occurs (i.e. no leakage current added), the diode can be used for DLTS experiments. The leakage current have an influence on ϕ_b thus it may affect the measurement of the trap concentration. Furthermore, R_s and R_{sh} may be found, indicating if they model practical diodes, since our diodes should have low values for series resistance R_s in order to prevent ohmic loss from the junction resistance and have large value for shunt resistance R_{sh} in order to prevent leakage current (24)(25).

Finally, the third section describes some practical considerations for an SKB fabrication. At first, ohmic contacts are

made on the SC and an evaporation of metal on the SC using Al-Pd metalization is described in order to obtained diodes with the best characterization as possible, as it was mentioned above.

3.1 Capacitance-Voltage Characteristics of a Schottky Barrier

For our experimental results, it is necessary to know the free carrier concentration N_D or N_A of an SC, and the barrier height V_b of the metal-semiconductor junction. In order to do so, it is required to know the capacitance of the junction under reverse bias voltage applied.

3.1.1 Space charge region of an SKB

An n-type Schottky barrier is a metal-semiconductor junction where the work function of the metal ϕ_m is greater than the work function of the SC ϕ_s ($\phi_m > \phi_s$). Its basic band diagram at equilibrium is shown in figure 3.1. The contact potential is represented by qV_i (eV) and the barrier height is represented by V_b (eV). The barrier height V_b is equal to the sum of qV_i and ϕ_n ($V_b = qV_i + \phi_n$) where ϕ_n is the difference between E_c and E_{fs} ($\phi_n = E_c - E_{fs}$) (26) where E_c is the energy level at the conduction band and E_{fs} is the Fermi level.

The width of the space charge region W with a voltage bias applied is given by (27)

$$W = \left(\frac{2\epsilon_s}{qN_D} [V_i - kT/q - V] \right)^{1/2} \quad (3.1)$$

where V_i is the contact potential, V is the external bias applied, ϵ_s

is the SC permittivity ², N_D is the shallow donor concentration³, k is the Boltzmann constant and T is the temperature in Kelvin. The derivation of the above equation is given in appendix II.

The width of the depletion region at zero bias (W_0) is obtained when V is equal to zero. For forward bias ($V = V_f$), W decreases below W_0 and for a reverse bias ($V = V_r$), W increases above W_0 .

By the known relation $C=dQ/dV$ where C is the capacitance, Q the charge density and V the voltage, and equation 3.1, the junction capacitance is found as (27)(28)

$$C_j = \frac{\epsilon_s S}{W} = S \left[\frac{q \epsilon_s}{2[V_i - (kT/q) - V]} N_D \right]^{1/2} \quad (3.2)$$

where S is the surface area of the junction and the other parameters have the same meaning as before.⁴

It is clear here that the reverse bias condition forms a parallel plate capacitor comprising a layer of dielectric thickness W and dielectric constant ϵ_s between two conducting electrodes (28).

The capacitance of equation 3.2 can easily be measured as:

² $\epsilon_s = \epsilon \epsilon_0$ where $\epsilon = 13.2$ for GaAs and $\epsilon_0 = 8.854 \times 10^{-14}$ F/cm.

³ Actually the free carrier concentration for an n-type GaAs sample is given by N_D since $N_D \gg N_A$.

⁴ The derivation of equation 3.2 is given in appendix II

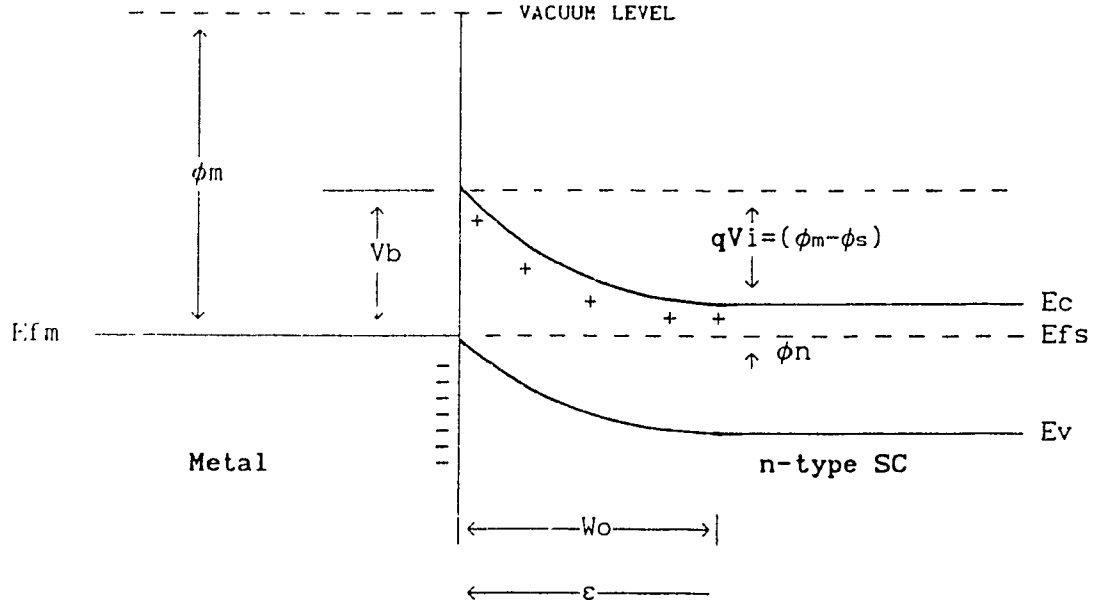


Fig. 3.1 Band diagram for the junction at equilibrium ($\phi_m > \phi_s$).
n-type metal-semiconductor junction.

function of the reverse bias $V = -V_r$. This equation can be rewritten as (27) (29)

$$\frac{1}{C^2} = \frac{1}{S^2} \frac{2(V_i - kT/q - V)}{q\epsilon_s N_D} \quad (3.3)$$

and the plot of $1/C^2$ as function of V is a straight line whose slope and intercept can be used to determine the doping concentration N_D and the barrier height V_b . In fact, equation 3.3 takes the form of a straight line $y = ax + b$ where y is $1/C^2$, x is V , a is the slope and b is the intercept with the y axis. Thus taking the slope of equation 3.3 we get

$$-\frac{d(1/C^2)}{dV} = \frac{1}{S^2} \frac{2}{q\epsilon_s N_D} \quad (3.4)$$

where the doping concentration is found as

$$N_D = \frac{1}{S^2} \frac{2}{q\epsilon_s} \left[\frac{-1}{d(1/C^2)/dV} \right] \quad (3.5)$$

The intercept of the straight line (equation 3.3) with the voltage axis gives the barrier height V_b (30).

Figure 3.2 shows typical $C(V)$ and $1/C(V)^2$ plots. Figure 3.2a is drawn from equation 3.2 and figure 3.2b from equation 3.3. From figure 3.2b, if the doping concentration N_D is not uniform in the SC, the plot $1/C^2$ will not be linear. Therefore, one has to choose two points P1 and P2 for the best linear fit. The slope of linear fits (i.e. N_D 's) may be different for points P1 to P2 and P2 to P3. It happens in some experimental cases that the concentration N_D is slightly different for different reverse bias voltage applied (i.e. to points P1, P2 and P2, P3).

The best linear fit to points P1 to P2 or P2 to P3 can be found by the least square method (31).

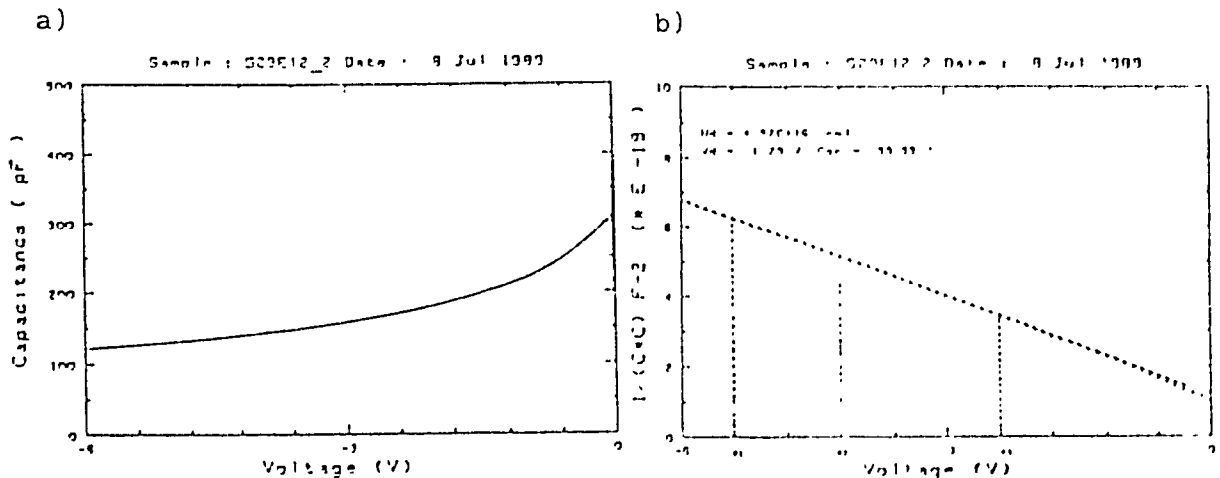


Fig. 3.2 Typical $C(V)$ and $1/C(V)^2$ plots

3.1.2 Experimental Considerations

In practice, to find N_D and V_b , we use a computer HP 300, a programmable multimeter HP 3455A, and a programmable capacitance-meter HP 4280A. The sample is inserted on the tip tail inside the cryostat so that the measurements are being performed under vacuum. This way, measurements are made under insulated conditions. The simplified flow chart of the computer program used to measure the capacitance $C(V)$ of Schottky barriers is shown in figure 3.3 (32). At the beginning, the computer reads from the operator the voltage range to be measured. Then, the capacitance meter (C-meter) performs the capacitance measurement for the range of voltage chosen and stores the values in its own buffer. Then the capacitance meter transfers the data to the computer upon request. Afterwards, the operator may choose to plot $C(V)$ measured as shown in figure 3.2a, or may choose to plot $1/C^2$ shown in figure 3.2b.

The operator chooses two points P_1 and P_2 ; the program does the linear fit in this range of points chosen in order to find a and b (from the line $y=ax+b$) from the least square method (31). Thus a is the slope $d(1/C^2)/dV$ which is substituted in equation 3.5 in order to get N_D . Finally V_b is found by the intersection of the straight line with the voltage axis (i.e. when $y=0$). Thus V_b is given as $-b/a$.

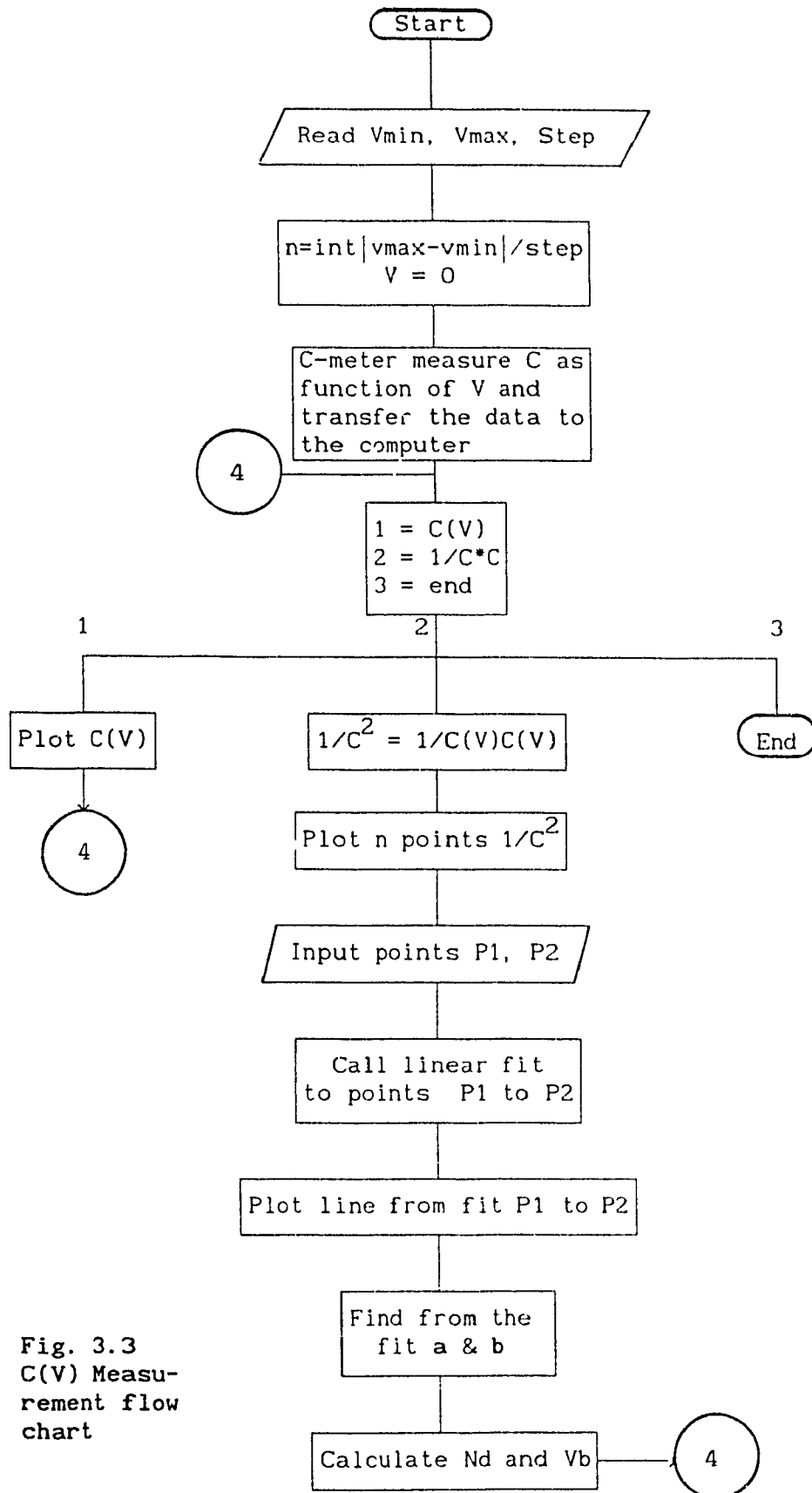


Fig. 3.3
C(V) Measu-
rement flow
chart

3.2 Current-Voltage Characteristics of a Schottky Barrier

Another interesting way to find the barrier height⁵ ϕ_b is to use the $I(V)$ characteristics of a Schottky barrier. Moreover, the measurement of I as function of V will allow us to find the characteristics of a non ideal diode such as the series resistance, the shunt resistance, the saturation current and the ideality factor.

3.2.1 Current Characteristic

The current of a practical metal-semiconductor diode made on high mobility semiconductor such GaAs is mainly due to thermionic emission of electrons over the barrier (23)(30) and the current I as function of the applied bias V is given by the relation

$$I = I_0 \left[e^{qV/nkT} - 1 \right] \quad (3.6)$$

where n is the diode ideality factor and I_0 is the reverse saturation current. For an *ideal* Schottky barrier with the doping concentration ranging from 10^{15} to 10^{17} cm^{-3} , the ideality factor n equals unity and the current flows only due to thermionic emission (23). For this case I_0 is written as

$$I_0 = SA^* T^2 e^{(-\phi_b/kT)} \quad (3.7)$$

⁵ When we use the $I(V)$ measurement method, we will use ϕ_b instead of V_b (in $C(V)$ measurement) in order to differentiate the barrier height found by one method or the other.

where ϕ_b is the barrier height (eV) and A^* is the effective Richardson constant of the semiconductor given by $7.8 Acm^{-2}K^{-2}$ for GaAs (37)(38). The other values have their usual meaning.

The barrier height ϕ_b in equation 3.7 may not be negligible and is dependent on the bias applied and the shallow donor concentration N_D . This is due to the effect of the image force barrier lowering. The image force barrier lowering known as the Schottky effect can be understood by referring to appendix V. The barrier height is therefore lowered by an amount (39)(40)

$$\Delta\phi_b = \left[\frac{q^3 N_D}{8\pi^2 \epsilon_s^3} (V_i - V) \right]^{1/4} \quad (3.8)$$

where ϵ_s is the permittivity of the SC and V is the applied voltage. The other values have their usual meaning.

3.2.2 Practical methods to find R_s , R_{sh} , n , I_o and ϕ_b

Here we describe a practical and convenient method to find R_s , R_{sh} , n , and I_o . To start off with, the theoretical equation 3.6 can be rewritten as (41)

$$I = I_o e^{(qV/nkT)} (1 - e^{-qV/nkT}) \quad (3.9)$$

For the case of a non-ideal Schottky barrier, the series resistance R_s from ohmic loss due to the junction resistance and the shunt resistance from the leakage currents are added to the ideal case of equation 3.6 (25). Thus equation 3.6 becomes

$$I = \left[I_o \left(e^{(q/nkT)(V-IR_s)} - 1 \right) + \frac{V}{R_{sh}} \right] \quad (3.10)$$

where the equivalent circuit is shown in figure 3.4. For this circuit, the current I from equation 3.10 is equal to I_{mes} (the current flowing out of the non-ideal diode). Then V is equal to V_{theo} the voltage of the ideal diode and $(V-IR_s)$ is the measured voltage V_{mes} at the non-ideal diode terminals. The current flowing out of the ideal diode is I_{theo} . Thus it can be seen that the measured values I_{mes} and V_{mes} are related with the junction values I_{theo} and V_{theo} by the following expressions (41)

$$I_{mes} = I_{theo} + G_{sh} * V_{theo} \quad (3.11a)$$

$$V_{mes} = V_{theo} + R_s * I_{mes} \quad (3.11b)$$

Thus equations 3.9 and 3.11 can be used to determine I_o , n , R_s and R_{sh} .

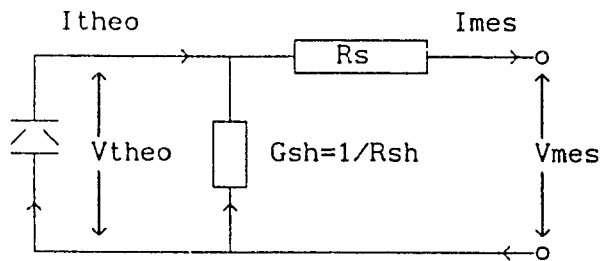


Fig. 3.4 Equivalent circuit of a non-ideal diode

The values of n and I_o can be determined accurately from the regression linear line (41). Equation 3.9 is written as

$$\ln \left[\frac{I}{(1 - e^{-qV/nkT})} \right] = \ln(I_o) + qV/nkT \quad (3.12)$$

This equation takes the form as $y = ax + b$, where $x = V$ and $y = \ln(I)$ for $V > 3kT$ (42). This equation is a straight line with slope a (i.e. a is obtained by differentiating the voltage V with respect to $\ln(I)$ in equation 3.12) and with b the intercept with the y axis when $V = 0$ corresponding to the ideal diode equation.

In practice, the I-V characteristics of a practical Schottky diode is measured as shown in figure 3.5a. Then the natural logarithm of the measured current is taken as function of the measured voltage. The linear part of the I-V characteristics measured as shown in figure 3.5b correspond to the theoretical diode given by equation 3.9. Thus two points P1 and P2 are chosen from that linear part and the best linear fit is performed in order to find the values of a and b from the line $y = ax + b$ (31).

By comparing a and b with equation 3.12, we find I_0 and n directly as (41)(42)

$$I_0 = e^b \quad (3.13a)$$

and

$$n = q/(akT) \quad (3.13b)$$

As shown in figure 3.5b, the non linear parts are the series resistance R_s and the shunt resistance R_{sh} . In order to find R_s , we take the maximum measured current I and we substitute it in equation 3.11b in order to get

$$R_s = \frac{V_{mes} - V_{theo}}{I_{mes}} = \frac{V_{mes} - \{(\ln(I_{mes}) - b)/a\}}{I_{mes}} \quad (3.14)$$

where V_{theo} is obtained from a , b and $\ln(I_{mes})$.

In a similar way R_{sh} is found using equation 3.11a. Therefore,

$$R_{sh} = \frac{V_{mes}}{I_{mes} - 10^{(a V_{mes} + b)}} \quad (3.15)$$

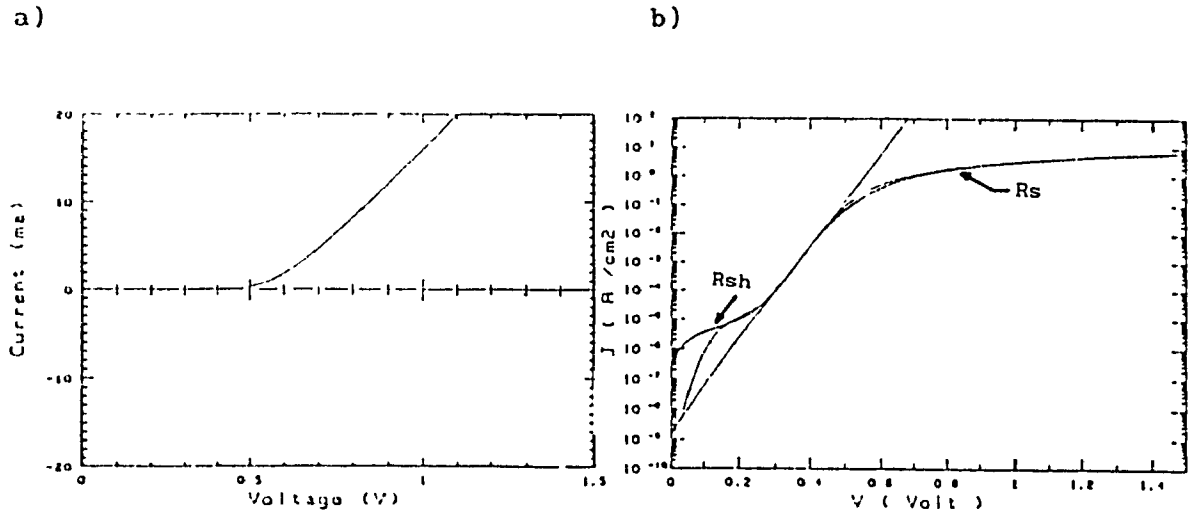


Fig. 3.5 a) Measured I-V characteristic b) $\ln(I)$ vs V

3.2.3 Experimental considerations

In order to get the experimental results for n , I_0 , R_s and R_{sh} , we use the computer HP, a programmable multimeter as described before, a generator HP S116A and a scanner Keithley 706. The simplified flow chart of the computer program is shown in figure 3.6 (32). The sample is placed inside the cryostat as before. This time there is a set of resistors, chosen by the scanner, placed in series with the diode, and the voltage V across R selected by the scanner is read. The current flowing through the diode is simply $I = V/R$. This is repeated up to the required values of N found from V_{min} and V_{max} . During this

process the value of I and V are recorded in an array and the plot is performed at the same time.

Then, the plot $\ln(I)$ vs V is performed. Two points P_1 and P_2 are chosen in the linear part of the plot in order to get the values of a and b from the regression line. Finally, the values of n and I_0 are found using equations 3.13, ϕ_b is then found using equation 3.7 and R_s and R_{sh} are found by equations 3.14 and 3.15 respectively.

3.2.4 Comparison of the barrier height ϕ_b between $C(V)$ and $I(V)$ measurements

So far we discussed two ways to find the barrier height ϕ_b : one with the $C(V)$ measurement and the other with the $I(V)$ measurement. In the first case, the barrier height is measured by a method which does not require movement of the electron over the barrier, therefore, the value of ϕ_b is not altered by the image force lowering. In the case of the $I(V)$ measurement, the electron is moved over the barrier that makes ϕ_b lowered by the image force (39). Therefore, the barrier heights obtained by the $C(V)$ method are larger than those obtained from the $I(V)$ measurement (43).

It is observe that in many cases the barrier height from the $I(V)$ measurement could be close to the one from the $C(V)$ measurement if the former is multiplied by the ideality factor n (43). We will discuss the experimental differences between ϕ_b and V_b in section 5.4.3.

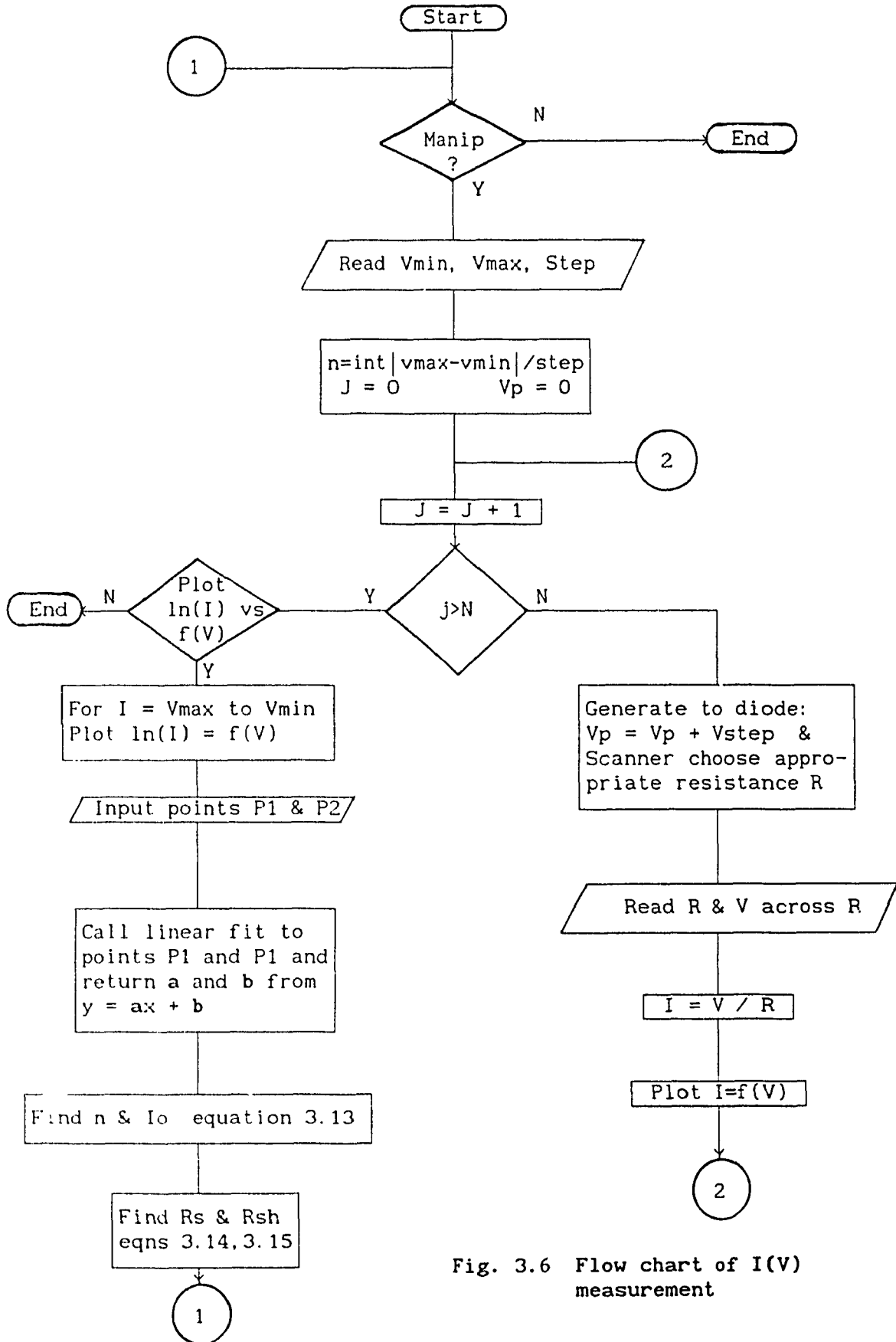


Fig. 3.6 Flow chart of I(V) measurement

3.3 Practical Consideration for Schottky Barrier Fabrication

The process used to make a Schottky barrier with a good ideality factor n is described here. Appendix X gives the steps for the fabrication of a Schottky diode and the section below explains the reasons for obtaining good diodes.

3.3.1 Practical considerations for ohmic contacts

As stated before, for low doping concentration ($N_D < 10^{17} \text{ cm}^{-3}$), the current over the barrier is mainly due to thermionic emission. In this case the junction resistance is independent of doping and is minimized for low barrier height.

For contact with high doping concentration ($N_D > 10^{17} \text{ cm}^{-3}$), the tunneling process dominates and the junction resistance depends largely on it. Thus for high doping concentration, low barrier height must be used to obtain low values of junction resistance (44).

The methods used to make ohmic contacts is described in appendix X. For our experimental purpose, we evaporated small area of indium on our GaAs samples. Then the contacts were made by alloying at the corresponding eutectic temperature (500°C) into the SC under hydrogen for two minutes (44). The ohmic contacts are then verified with the curve tracer.

3.3.2 Practical considerations for metal-semiconductor junction

According to the theory described in section 3.2.1, an ideal diode has an ideality factor n equals to one. But in practice, when such a diode is fabricated, this ideality factor n may be greater than one due to the image force lowering of the barrier and due to the presence of a

thin insulating interface layer (23).

For the case where $\Delta\phi_b$ is negligible, the ideality factor n of the diode may depend on the surface quality of the diode before a metallic evaporation is being performed on the GaAs sample. Therefore, maximum care is taken during the diode fabrication in order to get the surface of the sample as clean as possible.

In order to obtain Schottky diodes with n as close to one (typically; $1 < n < 1.1$), it is necessary to obtain interfaces electrically and thermally stable. This can be done by using the Al-Pd metalization system because of the weak reaction with GaAs (45).

In this process, the sample is cleaned using classical degreasing in trichloroethane, acetone and methanol, and dipped in hydrofluoridric acid (HF) in order to remove any oxides on its surface (45) if the case may be. Then the palladium (Pd) is deposited on the sample where circular areas of 0.8 mm of diameter have been defined with a photo lithographic process using negative photo resist. This deposition is obtained by dipping the sample into an activator solution containing hydrofluoridric acid, acetic acid and PdCl_2 involving the reduction of Pd^+ ions to metallic Pd by galvanic displacement.

Furthermore, before the sample is dipped into the activator, the sample is immersed into pure hydrochloric acid (HCl) in order to remove the oxides left on its surface. Then it is dipped into deionized water in order to remove the acids from the surface so it does not interfere with the solution.

Finally, an aluminum (Al) evaporation is performed under 10^{-6} Torr (or 1.33×10^{-4} Pa) vacuum in order to make a good contact between both Pd and Al. With the ohmic contacts and the Al-Pd deposited on the GaAs

samples, the Schottky barriers are verified with the curve tracer first. Then they are characterized with $C(V)$ and $I(V)$ measurements as described in previous sections.

4.0 CHARACTERIZATION OF DEEP LEVELS AND EXPERIMENTAL DESCRIPTIONS

4.0.0 Introduction

The aim of this chapter is to describe the experimental methods to find the apparent activation energy E_a and the total trap concentration N_t from deep level centers referred to as trap that can be present in semiconductor materials. In order to describe how to find these two parameters, we take the general case for an n-type SC containing only shallow donors and simple monovalent deep donors as an example, as it is described in references (16) and (46).

The shallow donor concentration N_D can easily be found with the C(V) measurement method as described in the previous chapter with the use of a Schottky barrier (SKB). In this chapter we still use an SKB as a test device, but this time by taking deep levels into account.

The SKB is initially under reverse bias where all shallow and deep levels above the Fermi-level are ionized. This corresponds to a junction capacitance C_0 . At this initial condition, we have the total trap concentration N_t and the shallow donors ionized. When an electrical pulse is applied to the SKB (decreasing the depletion layer width) which is still under reverse bias, there will be less deep levels ionized above the Fermi level; that is there will be a fraction of the total trap concentration N_t at time t that will be occupied by electrons. This is denoted by $n_r(t)$. For this case, the traps capture electrons from the conduction band since the capture rate dominates while the shallow donors remain ionized. The amount of the trap that will not be occupied by electrons at time t will be denoted

by $\{N_t - n_t(t)\}$.

When the pulse has elapsed, the initial reverse bias condition tends to take place (i.e. the depletion layer width increases to its original width). Since there are now electrons trapped, and the system tends to reach the equilibrium, the electrons will be remitted back to the conduction band since the emission rate dominates. As it will be seen in details in this chapter, the emission rate is temperature dependent and it has an effect on the variation of $n_t(t)$. Therefore, by the variation of $n_t(t)$, a corresponding capacitance transient $C(t)$ can be measured experimentally. The values of $C(t)$ is thus normalized to $\Delta C/C_0$ as it will be shown later on.

Experimentally, we measure the capacitance transients at instants t_1 and t_2 with a scan in temperature ranging from about 80K to 400K. Then we take the maximum peak height at a temperature T_M to determine the total trap concentration N_t , and then we vary times t_1 and t_2 in order to get different values of T_M . The latter will allow to find F_a . Before going further, in section 4.1 we give some general definitions on capture rate and emission rate in order to apply it to SKBs in section 4.2.

4.1 Some General Definitions

4.1.1 General equation of occupation of a defect state

In this subsection, we show the electronic transition between the conduction band E_c , the valence band E_v and a deep level trap E_t . The general rate equations governing the occupation of a defect state of total trap concentration N_t (17) are given by

$$\frac{dn_T(t)}{dt} = K_n \{N_T - n_T(t)\} - e_n n_T(t) - K_p n_T(t) + e_p \{N_T - n_T(t)\} \quad (4.1)$$

where $n_T(t)$ is the concentration of defects occupied by electrons at time t , $\{N_T - n_T(t)\}$ is the concentration of defects that are not occupied by electrons at time t , e_n is the emission rate for electrons, e_p is the emission rate for holes and K_n and K_p are the probabilities per unit time that a defect captures an electron and a hole respectively. Figure 4.1 shows the diagram of the electronic transition between the bands and level E_T at thermal equilibrium (47)(48). The single level generation and recombination through traps

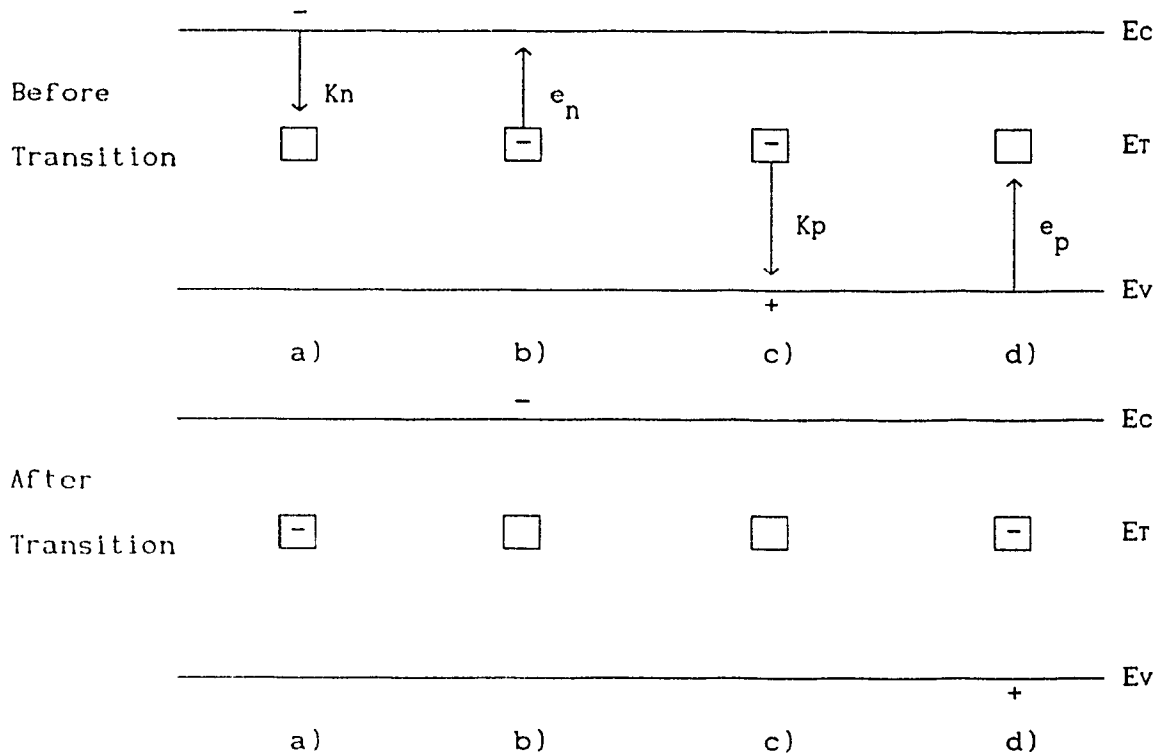


Fig. 4.1 The basic process of carrier generation and recombination through traps a) electron capture, b) electron emission, c) hole capture, d) hole emission.

can be described by four processes as shown in the figure. Those are a) the electron capture, b) the electron emission, c) the hole capture, and d) the hole emission. The direction of the arrow indicates the direction of the transition.

In general, for a given deep center it is assumed that (16)(17) one of the emission rate has to be much larger than the other. Thus deep level centers are classified as *electron traps* when $K_n \gg K_p$ by the condition $e_n \gg e_p$ and a *hole trap* when $K_p \gg K_n$ by the condition $e_p \gg e_n$ (49)(50). Note that an electron trap is a majority carrier trap in n-type material and a minority carrier trap in p-type material.

4.1.2 General definition of capture rate of free carriers

A deep defect has a specific capture cross section σ_n and σ_p for capturing electrons and holes respectively. For example, for a deep defect, σ_n describes (50)



and σ_p describes



where Nd^+ is an ionized donor, Nd is a neutral donor, Na^- is an ionized acceptor, Na is a neutral acceptor, $(e)_{CB}^-$ is an electron from the conduction band and $(h)_{VB}^+$ is a hole from the valence band.

The capture rate K_n of a flaw for an electron trap is given by the probability per unit time that a defect captures an electron from the

conduction band proportional to the concentration n of electrons¹ in the band (17)(51), thus

$$K_n = C_n n \quad (4.3)$$

where C_n (cm³/s) is the coefficient captures of electrons and is given by

$$C_n = \sigma_n \langle V_{thn} \rangle \quad (4.4)$$

where $\langle V_{thn} \rangle$ is the average thermal velocity of electrons which is given by (51)

$$\langle V_{thn} \rangle = \{3kT/m_n^*\}^{1/2} \quad (4.5)$$

where m_n^* is the electron mass effective, k is the Boltzmann constant and T is the temperature. Note that for an electron trap, the capture rate from the conduction band to the defect occurs according to the following relationships;

$$\frac{dn_T(t)}{dt} = K_n n_T(t) \quad (4.6)$$

where $dn_T(t)/dt$ is the rate of change of the concentration of flaws occupied by electrons, for capturing electrons.

¹ Replace n by p in all equations and "electron" by "hole" for a hole trap.

4.1.3 Definition of emission rate of a carrier trapped

For the case of an electron trap, the carrier emission from the defect to the conduction band occurs with the probability per unit time e_n (sec^{-1}). Thus, the rate of change in the concentration of defects occupied by electrons with respect to time for emitting electrons from the trap level to the conduction band is given by (17)(52)

$$\frac{dn_T(t)}{dt} = -e_n n_T(t) \quad (4.7)$$

4.1.4 Emission rate at thermal equilibrium

An electron trap exchanges carriers with the conduction band and a hole trap exchanges carriers with the valence band. For the case of an electron trap, equation 4.1 can be rewritten as (17)(52)

$$\frac{dn_T(t)}{dt} = nC_n\{N_T - n_T(t)\} - e_n n_T(t) \quad (4.8)$$

From equation 4.8, assuming steady state we obtain the emission rate at thermal equilibrium as

$$e_n = 1/\tau_n = N_c \sigma_n \langle V_{thn} \rangle g_n^* e^{-(E_d/kT)} \quad (4.9)$$

where E_d is the Gibbs free energy of transition, g_n^* is the degeneracy factor² and N_c is the effective density of state. The determination

² $g_n^* = g_e/g_f$ for a nondegenerated condition; g_e and g_f are statistical weights of the flaw electronic configuration when "empty" and "filled" with the electron.

of equation 4.9 is given in appendix IV where N_c is given.

For most SC, the quantity E_b is expected to be temperature dependent (53). Thus, the information relative to a transition may appear in terms of enthalpy (ΔH_n) and entropy (ΔS_n) of the transition rather than expression E_b directly. Thus the relation for the three thermodynamic functions are related by (53)(54)

$$\Delta H_n = E_b + T\Delta S_n \quad (4.10)$$

where T is the temperature. Equation 4.9 can thus be rewritten as

$$e_n = N_c \sigma_n \langle V_{thn} \rangle g_n^* \left[e^{\Delta S_n/k} \right] \left[e^{-\Delta H_n/kT} \right] \quad (4.11a)$$

or

$$e_n = T^2 \sigma_n \alpha \beta X_n e^{-\Delta H_n/kT} \quad (4.11b)$$

where α includes the constant terms in the density of states ($N_c = \alpha T^{3/2}$), β includes the constant terms in the average thermal velocity ($\langle V_{thn} \rangle = \beta T^{1/2}$) and X_n includes the entropy and the degeneracy factor ($X_n = g_n e^{\Delta S_n/k}$).

Experimentally the thermal activation energy ΔH_n can be determined approximately from equation 4.11b as

$$T^2/e_n \approx A e^{\Delta H_n/kT} \quad (4.12)$$

by taking a plot of $\log(T^2/e_n)$ as function of $(1/T)$ where $A = (\sigma_n \alpha \beta X_n)^{-1}$

(In section 4.2.5, we will give the procedure for finding the activation energy).

Now, since E_D varies non linearly with the temperature, as shown in reference (54), and if this non linearity may be small enough, the emission probability can be rewritten as

$$e_n \approx CT^2 e^{-E_a/kT} \quad (4.13)$$

over a reasonably broad temperature range of measurement, where $C=(\sigma_n \alpha \beta X_m)$ and E_a is the apparent (or effective) thermal energy³. Thus E_a indicates a value for ΔH_n for somewhere near the center of that measured range. Thus when E_D declines in a non linear way with rising temperature, any value deduced for E_a will tend to exceed E_D of any temperature. Therefore, it is assumed that the emission probability can be approximated for low temperature variation in E_D as

$$e_n = 1/\tau_n \approx N_c \sigma_n \langle V_{thn} \rangle g_n^{\bullet} e^{-(E_a/kT)} \quad (4.14)$$

meaning that the experimental measurement for the apparent activation energy E_a will be somewhat a bit higher than E_D .

Similarly, for a hole trap we obtain;

$$e_p = 1/\tau_p \approx N_v \sigma_p \langle V_{thp} \rangle (g_p^{\bullet})^{-1} e^{(-E_a/kT)} \quad (4.15)$$

³ We have written E_a instead E_{eff} for convenience.

4.2 Schottky Barrier Taking Deep Levels Into Account

This section considers the equations of a Schottky barrier taking deep level traps into account as shown in figure 4.2. Those equations will allow the determination of the transition region λ and the variation in capacitance $\Delta C/C_0$ (capacitance transients) from the variation of the trap concentration $n_T(t)$ occupied by electrons. From the capacitance transient the DLTS technique will then be applied in order to find E_a and N_T experimentally in the next section.

4.2.1 Determination of the transition region

Let us consider an n-type Schottky barrier under reverse bias by a voltage qV with a shallow donor N_D , and a deep level located at $(E_c - E_T)$ within the band gap with total trap concentration N_T . This is shown in figure 4.2a. Furthermore, we consider the charge distribution $\rho(x)$ constant assuming that N_D and N_T are completely ionized above the Fermi level and the semiconductor is uniformly doped (55). The charge distribution is shown in figure 4.2b. The transition region λ can be found by solving Poisson's equation

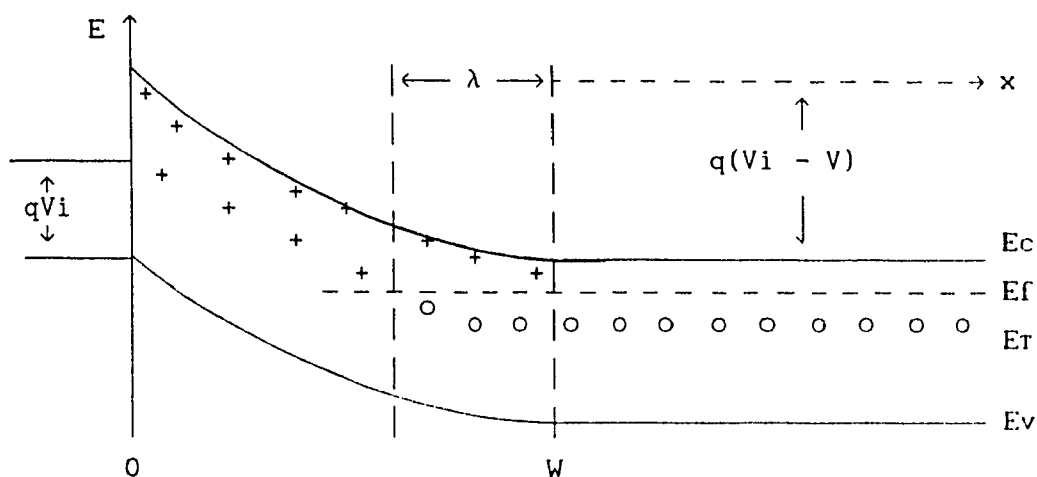
$$\frac{d^2V}{dx^2} = -\frac{q}{\epsilon_s}[N_D] \quad (4.16)$$

where q is the charge of an electron, ϵ_s is the SC permittivity, N_D is the shallow donor concentration, and where λ is defined in the space charge region as shown in figure 4.2. Thus, solving the above equation from x equals $(W - \lambda)$ to W we find λ (56) given as⁴

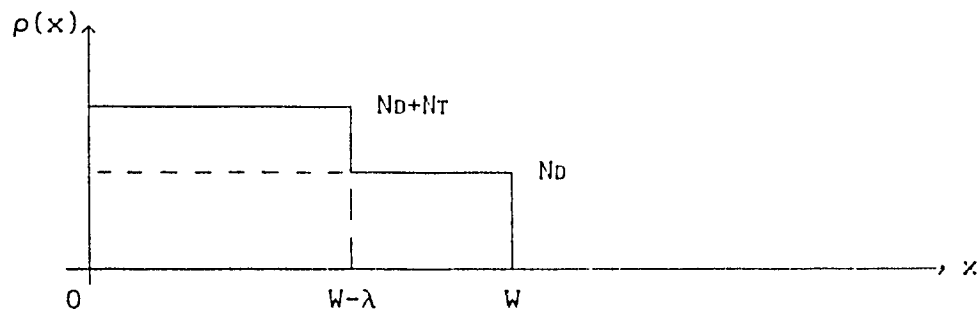
⁴ The derivation of the transition region is derived in appendix V.

$$\lambda = \left[\frac{2\epsilon_s}{q^2 N_D} (E_F - E_T) \right]^{1/2} \quad (4.17)$$

The value of E_F can be calculated from $n_0 = n_i e^{(E_F - E_i)/kT}$ where for the SC material used, n_i is the intrinsic carrier concentration, E_i is the intrinsic Fermi level and n_0 is the shallow donor concentration ($n_0 = N_D$) (57). The apparent activation energy ($E_a \approx E_r$) is determined experimentally. Therefore, knowing N_D which is determined from $C(V)$ measurement and E_a , λ can easily be found.



a) Diagram of a Schottky barrier with a deep level



b) Charge distribution

Fig. 4.2 Schottky barrier under reverse bias

4.2.2 Determination of the capacitance variation

Here we take the general case for an n-type SC containing shallow donors and simple monovalent deep donors as an example in order to find the variation in capacitance $\Delta C/C_0$. Initially, the Schottky barrier is under a constant reverse bias V_0 which is considered as the equilibrium case before time t_{-1} as shown in figure 4.3a. After time t_{-1} , a positive pulse from V_0 to V_1 is applied, where V_0 and V_1 are both negative values since the operation is performed under reverse bias. The pulse has a duration $\Delta t = t_0 - t_{-1}$ (sec.).

At V_0 we consider that the trap is empty from 0 to $(W_0 - \lambda_0)$ as shown by (+'s) in figure 4.4a since the monovalent deep donor trap is ionized as indicated in the figure, as well as the shallow one. The voltage pulse V_1 causes the filling of the trap with electrons from $(W_0 - \lambda_0)$ to $(W_1 - \lambda_1)$ as shown by (o's) in figure 4.4b since the capture rate K_n dominates. Therefore, electrons from the conduction band has been captured by the trap. Thus, solving the differential equation 4.6 from t_{-1} to t_0 (figure 4.3) we obtain the equation of the filling of the defect (capture of electrons) as

$$nT_i(t) = NT_i e^{K_n \Delta t} \quad (4.18)$$

At t_0 , the trap begins to empty according to the law of equation 4.7. Thus solving equation 4.7 from t_0 to t_∞ where t_∞ correspond to enough time so that the trap is completely empty (that is return to V_0), we obtain the equation of the emptying of the defect (emission of electrons back to the conduction band) as

$$nT_e(t) = NT(1 - e^{-t/\tau_n}) \quad (4.19)$$

Thus the variation of charges $nT_e(t)$ corresponds to an increasing value of capacitance $C(t)$ as shown in figure 4.3b. Note that the emptying of the trap defect is done by thermal relaxation (since τ_n is temperature dependent) and it takes much longer time to empty than filling by an electric pulse.

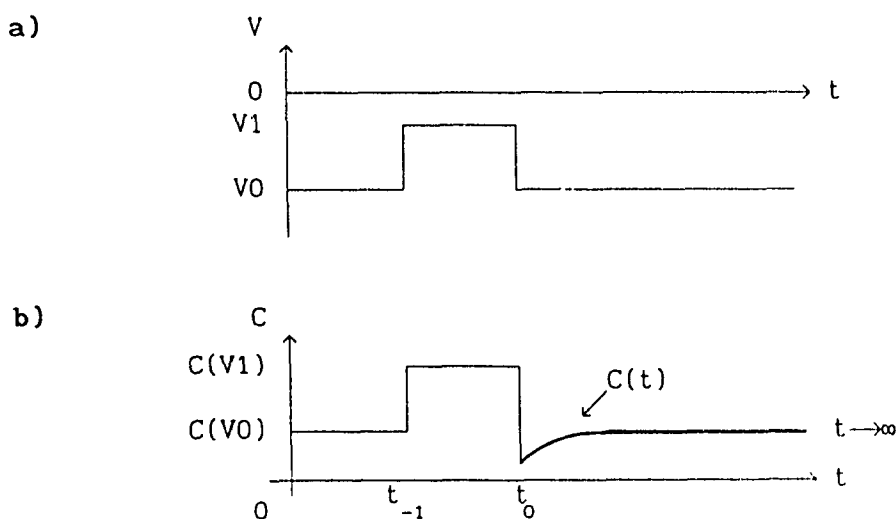


Fig. 4.3 a) Voltage pulse applied to a Schottky barrier
b) Corresponding change in capacitance

The variation in capacitance $C(t)$ is normalized to $\Delta C/C_0$ and is found by solving Poisson's equation with the limits shown in figure 4.4c where $\Delta C = (C(t) - C_0)$ and C_0 correspond to $C(V_0)$ shown in figure 4.3b (58). Thus we have

$$V(t) = \int_0^{W_0} x \frac{q}{\epsilon_s} N_D dx + \int_0^{W_1 - \lambda_1} x \frac{q}{\epsilon_s} NT dx + \int_{W_1 - \lambda_1}^{W_0 - \lambda_0} x \frac{q}{\epsilon_s} NT(1 - e^{-t/\tau_n}) dx \quad (4.20)$$

Space charge region and charge distribution of a Schottky barrier under reverse bias; $\circ \rightarrow$ filled trap with an electron and $+\rightarrow$ empty trap. a) At V_0 , b) At V_1 c) Charge distribution.

By solving the above equation we obtain the required result of $\Delta C/C_0$ which is given by (58)

$$\frac{\Delta C}{C_0} = \frac{C - C_0}{C_0} = \frac{N_T}{2N_D} \frac{\{(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (4.21)$$

which is the normalized variation of the capacitance between $(W_1 - \lambda_1)$ and $(W_0 - \lambda_0)$ due to trap defect when a bias pulse is applied to the Schottky barrier under reverse bias⁵. The above equation can be simplified further since $\lambda_{0,1}$ are small to as compare to $W_{0,1}$. Thus if N_D is uniformly distributed, $\lambda_0 = \lambda_1 = \lambda$ we have (56)

$$\frac{\Delta C}{C_0} = \frac{N_T}{2N_D} \frac{\{(W_0 - \lambda)^2 - (W_1 - \lambda)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (4.22)$$

4.2.3 Capacitive measurement method

The principle on capacitive measurement method starts off with a system in equilibrium; that is a Schottky barrier under reverse bias at V_0 corresponding to C_0 . A series of electric pulses applied to the Schottky barrier (external disturbances) will cause the system to be out of equilibrium during the pulse Δt as it can be seen in figure 4.5a. After each electrical pulse, transients in capacitance occur as shown in figure 4.5b. The shape of these transients will change with a constant increase in temperature (figure 4.5c) if a deep defect is present in the SC material since the emission rate e_n is temperature dependent. These transients are thus measured experimentally

⁵ The derivation of equation 4.22 is given in appendix VI.

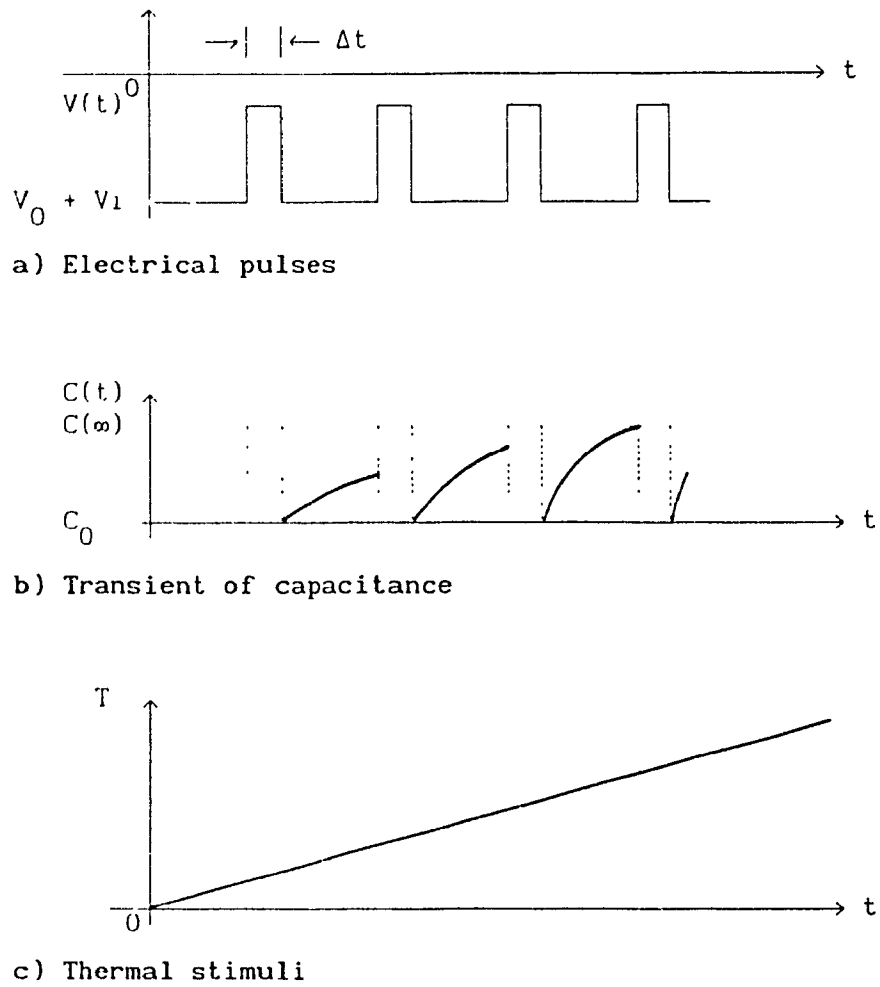


Fig. 4.5 Experimental sequence for capacitance measurements

4.2.4 DLTS method analysis

The DLTS method introduced by D. V. Lang in 1974 (6) consists in measuring the difference in capacitance transients of figure 4.5b at times t_1 and t_2 as it is shown on the left hand side of figure 4.6. The difference in capacitance transients is given by (50) the function

$$S(T) = C(t_2) - C(t_1) \quad (4.23)$$

where $S(T)$ is the plot of $C(t_2) - C(t_1)$ as function of the temperature T

as shown on the right hand side of figure 4.6. The normalized value $S(T)/C_0$ can easily be calculated by substituting equation 4.22 into 4.23 in order to get (60)

$$\frac{S(T)}{C_0} = \frac{C(t_2) - C(t_1)}{C_0} = \left[\frac{N_T}{2N_D} \frac{\{(W_0 - \lambda)^2 - (W_1 - \lambda)^2\}}{W_0^2} \right] (e^{-t_1/\tau_n} - e^{-t_2/\tau_n}) \quad (4.24)$$

By fixing times t_1 and t_2 we obtain a window constant in time (6), and if the temperature increase linearly with time, for a given defect, equation 4.24 will give rise to a DLTS peak where the maximum is located at a temperature T_M as shown in figure 4.6.

In order to find T_M , one has to differentiate equation 4.24 with respect to the temperature (taking equation 4.13 into account) and equate it to zero so we obtain the rate window $\tau_n = 1/e_n$ as (6)(60)⁶

$$\tau_n = \frac{t_2 - t_1}{\ln(t_2/t_1)} \quad (4.25)$$

By varying times t_1 and t_2 , the rate window τ_n will change accordingly, thus shifting the DLTS peak on the temperature axis as suggested by equation 4.24. The shift in the DLTS peak will allow the determination of the effective activation energy.

4.2.5 Arrhenius plot

When a deep level trap is characterized by its energy level E_a and its capture cross section σ_n , we may say that we have its signature

⁶This equation is derived in appendix VII

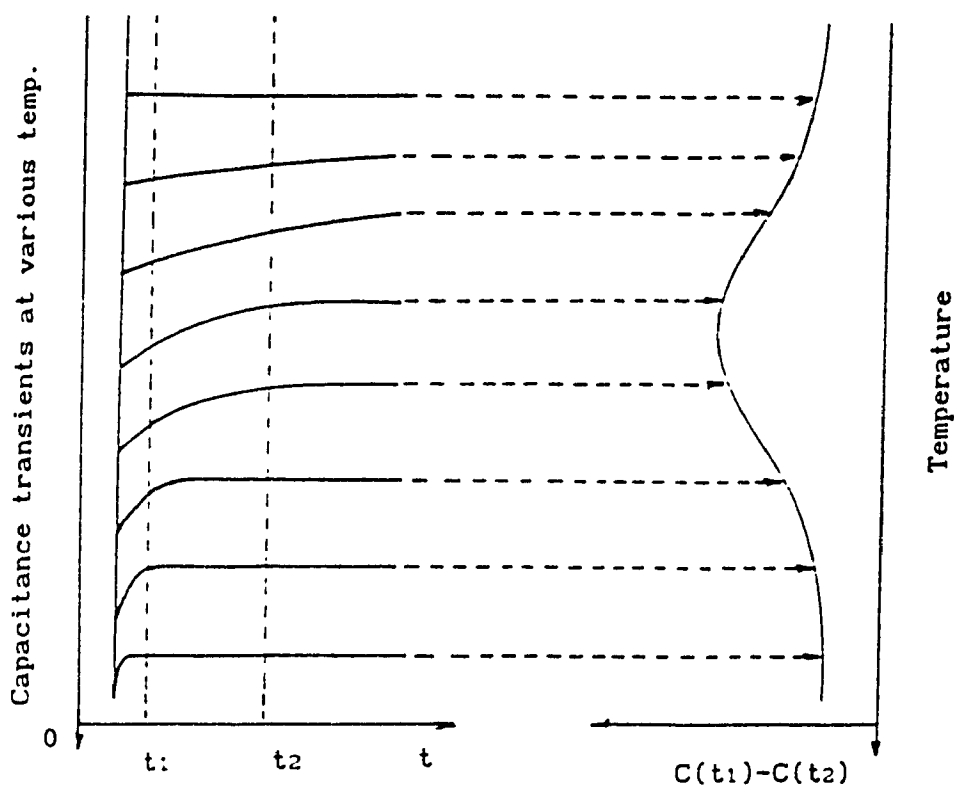


Fig. 4.6 DLTS peak due to a change in capacitance transient

(6). The signature of a trap energy level E_a is found by the Arrhenius plot. In this subsection we will see how to find the energy of activation E_a of a given trap when a DLTS measurement have been performed on a semiconductor sample.

By the relation $1/\tau_n$ given by equation 4.14 we find from appendix VII that this equation can be written as

$$\ln(\tau_n T^2) = \frac{E_a}{kT} - \ln\{\alpha\beta\sigma_n\} \quad (4.26)$$

where E_a is the apparent activation energy, k the Boltzmann constant, T the temperature, α and β are constant, $\tau_n = 1/e_n$ and σ_n is the capture cross section. Note that the second term of the right hand side in equation 4.26 is independent of the temperature. In fact, equation

4.26 is a straight line of the form $y = ax + b$ where x represents $1/T$. The slope is then given by

$$a = E_a/k \quad (4.27a)$$

and the intercept is

$$b = -\ln\{\alpha\beta\sigma n\} \quad (4.27b)$$

which cuts the y axis. We recall here that a and b can be found by equations from the linear fit.

Thus, the Arrhenius plot (6); $\ln(\tau_n T^2)$ vs $(1000/T)$ allows one to find the activation energy E_a of the deep level trap by taking the slope of the line, and the capture cross section by the intercept of the line with the y axis.

4.3 Experimental Description for Finding $S(T)/C_0$ E_a and N_t

In this section, we describe the experimental procedure to find the capacitance transient $S(T)/C_0$, the apparent activation energy E_a and the total trap concentration N_t .

4.3.1 Experimental considerations for capacitance transients measurement

The measurement of the peak $S(T)/C_0$ described in subsection 4.2.4 is performed with the same equipment as described in sections 3.1.2 and 3.2.4 where four electronic apparatus have been added. For a good visualization of the experimental measurement $S(T)/C_0$ by DLTS, a

schematic is shown in figure 4.7. The HP computer, the multimeter, the capacitance meter (61)⁷ and the pulse generator, are shown; where an oscilloscope has been added in order to visualize the pulse height and the time duration if necessary. A printer and a plotter have been added also in order to get the print out of the initial conditions given by the operator and the plot of the final result of $S(T)/C_0$; and finally, a power supply is connected to the heating element inside the cryostat in order to heat it up. The sample is then placed on the tip tail inside of the cryostat where the temperature may be changed from liquid nitrogen (77K) to approximately 400K under vacuum.

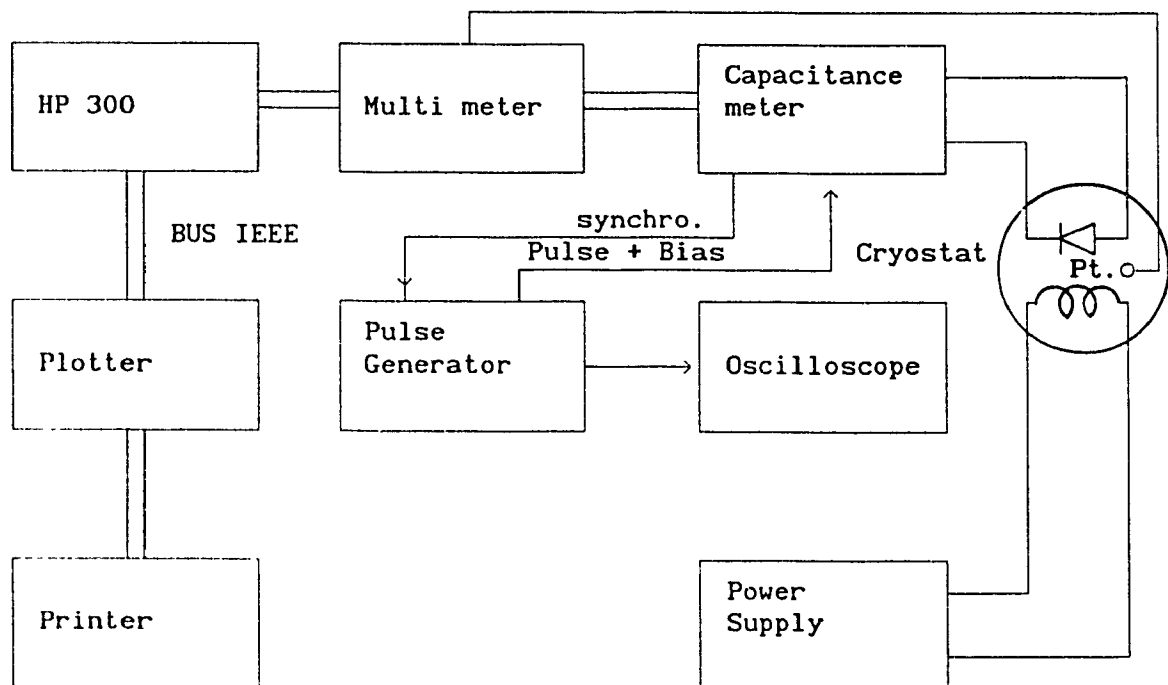


Fig. 4.7 Experimental setup for the measurement of $S(T)/C_0$ by DLTS

⁷ The capacitance-meter manual gives some indications for setting up fig. 4.7, and gives also some programming techniques.

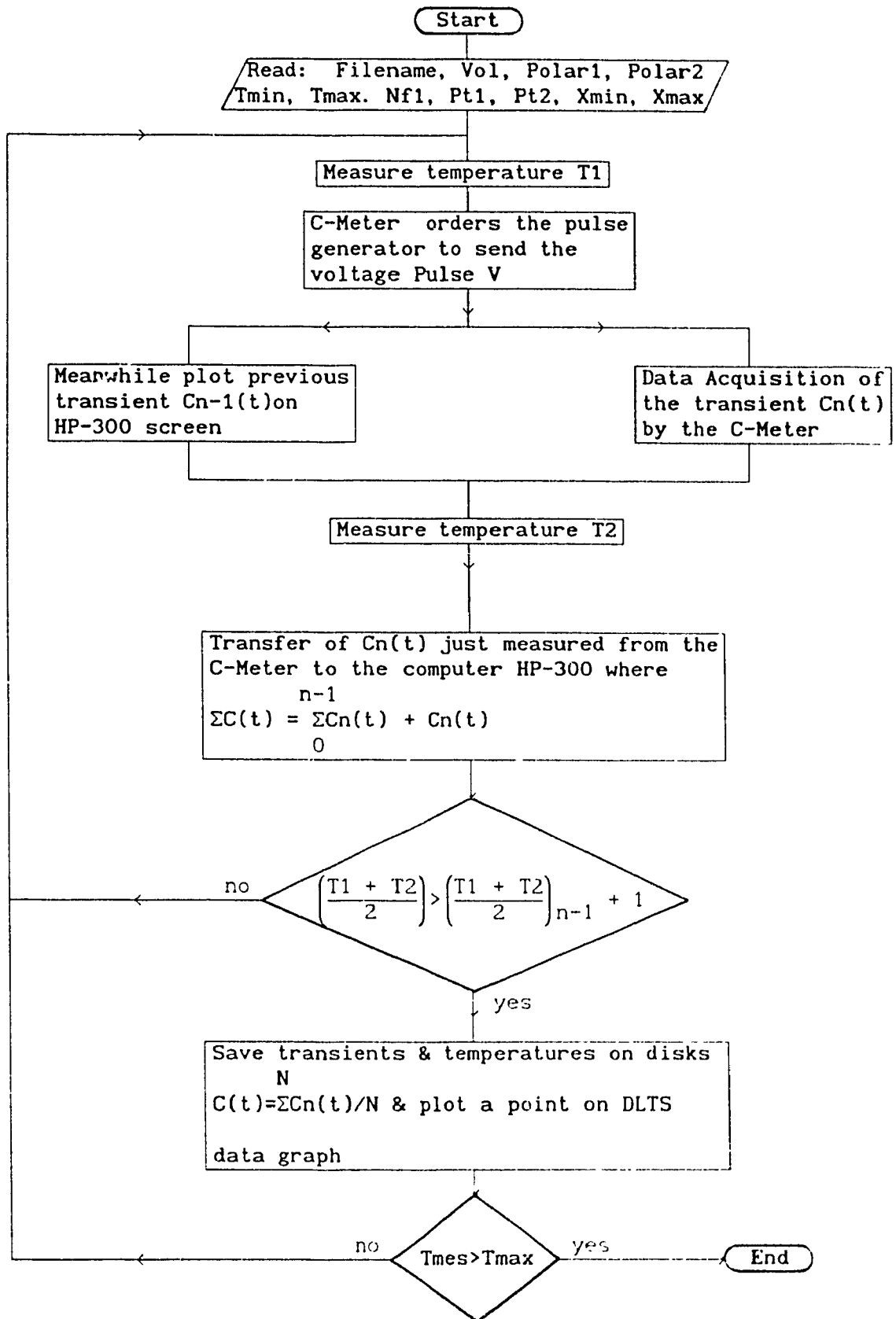


Fig. 4.8 Flow chart of DLTS by sampling

The principle of operation of the S(T)/Co measurement by DLTS is shown by the simplified flow chart in figure 4.8 above (61). The first step of the program allows the operator to enter all the parameters for the DLTS measurement. The reverse constant DC bias (Polar1) and the pulse height (Polar2) are entered (recall fig. 4.5a). Then the number of sampling points N for each capacitance transient is entered where N can range from 1 to 600. The pulse width in milliseconds and the time Td between two sampling points are also entered. Finally points Pt1 and Pt2 from figure 4.6 are entered in order to choose the rate window during the experiment. Figure 4.9 shows an example of one transient with variables to be entered initially that are stored in a data file by the computer.

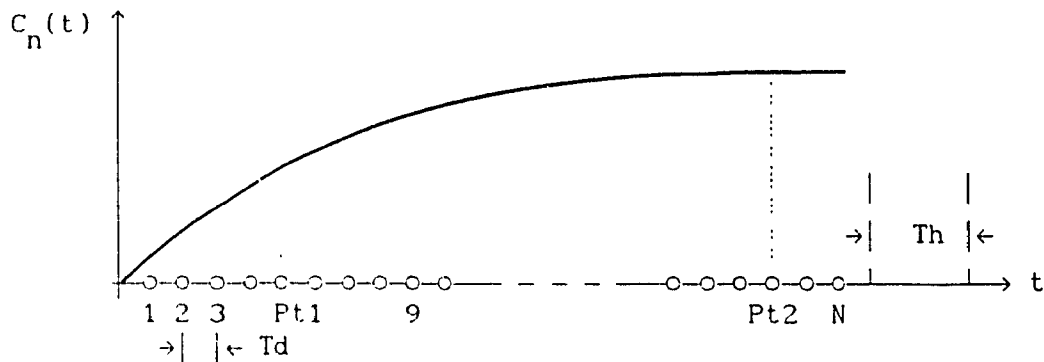


Fig. 4.9 Example for variables to be entered initially

The minimum temperature T_{min} and the maximum temperature T_{max} have to be entered in order to give the range of temperature the experiment is to be performed. Finally, the number of transients recorded in the file $Nf1$ (approximately 300) has to be set up by the operator, and the vertical lower bound X_{min} and upper bound X_{max} of the DLTS peak has to be set up before the experiment runs.

Thus a binary data file is created with file name (Name\$) in volume VOL of the mass storage unit chosen by the operator. Hence the binary data file can store all capacitance transients and temperature values for the entire temperature scan.

After the parameters has been entered, the computer measures a temperature T_1 . The temperature is measured with the platinum (Pt) resistance (R) installed inside the tip tail of the cryostat. The computer program ask the multimeter to get in ohmmeter mode so the resistance R can be read. The corresponding temperature due to the resistance read at that instant is given by the third order polynomial;

$$T = 31.5 + 23.5R + 0.002161R^2 - 3.58 \times 10^{-6}R^3 \quad (4.28)$$

derived from the sensor specification.

Then the capacitance meter orders the pulse generator, which is controlled by the HP-300 computer, to trigger the pulse (Fig. 4.5a). After the pulse duration, the capacitance meter enters N points of the transient into its buffer. Meanwhile, the computer can plot the previous transient $C_{n-1}(t)$ on the screen of the HP-300.

Once this has been achieved, a second measurement of temperature T_2 is performed and then, the transfer of transient $C_n(t)$ measured from capacitance meter to the computer HP-300 is performed where all the transients $C_n(t)$ are going to be stored in the computer buffer in array C(t).

Then the previous average temperature plus 1°C set by the operator is compared with the actual average temperature. If T_{av} is greater

than $T_{av-1} + 1^{\circ}\text{C}$, the transients and the temperatures data are saved on disks and a point is plotted on the $S(T)/C_0$ vs T° graph. If not, another measurement of T_1 is performed and the process continue as indicated by the flow chart.

Here the program stops when the measure of temperature is greater than T_{max} set at the beginning. When the computer has finished to perform its data acquisition, the DLTS peak(s) is (are) usually shown on the plotter and all transients and temperatures are stored on the disk for further purposes as it will be seen shortly.

4.3.2 Experimental procedures for finding E_a

In practice a computer program called DLTS spectrum reads the capacitance transients and the corresponding temperatures T stored on the disk (transient on the left hand side shown in figure 4.6) to transfer them into an array $C(t,T)$. Then from $C(t,T)$, the value of the experimental signal curve is plotted for n different times t_1 and t_2 as follows (right hand side of figure 4.6);

$$\frac{S(T)}{C_0} = \frac{C(t_2) - C(t_1)}{C_0} (e^{-t_1/\tau_n} - e^{t_2/\tau_n})^{-1} \quad (4.29)$$

where the experimental values of $\{[C(t_2) - C(t_1)] / C_0\}$ has been multiplied by $(e^{-t_1/\tau_n} - e^{t_2/\tau_n})^{-1}$ in order to find the total trap concentration N_t directly as it will be seen shortly. The term on the right hand side bracket is a correction factor. Thus the result will give n different peaks with the same height shifted in temperature, where the maximum peaks are found at T_m where $m = 1$ to n for this case.

For example, the operator can choose the values of t_2 as ten times

t_1 where t_1 can take five values such as 2, 3, 4, 5, 6. Therefore, it is obvious that the rate window τ_n given by equation 4.25 will change accordingly giving five different values for T_M for five corresponding DLTS peaks. The flow chart of figure 4.10 summarizes well the above statements of the experimental procedure.

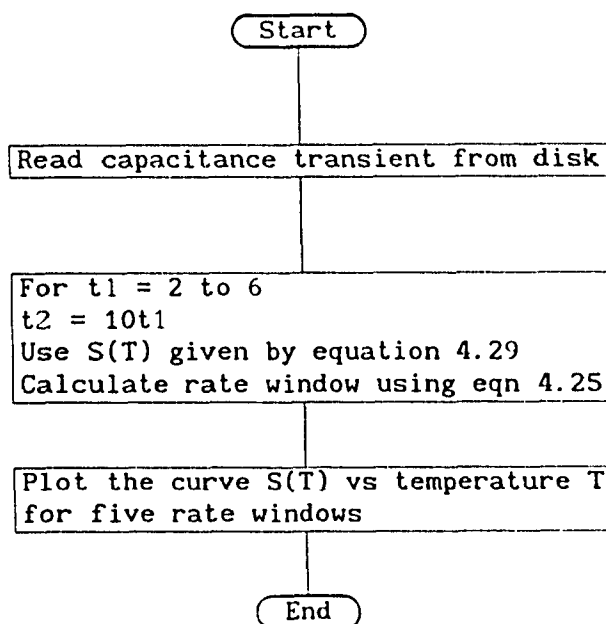


Fig. 4.10 Flow chart of the DLTS spectrum

The apparent activation energy E_a for this example is found knowing the peaks of $S(T_M)$ for five different rate windows. Therefore, a program called Arrhenius plot, enters all five temperature T_M with their respective emission rate τ_n and perform the plot $\ln(\tau_n T^2)$ vs $(1000/T)$ as shown by the flow chart of figure 4.11.

Then the linear fit is used (31) in order to find a and b from the straight line $y = ax + b$ as before and equations in 4.27a and 4.27b are used to find E_a and σ_n respectively.

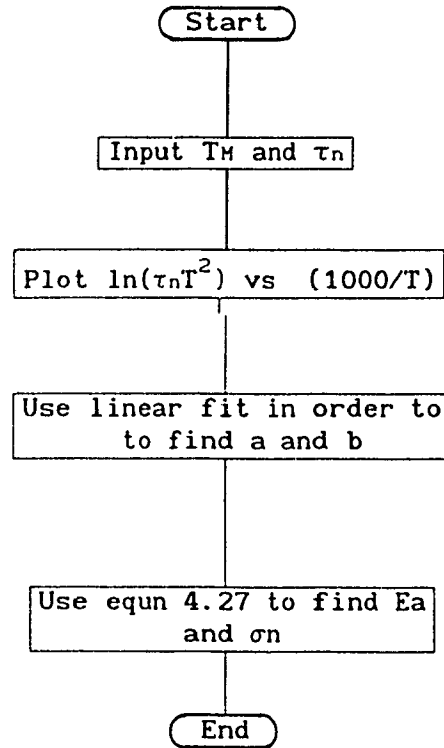


Fig. 4.11 Flow chart for Arrhenius plot

4.3.3 Summary of experimental procedure for finding all parameters and N_t

The very first thing to do to find all the parameters is to find N_D using the $C(V)$ method as explained in section 3.3.1. Then we have to perform the DLTS experiment as described in section 4.3.1 where the flow chart of figure 4.8 summarizes it well. At this point all the capacitance transients are stored on the disk.

The second step is to find the energy of activation E_a and the capture cross section σ_n of the trap of interest with the Arrhenius plot as described in section 4.3.2 with the help of the flow charts of figures 4.10 and 4.11.

Then the transition region λ can be found using equation 4.17 and

the values of W_0 and W_1 can be found from C_0 and C_1 measured by the capacitance meter respectively by the relation $W = \epsilon S/C$. Finally, the total trap concentration N_T can be found using equation 4.29 (with the help of equation 4.24) by taking $S(T_M)$ which is the maximum height of the experimental peak. Therefore,

$$N_T = 2S(T_M)N_D \left[\frac{\{(W_0 - \lambda)^2 - (W_1 - \lambda)^2\}}{W_0^2} \right]^{-1} \quad (4.30)$$

where the values have their usual their usual meaning.

5.0 RESULTS AND DISCUSSIONS

5.0.0 Introduction

In this chapter we discuss the deep level traps found in GaAs epitaxial layer by DLTS measurement technique under different conditions where all the detailed results are given in appendix I. The epitaxial layers were grown by the CSVT technique (5)(62) as described in appendix VIII. The samples labeled with letters R, B, E, AL, AU and AS had their epitaxial layer fabricated in our laboratory at Concordia University in Montréal and those labeled with letter D were fabricated at INRS Energie in Varenne Québec.

The sources and substrates used for the epitaxial layer growth in samples labeled R, B and E were both (100) direction undoped SI GaAs. For samples labeled AL, AU and AS, the source was undoped SI GaAs (100) direction and the substrates were undoped SI GaAs or Si-doped GaAs (100) direction. For the samples labeled D the source was Si-doped GaAs and the substrates were undoped SI GaAs and Si-doped GaAs. The electrical characteristics were determined by Hall effect measurements (63) using the van der Pauw technique at room and liquid nitrogen temperatures. For all samples, all the deposited layers were n-type with a residual doping concentration of 5×10^{15} to $5 \times 10^{17} \text{ cm}^{-3}$. The measured room temperature carrier mobilities were in the range of $3000 \pm 1500 \text{ cm}^2/\text{Vs}$.

The temperature range of the epitaxial deposition was 750 to 880°C with a nominal temperature difference of 40°C between the source and the substrate. The thickness of the deposited epitaxial layers were varying from 2.5 to 70µm.

Knowing the above characteristics from the laboratory where we fabricated the epitaxial layers, it was therefore possible to characterize those samples by the $C(V)$, $I(V)$ and DLTS measurements. The DLTS measurements allowed us to identify deep level traps donor such as EL2 and ELCS1 in samples labeled with R, B, E, AL, AU and AS. In samples labeled with D we have found different donor traps in addition to EL2 and ELCS1.

In the following sections, we discuss the results obtained by the method described in previous chapters. Then we show that the evolution of EL2 concentration is function of the possible off-stoichiometry variation with the deposition temperature (64) in CSVT as it is the case in GaAs grown by vapor phase epitaxy (VPE), metal organic chemical vapor deposition (MOCVD) (65) and liquid-encapsulated Czochralski (LEC) GaAs grown crystal (66).

5.1 Determination of free carrier concentration and barrier height

The n-type GaAs samples grown by CSVT have unknown free carrier concentration N_D and barrier height V_b . In order to find them we use the $C(V)$ measurement as described in section 3.1. An example of N_D and V_b found by the $C(V)$ measurement is given in figure 5.1 for $C(V)$ and figure 5.2 a and b for $1/C(V)^2$. All other values for N_D and V_b have been found the same way and the results can be found in appendix I for all samples studied.

The values of N_D for some samples have been found by the Hall effect (63)(67). The Hall effect measurement using the Van der Pauw technique gives the average resistivity through the epitaxial layer whereas the $1/C(V)^2$ measurement uses the slope. The latter measurement

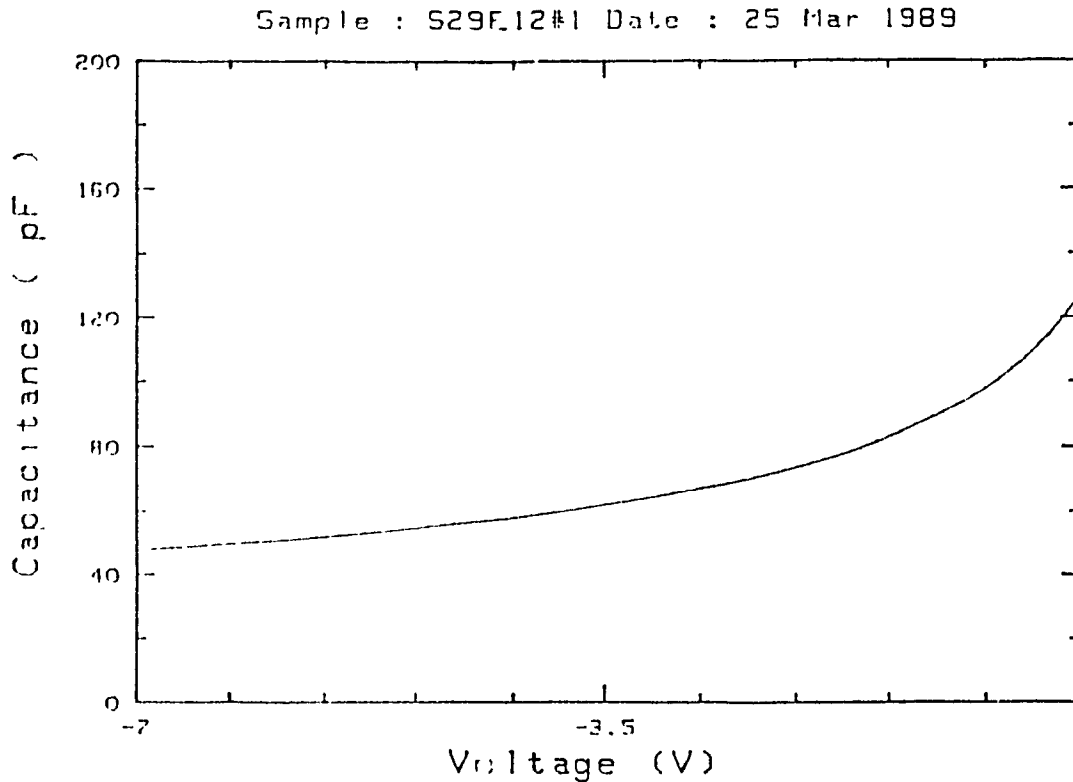
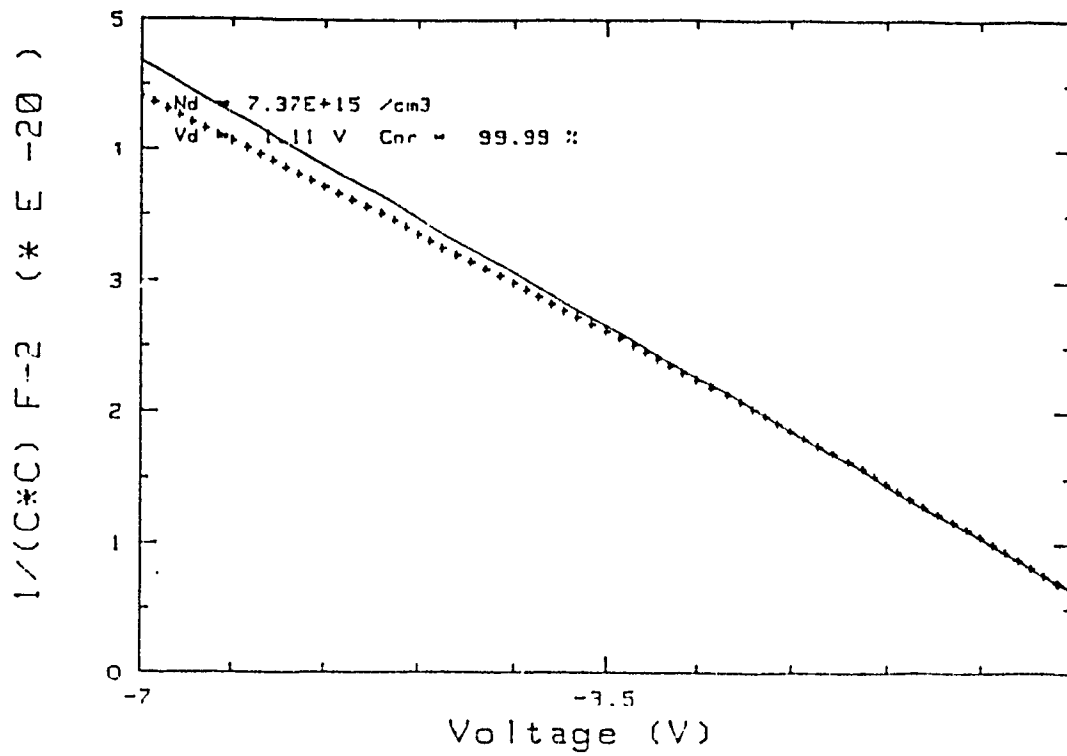


Fig. 5.1 C(V) measurement

(figures 5.2 a and b) shows the non uniformity of the doping since the slope is not quite linear. There are two apparent straight lines corresponding to two different N_D s. Therefore, the Hall effect measurement gives the overall free carrier concentration N_D and can be different from the $1/C(V)^2$ measurement due to the non uniformity of the doping in the GaAs n-type epitaxial layer (68) and the error in diameter of the metal deposited on the epitaxial layer.

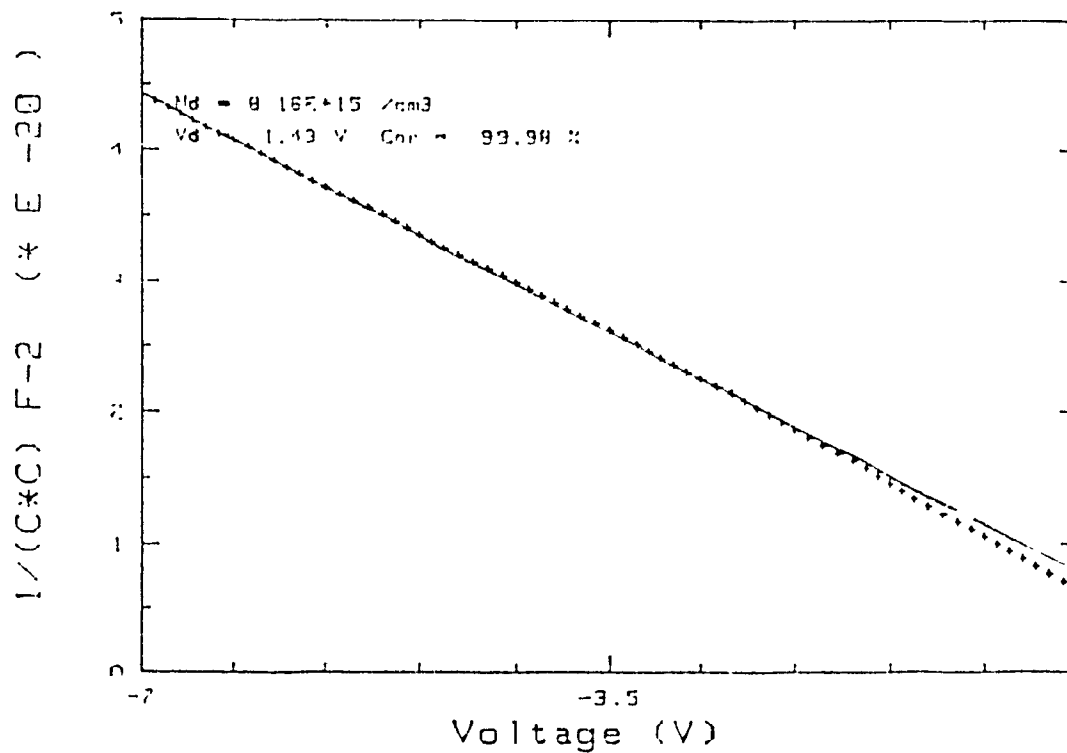
The non-uniformity of the doping was discussed extensively in references (68) and (69) for GaAs epitaxial layers grown by CSVT on GaAs substrates. From the charge density, N_D , profile of GaAs epitaxies for different thickness, it is shown that the epitaxial layers are not homogeneously doped. Thus the doping concentration N_D

Sample : S29E12#1 Date : 25 Mar 1989



a) (-2V 0V Bias)

Sample : S29E12#1 Date : 25 Mar 1989



b) (-7 -2V Bias)

Fig. 5.2 $1/C(V)^2$ measurement

varies with the thickness: the doping level increase from the surface of the layer to the interface between the epitaxial layer and the substrate (68).

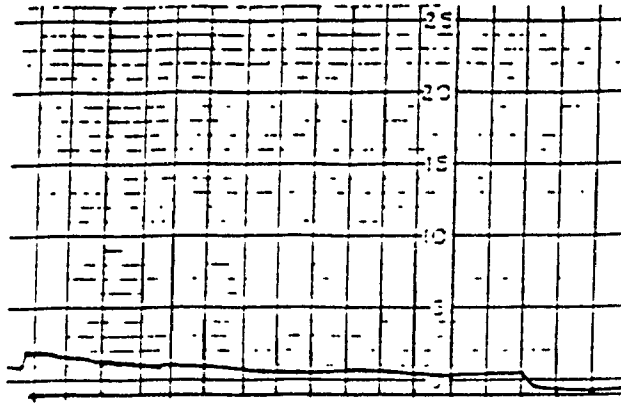
The accuracy of the diameter of the circle defining the surface area of the metal on the epitaxial layers of the GaAs SC plays an important role in the determination of N_D . Referring to equation 3.5, it is seen that N_D depends on the surface area of the junction.

In order to verify the possible range of error in N_D , we have taken some samples at random and we measured the diameter of the surface area of the metal with a *Talysurf*. In high resolution, a diamond stylus is used having a tip width of less than $1.25\mu\text{m}$ and five resolutions of the pen shift control provide a total pen shift equivalent to a change in stylus height of $\pm 0.025\text{mm}$ within $\pm 5\%$ (70). The measured values are given in table 5.1, and three typical examples of the diameter taken are shown in figure 5.3.

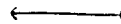
With the help of a microscope and then the *Talysurf* we have noticed that some surface areas were circular and some were elliptical. As given in table 5.1, we have calculated the surface area of the elliptical junction ($S=\pi ab$) and we changed it to an effective diameter for a circle ($S=\pi(D/2)^2$) since during the experiment, a diameter of 0.8mm was expected from the masking process which is described in appendix X in section C. Thus we notice from the table that the diameter area are in approximate range from 0.75 to 0.85mm which causes a considerable error in N_D .

Originally, we wanted a precise 0.8mm diameter. So we made

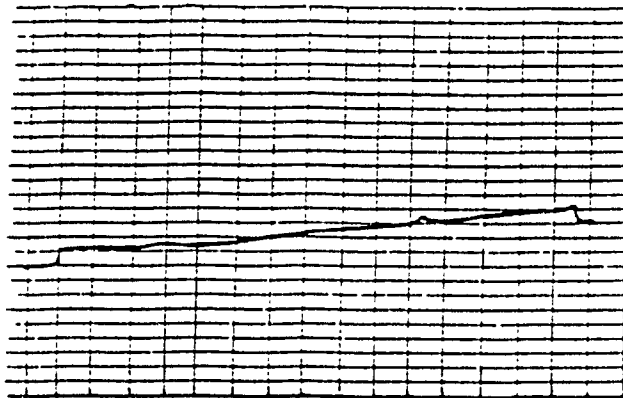
a)
5 μ m
full
scale



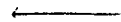
0.05mm/div.



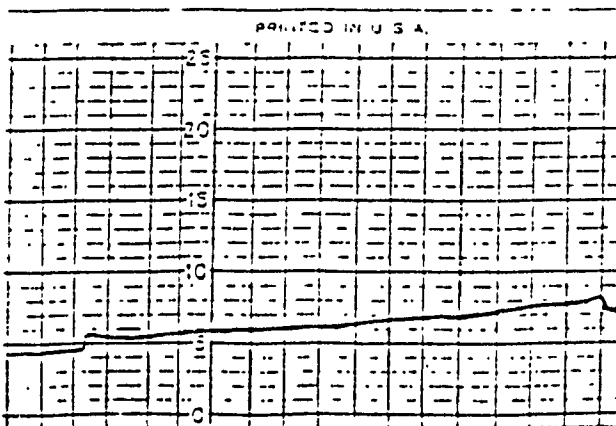
b)
5 μ m
full
scale



0.05mm/div.



c)
5 μ m
full
scale



0.05mm/div.

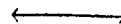


Fig. 5.3 Typical curves from the Talysurf

circles of 20mm of diameter precisely with a compass on *Rubilith*¹ and we reduced them twice five times with a reducing camera in order to obtain the required diameter. For the first set of masks we obtain ellipses since we realized that the camera reduced a bit more on the y axis than on the x axis to which introduced an error in the diameter D.

The second set of masks made where circular and their diameters were found to be around 0.74mm to which can be seen from the table 5.1.

TABLE 5.1: Diameter found from the Talysurf.

No.	S mm ²	Ellipse		Circle	S mm ²	Effective D(mm)
		a(mm)	b(mm)	D(mm)		
1	0.4959	0.820	0.770			0.7946
2	0.4959	0.820	0.770			0.7946
3	0.4688	0.770	0.730			0.7497
4	0.4898	0.810	0.770			0.7897
5	0.4959	0.820	0.770			0.7897
6	0.5329	0.780	0.870			0.8237
7	0.3675	0.600	0.780			0.6841
9				0.740	0.4300	
10				0.740	0.4300	
11				0.740	0.4300	
12				0.850	0.5640	
13				0.850	0.5640	
14				0.740	0.4300	

¹ Special paper for photographic process

This time the masks were circular since we reduced the initial circles once five times on the y axis and once five times on the x axis in order to reduce the error considerably. It is noticed that some diameters vary even when we use the same masks for fabricating the diodes. This is because of an improper vertical spacing between the mask and the sample on the *mask aligner* which is not always obvious to the operator. Therefore, an improper spacing can cause a change in D since the ultra violet (UV) light can spread a little under the mask during photo resist polymerization thus increasing the surface area of the junction.

The errors in the diameter and thus the error in N_D are shown in table 5.2. We took a sample (CP26_1) that a nice $C(V)$ characteristic and we measured N_D for different bias. Here the comparison is obvious; for a variation of +6.25% in D (i.e. from 0.8mm as an initial value to 0.85mm), it introduces an error of 27.7% in N_D for bias between (0-2V). For bias between (-2-6V) with +6.25% of variation in D , we have a +29.8% of error in N_D . Similarly, for a variation of -6.25% in D , we have an error of -29.6% in N_D for bias of (0-2V), and -51.7% error in N_D for (-2-6V) bias.

Also, another percentage of error in N_D can be added to the above if the slope is taken for larger range of bias (-2-6V) as compared to a lower range (-2-10V). It can be seen from table 5.2 (between # 10 and 13) that there is a 13.46% error between (-2-10V) bias and (-2-6V) bias for the same D . The value for N_D should be more accurate with (-2-10V) bias simply because more points are available for the linear fit. It occurs some times in practice that we cannot go farther than (0-4V) bias since we are limited by the reverse breakdown voltage of the diode

itself where the capacity change drastically. For a low bias (0-2V) (between # 1 and 11) the percentage of error is lower (3.1%) since the carrier concentration does not vary much near the surface (68).

TABLE 5.2: Error found in N_D according to a change in diameter D.

No	Bias(V)	D(mm)	N_D (cm ⁻³)	%err. D	%err. N_D	Between No.	% error
1	0 -2	0.80	2.26E15	0.00		1 and 11	03.1
2	0 -2	0.81	2.14E15	1.25	05.60	1 and 2	05.60
3	0 -2	0.85	1.77E15	6.25	27.68	1 and 3	27.68
4	0 -2	0.90	1.70E15	12.50	33.00	1 and 4	33.00
5	0 -2	0.75	2.93E15	-6.25	-29.60	1 and 5	-30.00
6	-2 -6	0.75	3.52E15	-6.25	-51.70		
7	-2 -6	0.90	1.41E15	12.50		7 and 16	-25.79
8	-2 -6	0.85	2.08E15	6.25	29.81		
9	-2 -6	0.81	2.57E15	1.25			
10	-2 -6	0.80	2.70E15	0.00		10 and 13	13.46
11	0 -2	0.80	2.33E15	0.00	03.10		
12	-4 -10	0.80	3.21E15	0.00		12 and 13	37.00
13	-2 -10	0.80	3.12E15	0.00	13.46		
14	0 -2	0.90	1.46E15	12.50			
15	-4 -10	0.90	1.95E15	12.55			
16	-2 -10	0.90	1.90E15	12.55			

Finally, it is observed that the choice of the points for the linear fit may introduce another percentage of error (71). For example, we have taken the slope for bias between (-2-10V) and (-4-10V) and we found 37% of error (between # 12 and 13). It is therefore critical to

choose the proper points for the linear fit in the most linear region that appears to the operator on the screen of the computer.

Therefore, the error in N_D depends mostly on what was discussed above since the C-meter is a reliable piece of equipment. Because of the importance of the $C(V)$ measurement, the C-meter is discussed below.

The basic measurement accuracy of the 4280A C-meter is 0.01%, and measurement resolution is 1fF on the most sensitive range (pF). The measured capacitance is displayed with 5-1/2 digit on high resolution (72). For a small $\Delta C/C$ transient, the capacitance measured may be very small (near 1fF) thus limiting the measurement of the peak $S(T)$. This small measurement in capacitance C can keep from seeing the EL2 trap for example. At this point the C-meter is working on its limit.

The capacitance measurement is achieved by an internal 1MHz sine wave source of 30m Vrms or 10m Vrms to suit the characteristics of the device under test (the measurement range is given in the manufacturer table). A built in DC source whose output can be swept in a staircase manner, and an automatic error correction function to ensure accurate repeatable measurements are used to change the capacitance of an Si diode junction under test. The error correction function "virtually eliminates the effects of error-causing strays and residual inherent in the test leads and test fixtures used to connect test samples to the unknown terminals" (73). Figure 5.4 shows the simplified capacitance circuit measurement.

The diode is connected inside the cryostat under vacuum to which the cryostat is linked by two coaxial cables to the two terminal pair configuration at the C-meter. This eliminates mutual inductance between test leads because of their insulation and reduce the effect of

environmental noise when measurement requiring pulse biasing (72). With this connection mode, the C-meter measures the capacitance C and the conductance G , of the equivalent unknown parallel circuit of the device connected to the terminals (73).

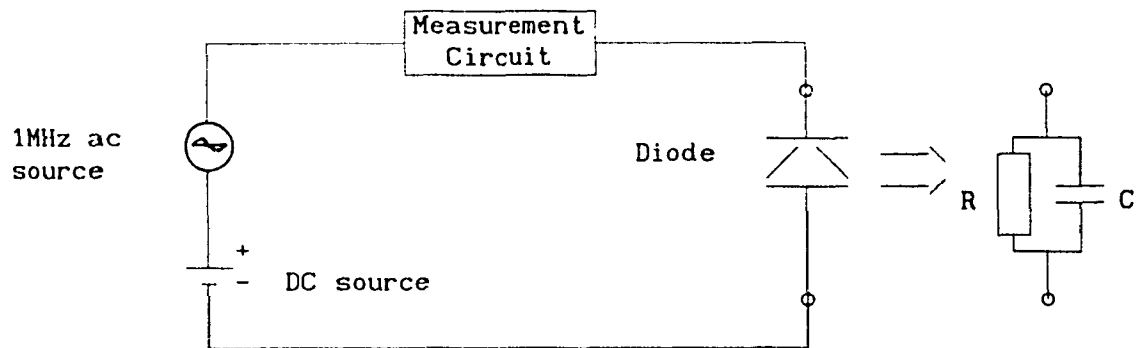


Fig. 5.4 Capacitance circuit measurement

The 1MHz sine wave frequency source is periodically tested with an oscilloscope and a frequency counter. The internal DC source is also verified periodically using the HP3456A multi meter² where the procedure is described in the users manual using appropriate tables (74). Finally the manufacturer gives the procedures to follow and tables to perform the C and G standard tests according to specific connection modes. Here the manufacturer specifies that the tests must be performed at $23^{\circ}\text{C} \pm 5^{\circ}\text{C}$ with the C-meter warmed up 30 minutes before the test.

Therefore, we can rely on this sophisticated C-meter to find the free carrier concentration N_D after tests performed periodically.

²The multi meter will be discussed in a further section.

5.2 Apparent Activation Energy E_a

In this section, we determine experimentally the thermal ionization energy E_a (or equivalently the apparent activation energy) from the DLTS measurements performed in all our samples. Then we discuss the probable causes of error. In further sections we will discuss the particularity of each activation energy E_a or deep lying trap level.

5.2.1 Identification of deep level traps

The ionization energy E_a was found from the DLTS peak measured as described in section 4.2.4 and 4.2.5. An example of DLTS peaks is shown in figure 5.5. Then the Arrhenius plot described in section 4.3.2 was used. In practice we selected samples where the peak height was high enough in order to determine E_a .

In all the samples except some samples in the series D369 though D378, we found two different peaks which are shown in figure 5.5 where the growth of epitaxial layers made by CSVT was performed using semi-insulating source for all samples and both a semi-insulating and Si-doped substrates. The peak on the left hand side is found at a temperature near 300K for a rate window τ_n equals to 0.391s and the one on the right hand side is found at a temperature near 335K for the same rate window. These two peaks have been found in all samples with different peak height especially for the peak at 300K as it will be discussed later on.

For the peak on the right hand side, we have drawn twenty seven peaks using the DLTS spectrum program given by the flow chart of figure 4.10. Figure 5.6 shows only 5 peaks for convenience. The sample used was #R16. From these peaks, the temperature were taken for each

maximum peak and corresponding emission rate. The results are shown in table 5.3. Then the Arrhenius plot was used as described by the computer program from the flow chart of figure 4.11. The plot is shown in figure 5.7. Finally, from this plot, the apparent activation energy E_a was found to be equal to 816.07meV and the capture cross section σ_n was found to be equal to $3.02 \times 10^{-13} \text{cm}^2$. This ionization energy and capture cross section is a particular trap level identified as the EL2 deep level donor electron trap. Our measurement agrees with the published results (65)(75) where EL2 is found to be E_a equals to 820meV and σ_n equals to $1.7 \times 10^{-13} \text{cm}^2$.

In order to find the uncertainty of our results in E_a , we have taken the same sample (R16) and we have performed six DLTS measurements on it. Then we have found six E_a and six σ_n using 14 temperature peaks and emission rates each time. Then we averaged up the six E_a and σ_n and we calculated the standard deviation (76). The results are given in table 5.4. Thus we found an average E_a equal to 800.2meV with $\pm 18 \text{meV}$ of deviation from the mean and with σ_n equal to $1.97 \times 10^{-13} \text{cm}^2$ with $\pm 1.4 \times 10^{-13} \text{cm}^2$.

The uncertainty found in E_a is $\pm 18 \text{meV}$ which is low since the total band gap energy E_g for GaAs is equal to 1420meV (77). Furthermore, a variation of a few degrees in temperature does not change much the slope of the line on the Arrhenius plot (i.e no large variation in E_a) but may cause a large variation in σ_n ; since σ_n is taken on the y axis of the plot. Thus a slight change in the slope will give rise to a large error in σ_n even if the mean of σ_n agrees with published results.

In order to support our results for E_a for EL2, we measured E_a for sample B51 with the above method. We found E_a equals to 830meV and σ_n

Sample : AS40MEP16 Date : 5 Oct 1989

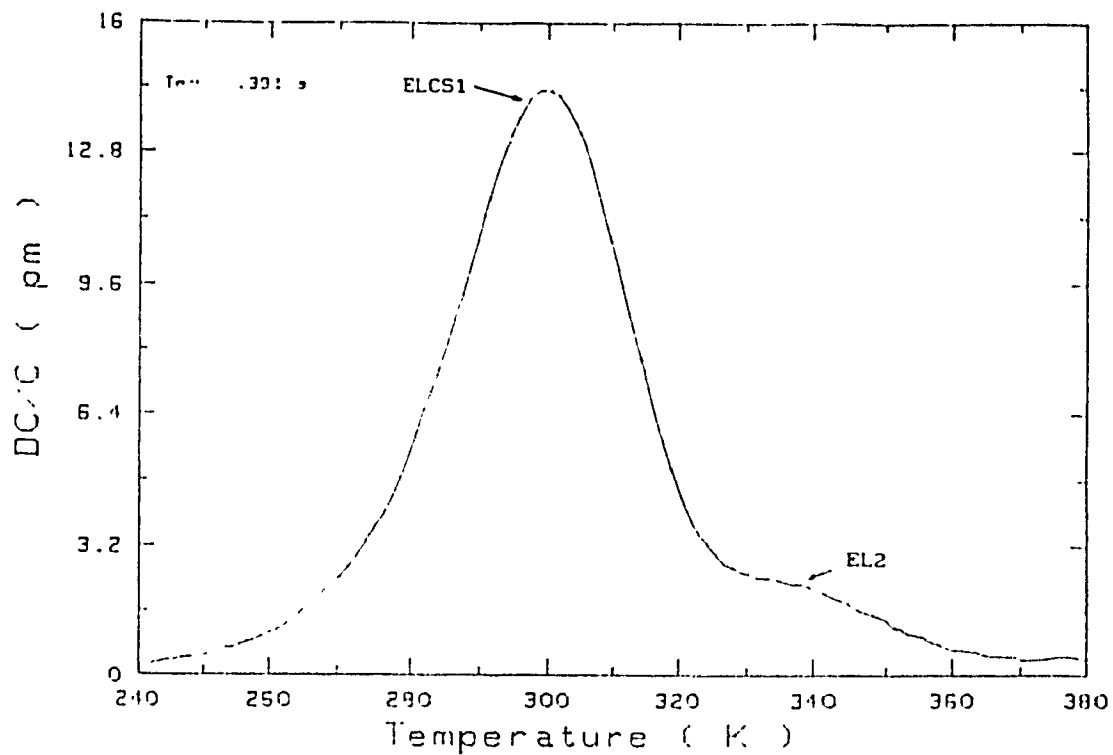


Fig. 5.5 Typical DLTS spectrum

Sample : S31R16-1#2 Date : 31 Jan 1989

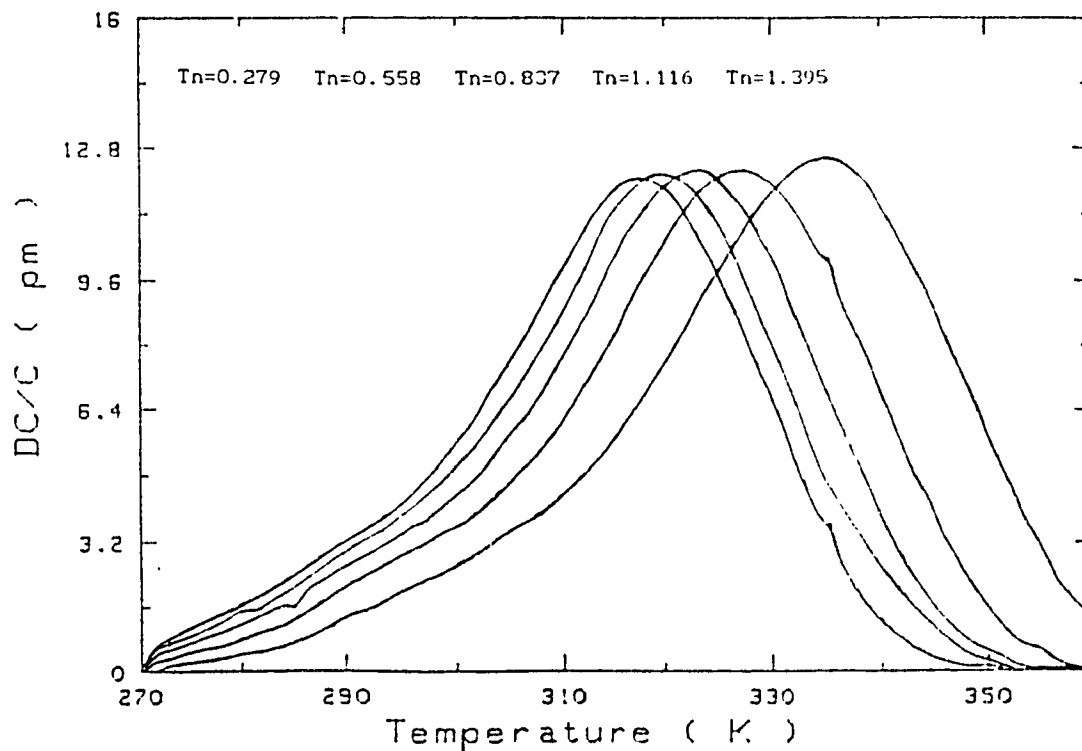


Fig. 5.6 DLTS peaks for different rate window (for EL2)

TABLE 5.3: Temperature with corresponding rate window for fig. 5.7.

No.	Temperature (K)	rate (s) window	No.	Temperature (K)	rate (s) window
1	308.05	3.5410	15	319.51	1.1160
2	310.98	2.6560	16	326.34	0.5130
3	321.46	0.8850	17	333.90	0.2660
4	310.73	7.7910	18	325.36	0.6700
5	312.68	2.2320	19	322.93	0.8730
6	315.12	1.6740	20	327.78	0.5020
7	319.51	1.1160	21	332.68	0.3350
8	326.34	0.5580	22	339.07	0.1670
9	306.34	3.9090	23	319.05	1.1730
10	312.68	2.3450	24	321.46	0.9380
11	322.19	0.7820	25	323.41	0.7040
12	336.59	0.2350	26	327.59	0.4690
13	315.61	1.5130	27	309.27	3.1270
14	322.93	0.7970	28		

TABLE 5.4: Several measurements of apparent activation energy for EL2

No.	Ea(meV)	Sigma(cm-2)
1	782.23	8.48E-14
2	796.22	1.33E-13
3	818.30	3.27E-13
4	824.23	4.21E-13
5	797.29	1.36E-13
6	782.23	8.46E-14
average	800.20	1.97E-13

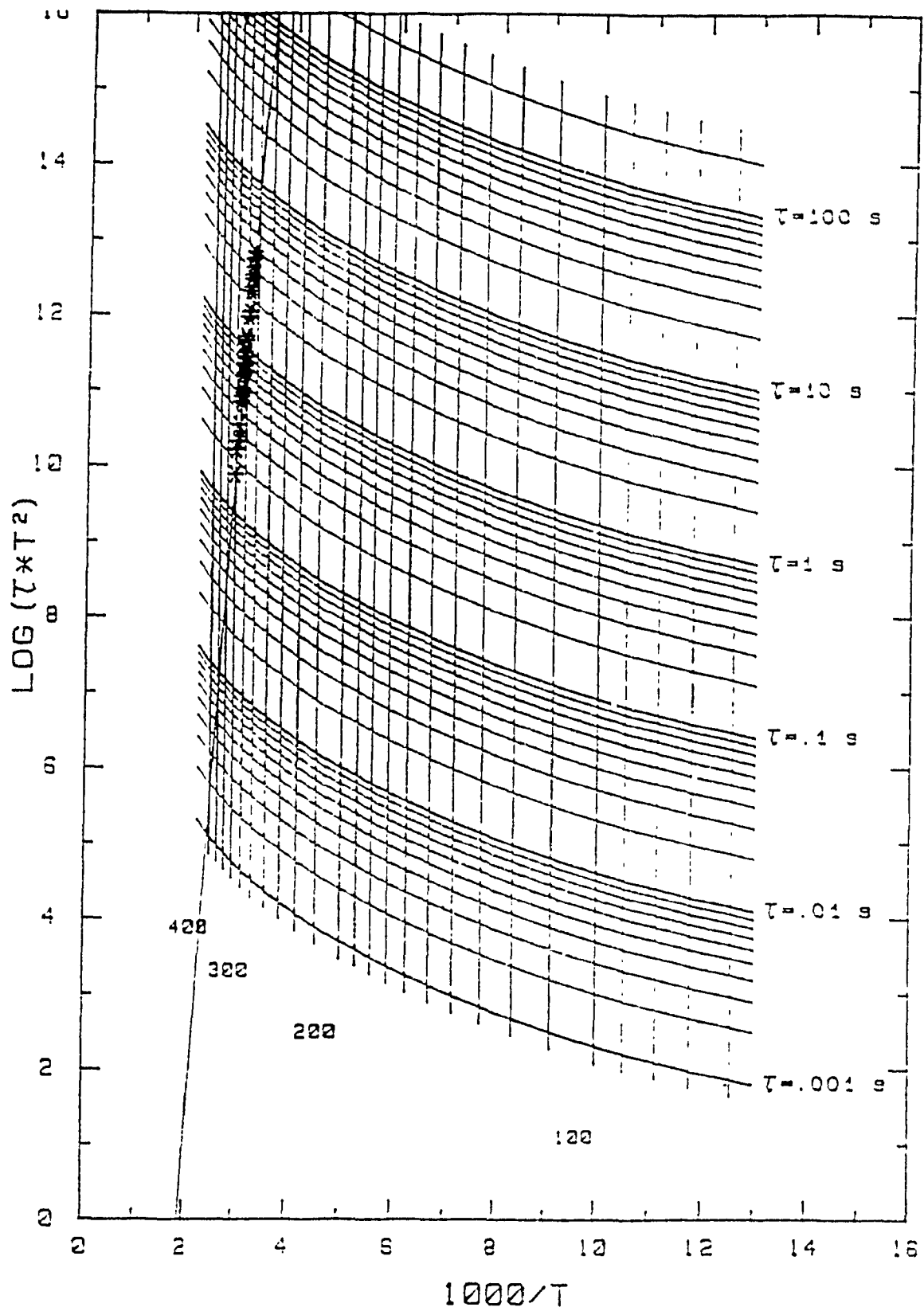


Fig. 5.7 Arrhenius plot allowing to find E_a

equals to $1.9 \times 10^{-13} \text{ cm}^2$. Furthermore, we took a Bridgman sample where EL2 is expected to be found (78). We performed our DLTS experiments on the sample with our experimental apparatus and we found E_a equals to 304.9 meV and σ_n equals to $2.46 \times 10^{-13} \text{ cm}^2$ which agrees with published results.

In some cases the EL2 deep lying trap level is seen in low concentration (low peak height) and for these cases it is rather difficult to measure E_a . An example of EL2 in low concentration (right hand side peak) was shown in figure 5.5. Therefore once we have determined E_a properly, we may recognize the EL2 trap level if the peak is located at 335K for τ_n being equal to 0.391s. EL2 can also be recognized for each temperature and corresponding τ_n in figure 5.6 since it has been determined from this plot.

The next trap to be discussed is also found in all samples with the peak temperature near 300K for τ_n at 0.591s. This is the left hand side peak shown in figure 5.5. We have measured E_a and σ_n with the same method as described above. We found an overall average in E_a equal to 730 meV \pm 31 meV with σ_n equal to $3.8 \times 10^{-13} \text{ cm}^2 \pm 4.2 \times 10^{-13} \text{ cm}^2$ where the capture cross section may vary considerably for the reasons mentioned above. This deep donor trap is identified as ELCS1 with 730 meV and 10^{-13} cm^2 (79)(80). Our results agree with published results within the limit of error found above.

We have verified this deep donor trap by comparing the DLTS measurement made on samples at USTL Montpellier France and at Concordia University in Montreal. We took eleven samples at random (#AU & ALU) that were characterized in Montpellier and thirteen samples at random that were characterized in Montreal: samples series # S29E, S30R and

R. Then we averaged up each set and we found the results which are shown in table 5.5. These results show that the ionization energies E_a were comparable for different samples where they were characterized at two different laboratories.

TABLE 5.5: Comparison for ELCS1 trap found at different laboratories:

Sample #	$E_a(\text{meV})$	$\text{Sigma}(\text{cm}^{-2})$
AU & AL	726.8 ± 34	$4.38 \text{E}-13$
S29E	712.3 ± 43	$5.77 \text{E}-13$
S30R	710.2 ± 26	$2.20 \text{E}-13$
R	715.4 ± 27	$3.28 \text{E}-13$

We have found another particular peak in samples D372 and D373 after annealing and etching them. Eight different measurements have been taken for E_a . We found an average E_a equal to $614.75 \text{meV} \pm 43 \text{meV}$ with σ_n equal³ to $1.58 \times 10^{-15} \text{cm}^2$. We think that this trap was not found elsewhere in GaAs epitaxial growth by CSM. Of course more results should be taken to ascertain the validity of this result. This trap can be recognized for a temperature 285K for τ_n equal to 0.391s

Finally, in samples series D370 we found four donor traps after annealing the samples at 750°C for 1/2 hour. These are shown in figure 5.8. Using always the same method, we found the ionization energies and capture cross sections. They are given in table 5.6 for these traps found at low temperatures it is not possible to determine

³ Let $E_a = 0.62 \text{eV}$ and $\sigma_n = 1.6 \times 10^{-15} \text{cm}^2$ for convenience, for this particular trap.

La correctly with the cryostat we are usually using in our laboratory. The reason will be given in the next subsection. We can say that the E_a values found are rough approximation for the latter case.

Sample : 36D374_2 Date : 28 Jun 1989

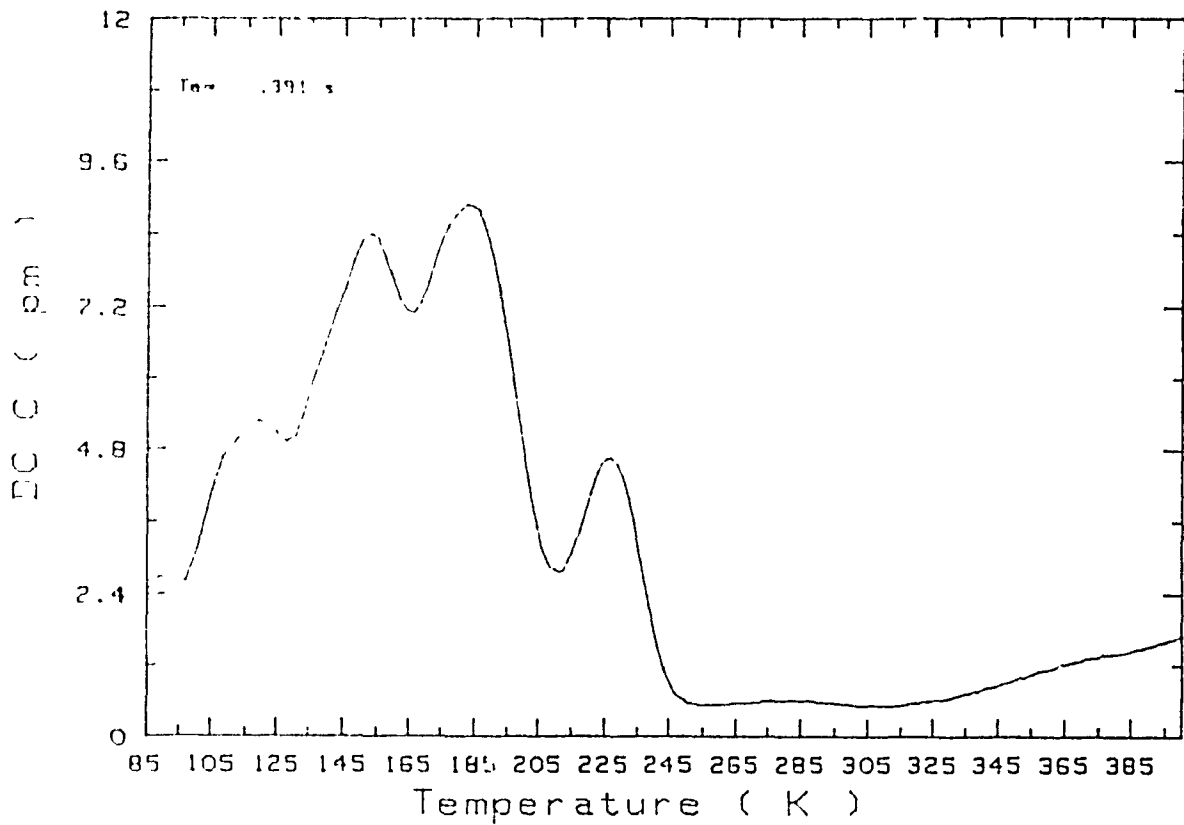


Fig. 5.8 DLTS spectrum for sample D374

TABLE 5.6. Apparent activation energies for peaks shown in fig. 5.8.

Peak No.	$E_a(\text{meV})$	$\text{Sigma}(\text{cm}^{-2})$
1	238.00	
2	327.70	4.83E-14
3	387.50	4.11E-15
4	517.05	1.51E-14

5.2.2 Probable causes of error in finding E_a

From one DLTS measurement to another for a given rate window the peak may shift a few degrees in temperature. This shift in temperature may cause errors in finding E_a and σ_n . Furthermore, the thermal velocity rate (ΔT) is suppose to be constant and slow ($\Delta T \cong 1$ to 2K/min.) for a better averaging for the DLTS peak signal $S(T)$.

From the discussion in the previous section, we know that we can rely on the equipment for the DLTS measurement. Consequently, the validity of our experiment depends on the temperature measurement at the sample which is under vacuum inside the cryostat. The temperature is measured with a platinum resistance which is placed on the sample. Then the temperature is calculated with equation 4.28

To check the validity of our platinum resistance, we have measured its resistance at liquid nitrogen (77K or -196°C), at melting temperature with deionized water (DI) (273K or 0°C), at ambient temperature (288K or 25°C), and at boiling DI water temperature (373K or 100°C). Thus we have measured the resistance and compared with the manufacturer specifications. Then we have calculated the corresponding temperature using equation 4.28.

It is observed from table 5.7 that the errors in resistance and in temperature are low. Thus the temperature given by the platinum resistance is reliable.

Another point that we have verified was where to put the resistance for maximum reliability in temperature? In order to ascertain the validity of our measurement in temperature depending where the resistance is located, we have put two identical platinum resistances that we have tested before the experiment, and we have put

TABLE 5.7. Error between theoretical and experimental temperature measurements.

Temperature T1		R (ohm)		% Error	Temp(K) T2	DT	% Error
C	K	Read	Given	in R	Calculated	K	T1 & T2
-196.0	77	21.62	21.00	2.95	80.79	3.79	-4.40
00.0	273	101.00	100.00	1.00	275.59	2.58	-0.94
25.0	298	110.68	110.00	0.62	300.47	2.47	-0.82
100.0	373	137.00	138.50	1.10	369.09	3.95	+1.08

one inside the cryostat tip tail (made of copper) and one on the sample which is placed on the tail inside the cryostat. Then we have performed a DLTS measurement from 80K to 400K and we have measured the values of R1 and R2 at an average spacing at every 3 ohms. The results are shown in table 1 in appendix IX.

The results show that the sample and the cryostat tail are following each other in temperature within an average of 1% of error. This is very important that the sample and the cryostat tail follow to each other in temperature; if it is not the case, a large error in temperature reading will occur thus shifting the DLTS peak in temperature inducing an error in finding E_a . Therefore, whether the platinum resistance is placed on the tip tail of the cryostat or on the sample, the reading in temperature should be correct within 1% of error in the resistance value.

Another problem in using the cryostat is the thermal rate velocity in temperature (ΔT): the cryostats used are cooled down with liquid nitrogen (77K) and warmed up to around 400K so the sample can follow this range of temperature.

The main problem is the high thermal velocity (K/min.) in low temperature. The cryostat used in Montreal has a tendency to warm up to rapidly from around 100K to 260K where the operator has no control over it. An example is shown in figure 5.9a. This is the reason why we cannot assure the validity of E_a found for the four DLTS peaks given in table 5.6, which was discussed in subsection 5.2.1. Therefore the proper measurement of E_a for the peaks found below 260K should be done with a cryostat that has a low thermal rate velocity in low temperature from 77K to 260K.

For temperatures higher than 260K up to 400K, it is up to the operator to control the temperature manually so that the thermal speed be as constant as possible because we want a good averaging of the signal $S(T)$. Figure 5.9a shows a typical example of an average control in thermal speed where ΔT is around 1.5K/min. In this case E_a can be determined properly. Figure 5.9b shows an example where ΔT varies from around 1K/min. to 4.4K/min. For the latter case the signal averaging is not correct thus inducing an error in the DLTS peak measurement.

The cryostat used in Montpellier France had the possibility of a low thermal rate velocity in low temperature. In order to keep our ΔT as constant as possible, we have built a temperature regulator. The circuit is shown in figure IX.1 in appendix IX. This circuit compares the increment in temperature with a linear ramp where we can choose its desired increment in thermal speed. The ramp is generated by a simple integrator circuit (S1). By comparing the two signals, the power supply feeds more or less power to the heating element inside the tail of the cryostat. This circuit worked out very well with the cryostat used in Montpellier. Table IX.2 in appendix IX shows the results in

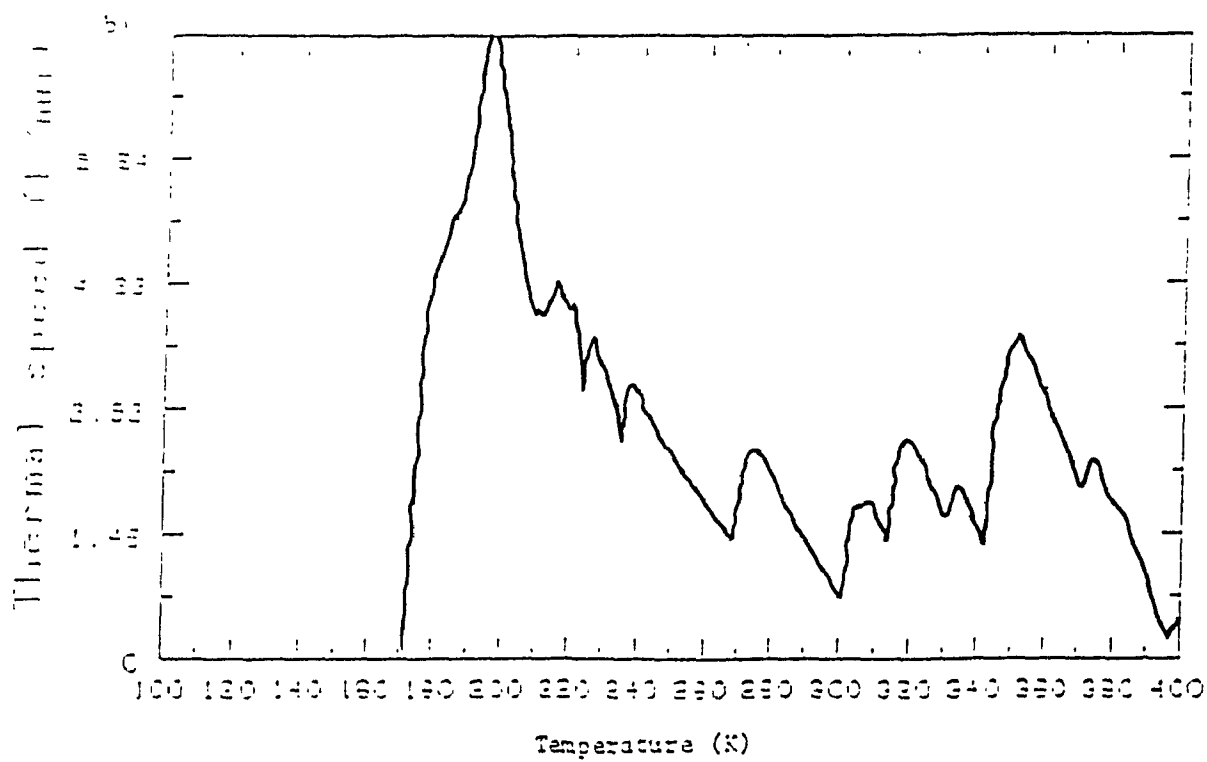
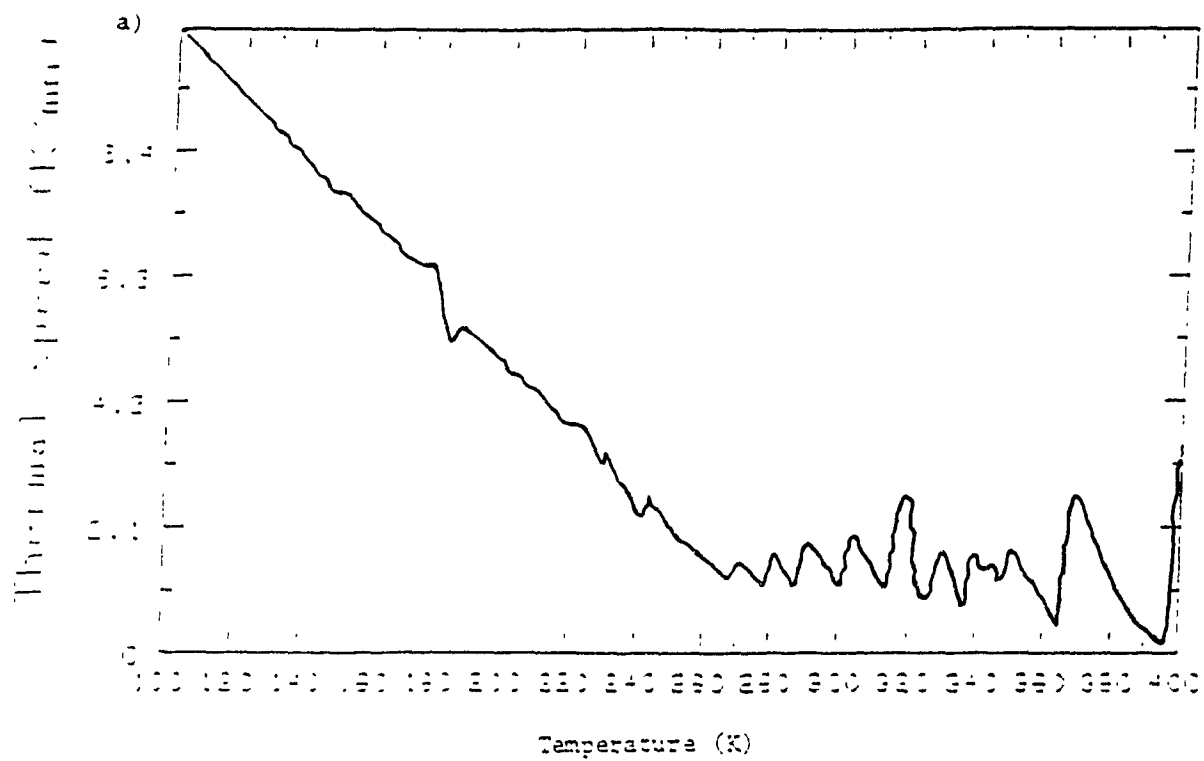


Fig. 5.9 Examples of thermal speed as function of the temperature

ΔT for a DLTS experiment from 80K to 400K. The low variation in ΔT ($\Delta T_{\text{average}} = 1.5\text{K/min.}$) shows that the increment in temperature was fairly constant thus allowing the operator to determine E_a properly for DLTS peaks found at any temperature range.

Unfortunately, this circuit did not function properly with the cryostat used in Montréal because of the high thermal speed change in low temperature. However it could work out for temperatures greater than 260K after a proper adjustment of the potentiometer in the circuit. In order to make it work in low temperature, we suggest to redesign the circuit using a pump that would cool down the cryostat by injecting liquid nitrogen in it if the case may be. This way, ΔT would be constant throughout the whole experiment.

5.3 Experimental Results

The determination of deep level trap concentration N_t allows to draw interesting conclusions as it will be seen in further sections. We have determined the value of N_t experimentally using equation 4.30. From the plot of DLTS experiments we have measured the peak height $S(T_M)$. Then we find $C(V_0)$ and $C(V_1)$ from the $C(V)$ plot (figure 5.1) in order to find W_0 and W_1 . Finally λ is found from equation 4.17 since E_a has been found previously. Then the value for N_t were calculated for all samples.

Here we show the experimental results for samples R16, B46 and B51 put in tables 5.8, 5.9 and 5.10 respectively. For example, table 5.8 shows the sample number on the upper left hand side rectangle. Then " T_{subs} " represents the substrate temperature during the epitaxial layer growth for that particular sample (R16). Then the epitaxial layer

thickness, the free carrier concentration (N_D) and the mobility (μ) are given. Both N_D and μ were found from the Hall effect measurements. From the table, we can find in each column:

- E_a . The apparent activation energy (eV)
- W_0 : Depth from the junction corresponding to the bias voltage V_0 (μm)
- W_1 : Depth from the junction corresponding to the bias voltage V_1 (μm)
- R_s : The series resistance (Ω)
- R_{sh} . The shunt resistance ($1 \cdot E6$) (Ω)
- J_s : The reverse saturation current ($1 \cdot E-9$) (A/cm^2)
- N_T : Deep level trap concentration ($1 \cdot E14$) (cm^{-3})
- N_D : Concentration of shallow donor ($1 \cdot E15$) (cm^{-3})
- n : The ideality factor
- ϕ_b : Barrier height determined by $I(V)$ measurement (eV)
- V_b : Barrier height determined by $C(V)$ measurement (eV)
- %er: Percentage of error between V_b and $n \cdot \phi_b$.

For example, in table 5.8, in the first row, the values for R_s , R_{sh} , J_s , N_D , n , ϕ_b and V_b are given from the experimental characterization of a Schottky barrier discussed previously. The results are now put in tables. Thus in the first row and the first column of table 5.8, we may observe the apparent activation energy E_a (0.80eV) where its corresponding deep trap concentration can be found (in the same row). W_0 and W_1 correspond to the distance from the junction depth where the DLTS have been investigated in order to find N_T . For example, in the first row, at $V_0 = -5V$ and $V_1 = 0V$ we have the

TABLE 5.8: Results for sample R16

Sample R16		T _{subs} = 860.0 °C											
Thickness = 41.0 μm		N _D H = 8.15E15 at/cm ³						μ = 4760 cm ² /V-s					
E _a eV	W ₀ μm	W ₁ μm	R _s Ω	R _{sn} Ω	J _s A/cm ²	N _T at/cm ³	N _D at/cm ³	V ₀ Volt	V ₁ Volt	n	φ _b eV	V _b eV	%err V _b & n*φ _b
.80	1.534	0.620	30.4	140.	.626	0.417	03.69	-5	0	1.074	0.380	1.060	12.1
.72	1.534	0.620				0.631	03.69	-5	0				
.80	1.767	0.911				0.516	03.69	-7	-1				
.72	1.767	0.911				0.572	03.69	-7	-1				
.80	1.767	0.911				0.485	03.69	-7	-1				
.72	1.767	0.911				0.608	03.69	-7	-1				
.80	1.985	1.029	33.1	9.64	.907	0.394	02.93	-7	-1	1.095	0.347	0.950	02.4
.72	1.985	1.029				0.461	02.93	-7	-1				
.80	1.985	1.029				0.390	02.93	-7	-1				
.72	1.985	1.029				0.447	02.93	-7	-1				
.80	2.200	1.166	163	11.0	.861	0.749	0.361	-2	0	1.099	0.337	---	
.72	2.200	1.166				0.110	0.361	-2	0				
.80	3.470	2.450				0.622	1.061	-7	-3				
.72	3.470	2.450				0.097	1.061	-7	-3				

TABLE 5.9: Results for sample B46

Sample B46			Tsubs = 850.0 °C										
Thickness = 70.0 μm			N _D H = 5.11E16 at/cm ³				μ = 4150 cm ² /V-s						
E _a	W ₀	W ₁	R _s	R _{sn}	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						
30	0.535	0.230	4.33	2.39	99.0	01.13	32.10	-5	0	1.316	0.757	---	
72	0.535	0.230				---	32.10	-5	0				
30	0.663	0.416	5.47		34.6	01.27	27.26	-7	-2	1.310	0.768	---	
72	0.663	0.416				08.91	27.26	-7	-2				
30	0.353	0.237				0.806	73.90	-1	0	---	---	0.970	
72	0.353	0.237				12.40	73.90	-1	0				
30	1.116	1.035	6.27	13.2	1.07	2.655	40.70	-1	0	1.091	0.854	0.890	-4.5
72	1.116	1.035				12.30	40.70	-1	0				
30	1.395	1.186				01.16	40.70	-7	-2				
72	1.395	1.186				09.10	40.70	-7	-2				
30	2.475	2.363				0.786	79.20	-1	0	1.083	0.846	0.850	-7.2
72	2.475	2.363				6.420	79.20	-1	0				
30	2.737	2.475				0.551	79.20	-5	-1				
72	2.737	2.475				5.180	79.20	-5	-1				
30	3.365	3.410				---	22.00	-2	0	1.068	0.894	0.880	-7.8
72	3.465	3.410				4.761	22.00	-2	0				
30	3.465	3.465				---	22.00	-7	-2				
72	3.346	3.465				4.180	22.00	-7	-2				

TABLE 5.10: Results for sample B51

Sample B51		Tsub = 330.0 °C											
Thickness = 44.0 μm		N _D H = 6.90E16 at/cm ³						μ = 3940 cm ² V-s					
Ea eV	W ₀ μm	W ₁ μm	Rs Ω	Rsh Ω	Js A/cm ²	N _T at/cm ³	N _D at/cm ³	V ₀ Volt	V ₁ Volt	n	φ _b eV	V _b eV	Kerr V _b & n*φ _b
.80	0.670	0.267	3.61	10.9	53.1	0.292	18.20	-5	0	1.382	0.760	0.940	10.5
.72	0.670	0.267				---	18.20	-5	0				
.80	0.757	0.535				0.403	18.20	-7	-2				
.72	0.757	0.535				2.183	18.20	-7	-2				
.80	0.416	0.267				0.630	18.20	-1	0				
.72	0.416	0.267				2.270	18.20	-1	0				
.80	0.729	0.286	5.92	9.45	1.89	0.274	16.70	-5	0	1.314	0.786	0.910	11.9
.72	0.729	0.286				---	16.70	-5	0				
						---	13.30	-1	0	1.064	0.876	1.330	0.85
						---	13.30	-1	0				
.80	1.433	1.147				0.420	13.30	-7	0				
.72	1.433	1.147				0.229	13.30	-7	0				
.80	2.706	2.382	6.34	10.7	2.09	1.130	14.50	-2	0	1.025	0.911	---	
.72	2.706	2.382				---	14.50	-2	0				
.80						1.220	14.50	-7	-2				
.72						---	14.50	-7	-2				

corresponding depth as $W_0=1.534\mu\text{m}$ and $W_1=0.620\mu\text{m}$ respectively. Then, in the second row, for $E_a=0.72\text{eV}$, we may find the same distances (W_0 and W_1) for the same bias since both traps have been found on the same diode. It can be seen that other DLTS measurements have been performed at different bias on the same diode. For instance, for $E_a=0.8\text{eV}$ at $V_0=-7\text{V}$ and $V_1=-1\text{V}$ for two different DLTS measurements at those bias, we find $N_T=0.516 \text{ E14 cm}^{-3}$ and $N_T=0.485 \text{ E14 cm}^{-3}$ with 6.3% error between the two and similarly for $E_a=0.72\text{eV}$ we find $N_T=0.572 \text{ E14 cm}^{-3}$ and $N_T=0.608 \text{ E14 cm}^{-3}$ on the same diode with 6.3% error also. In appendix 1, we can find all the detailed values for all the DLTS experiments performed to all samples studied.

Note that, whenever R_s , R_{sh} , J_s , N_D , n , ϕ_b and V_b are appearing in a new row, this means that the following DLTS measurements have been made on another SKB but on the same epitaxial layer (for R16 in this case). When, a dotted line cuts the table horizontally, this means that an etch of about $1\mu\text{m}$ was made on the epitaxial layer of that sample. Thus in table 5.8, in the first row below the dotted line we have $V_0=-2\text{V}$ and $V_1=0\text{V}$ for a corresponding $W_0=1.2\mu\text{m}$ and $W_1=0.166\mu\text{m}$, but we have added $1\mu\text{m}$ to W_0 ($2.2\mu\text{m}$) and W_1 ($1.166\mu\text{m}$) since we are now investigating at $1\mu\text{m}$ deeper from the initial surface since we have etched the sample.

In summary, table R16 shows that the basic characteristics of the fabricated diodes were good since $n \leq 1.1$ and $\phi_b \geq 0.85\text{eV}$. With this in mind, we observe that as we go deeper from the junction in performing DLTS measurements. We find that EL2 ($E_a=0.8\text{eV}$) seems to remain constant whereas, the ELCS1 ($E_a=0.72$) tends to vanish. The same phenomena are observed in sample B46 (table 5.9) and sample B51 (table 5.10) but with

more etching steps. In section 5.5 we will show the curves from these data and discuss them.

5.4 n, I_0 , V_b , R_s and R_{sh} measurements

The values of n , I_0 , V_b , R_s and R_{sh} are also given in table I in appendix I. The diodes are usually checked first with the curve tracer but with no accuracy. This is a quick way to check if the fabricated diodes have a junction that can be exploited. The accurate method to find the above results is done by using the $I(V)$ measurement method as describe in section 3.2. A typical example of $I(V)$ measurement method is shown in figure 5.10 for $\ln(I)$ as function of the positive voltage applied. The accuracy of the measurement depends on

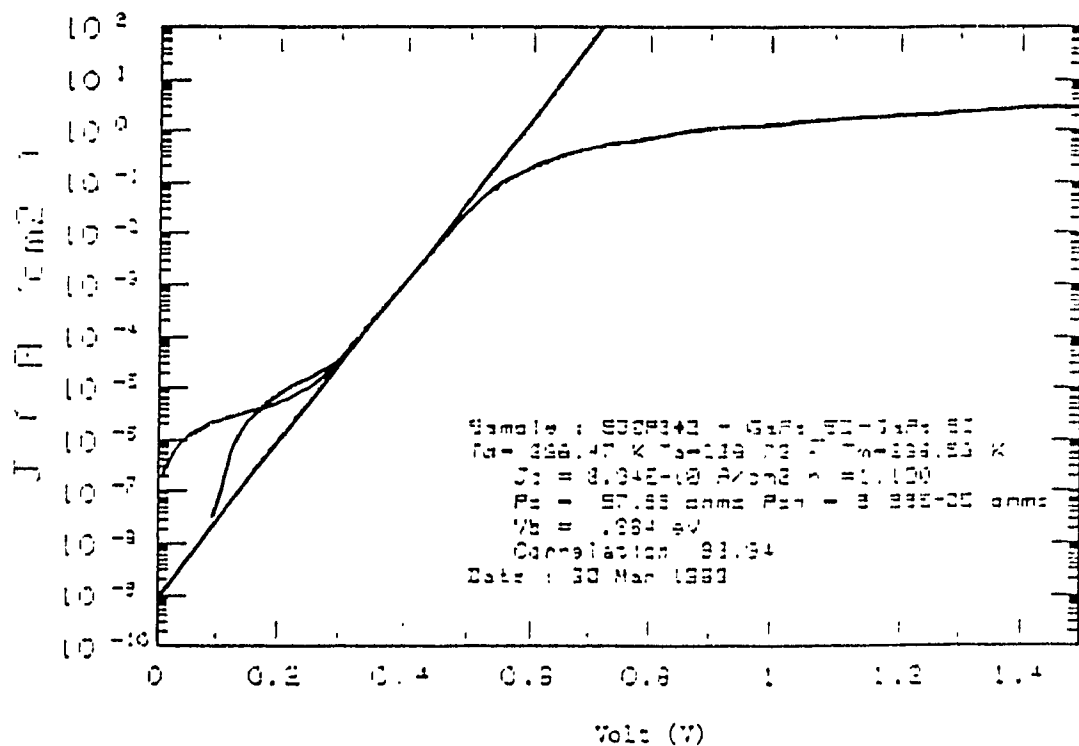


Fig. 5.10 An example of experimental curves of $\ln(I)$ vs V

the HP 3455A multi meter accuracy and the resistance R used to find I (see figure 3.6).

The resistance R used have an accuracy of 1% of the nominal value. The multi meter put in ohm-meter mode which reads the value of R chosen by the scanner has an accuracy of 0.0045% of reading +0.004% on high resolution mode (6 digits used) operated at $23^{\circ}\text{C} \pm 1^{\circ}\text{C}$ (S2). The multi meter in DC voltmeter mode which assign the voltage values on R has an input resistance R_{in} greater than $10^{10}\text{M}\Omega$ on 0.1V through 10V range. The accuracy of reading on 10V range on high resolution is $\pm 0.002\%$ of reading +0.0003%. Therefore, we can rely on the multi meter measurement because of its high accuracy performance when it is periodically calibrated. A removable reference module can be sent periodically for calibration (S2) to ensure the accuracy of the apparatus.

Here it can be observed from the tables in appendix I that we have fabricated good Schottky barriers for our analysis purposes since most of our diodes have an ideality factor n between 1.05 and 1.1. The values of R_s and R_{sh} varies from one sample to the other since we used an approximation method to find them. We require some approximating values for R_s and R_{sh} in order to have a good idea so as to see if there are in a reasonable expected range since we don't need them for further analysis as far as we are concerned.

5.4.1 Plots of N_D vs ϕ_b and J_s vs ϕ_b

From table I.1 in appendix I, it can be seen that ϕ_b is not always constant throughout the whole table. This depends partly on the free carrier concentration N_D . We recall from section 3.2.1 that the barrier height ϕ_b is lower by an amount $\Delta\phi_b$ due to the image force lowering. From equation 3.8, it is seen that $\Delta\phi_b$ is dependent on N_D . We note also that ϕ_b is also dependent on the work function ϕ_m . ϕ_m should remain constant since we are always using the Al-Pd metalization system on our Schottky barriers thus not altering ϕ_b very much.

As discussed in section 5.1, N_D may be different and not uniformly distributed in several samples; thus ϕ_b varies. We have plot the free carrier concentration N_D vs ϕ_b for samples series D369 through D378 in order to show their dependence. This is shown in figure 5.11.

It is observe that for low ϕ_b , N_D is large and for ϕ_b increasing N_D is decreasing. This means that $\Delta\phi_b$ is increased as N_D is increased, thus decreasing ϕ_b where ϕ_b is the height of the resultant barrier. This experimental plot is in agreement with the image force lowering theory explained in in appendix V and given in equation 3.8.

The dispersion between the points is about 0.6 decade. This may be caused by the non-uniformity in the doping. If N_D varies for different bias on the same sample ϕ_b will vary accordingly. Another probable cause of error is the surface area of the junction. ϕ_b is determine from equation 3.7; if there is a small change in S , it will induce a change in ϕ_b . A third probable cause of error would be due to some kind of contamination left on the sample surface when we where fabricating the diodes. It is very important that the surface be very cleaned. Unfortunately, we don't have a perfect control over it due to

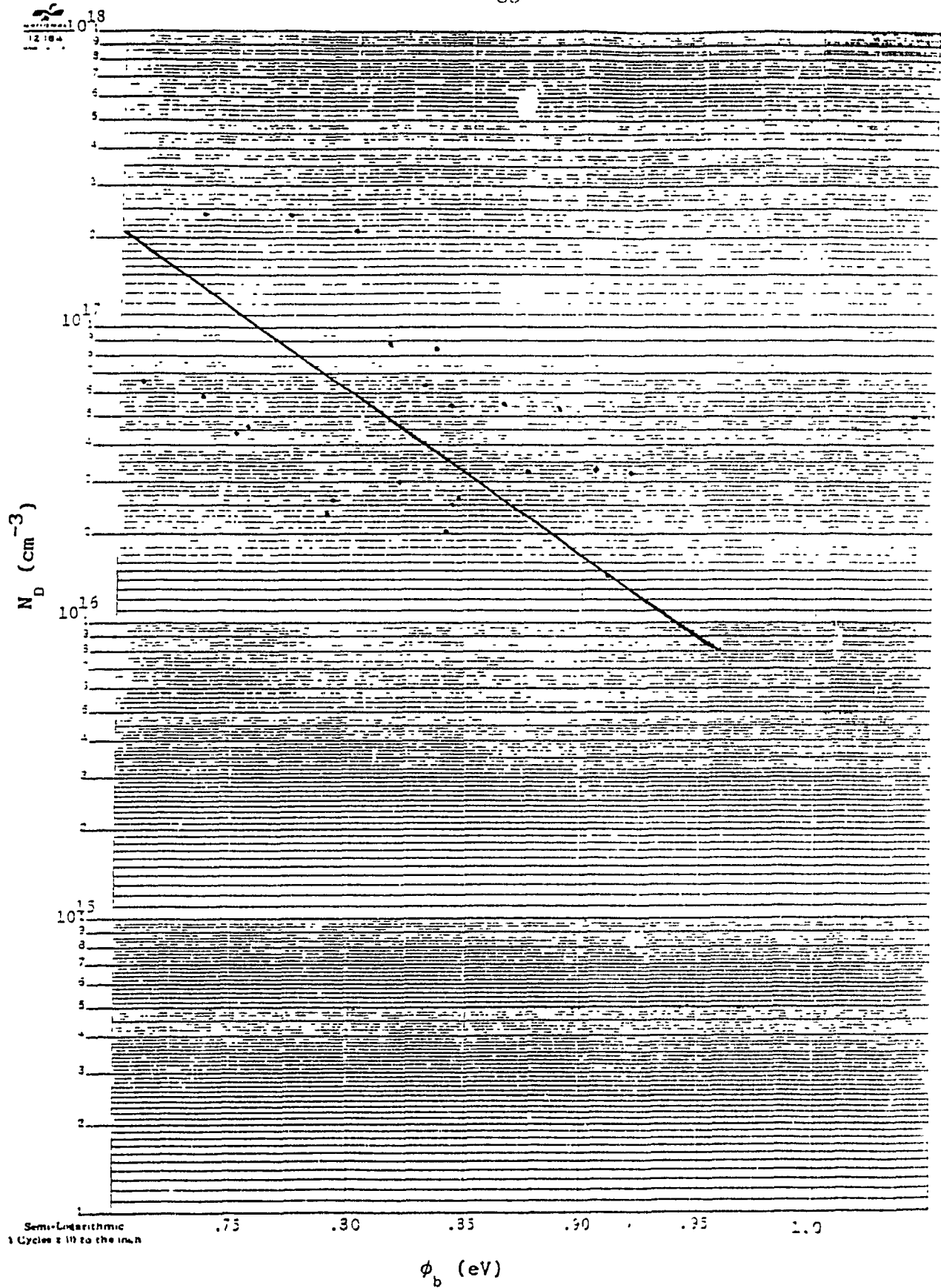


Fig. 5.11 Graph of N_D vs ϕ_b for samples D369 through D378

too many parameters variations during the fabrication of Schottky barrier diodes. If there is a layer in between the surface of the sample and the metal due to contamination, a voltage drop may occur across this layer (23)(83), thus lowering the initial value of ϕ_b regardless $\Delta\phi_b$. Therefore, if this layer varies in thickness, dispersion of points may occur.

Since ϕ_b varies, we have plot in figure 5.12 J_s ($J_s = I_0/S$) vs ϕ_b for the same set of sample in order to verify equation 3.7 experimentally. As ϕ_b is increased, J_s decreases which verifies this equation (22). Therefore, for each sample used, the characteristic of each diode is slightly different from one to another which is due to the change in N_D and the diode quality fabrication to which we have a good control on n but not as well on ϕ_b .

To show the dependence on other samples, we have plot N_D vs ϕ_b for samples series B39 to B60 as shown in figure 5.13. Due to a low variation in N_D for this set of samples, there is a low variation in ϕ_b . This leads to $\Delta\phi_b$ mostly constant for this set of sample. This is still in agreement with appendix V but with a slow decreasing slope. The plot of N_D vs ϕ_b is also shown in figure 5.14 for samples series R2 through R16. It shows some dependence but with a steeper negative slope within a small range in ϕ_b . Therefore N_D plays an important role in the determination of ϕ_b .

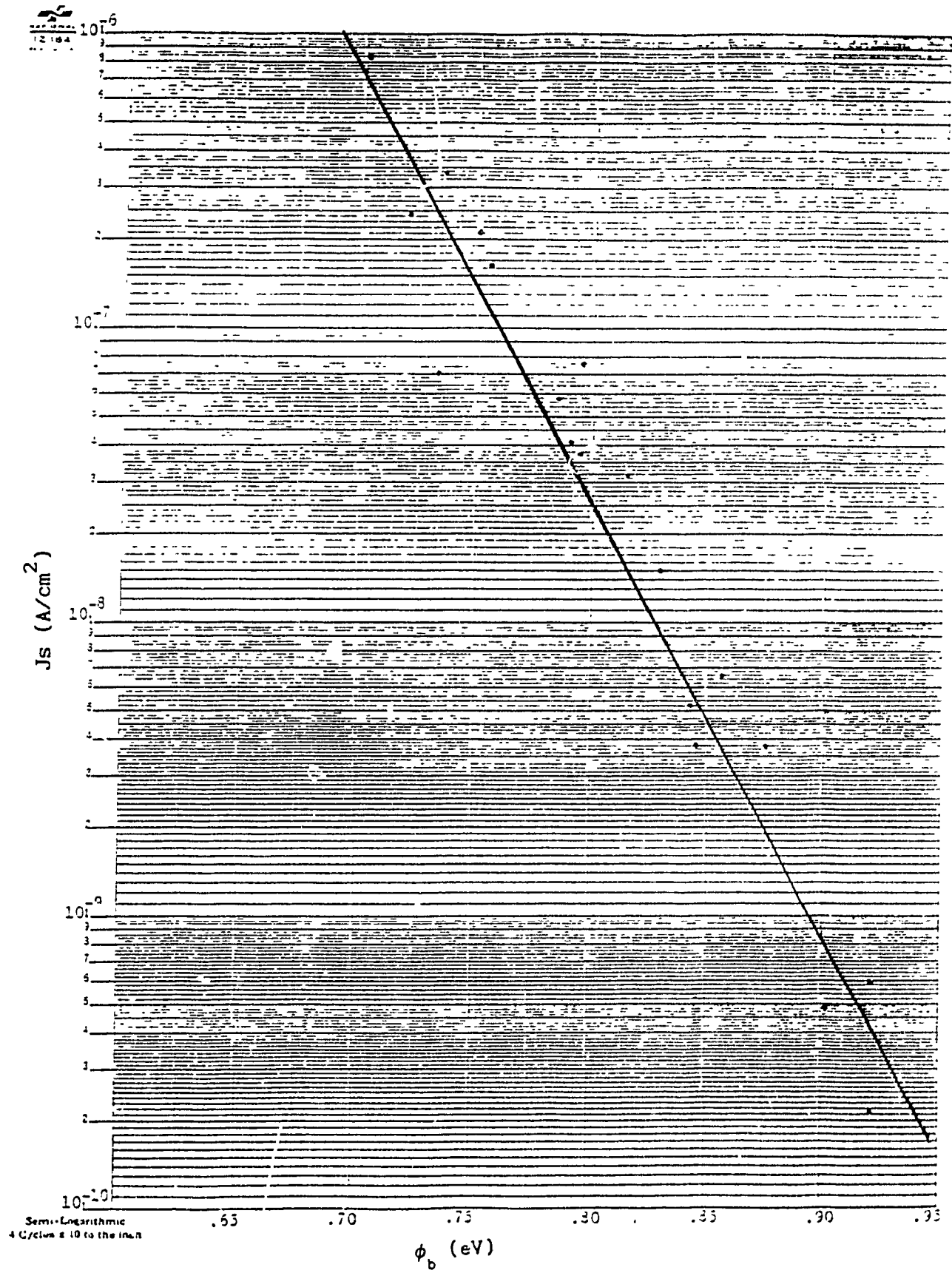


Fig. 5.12 Graph of J_s vs ϕ_b for samples D369 through D378

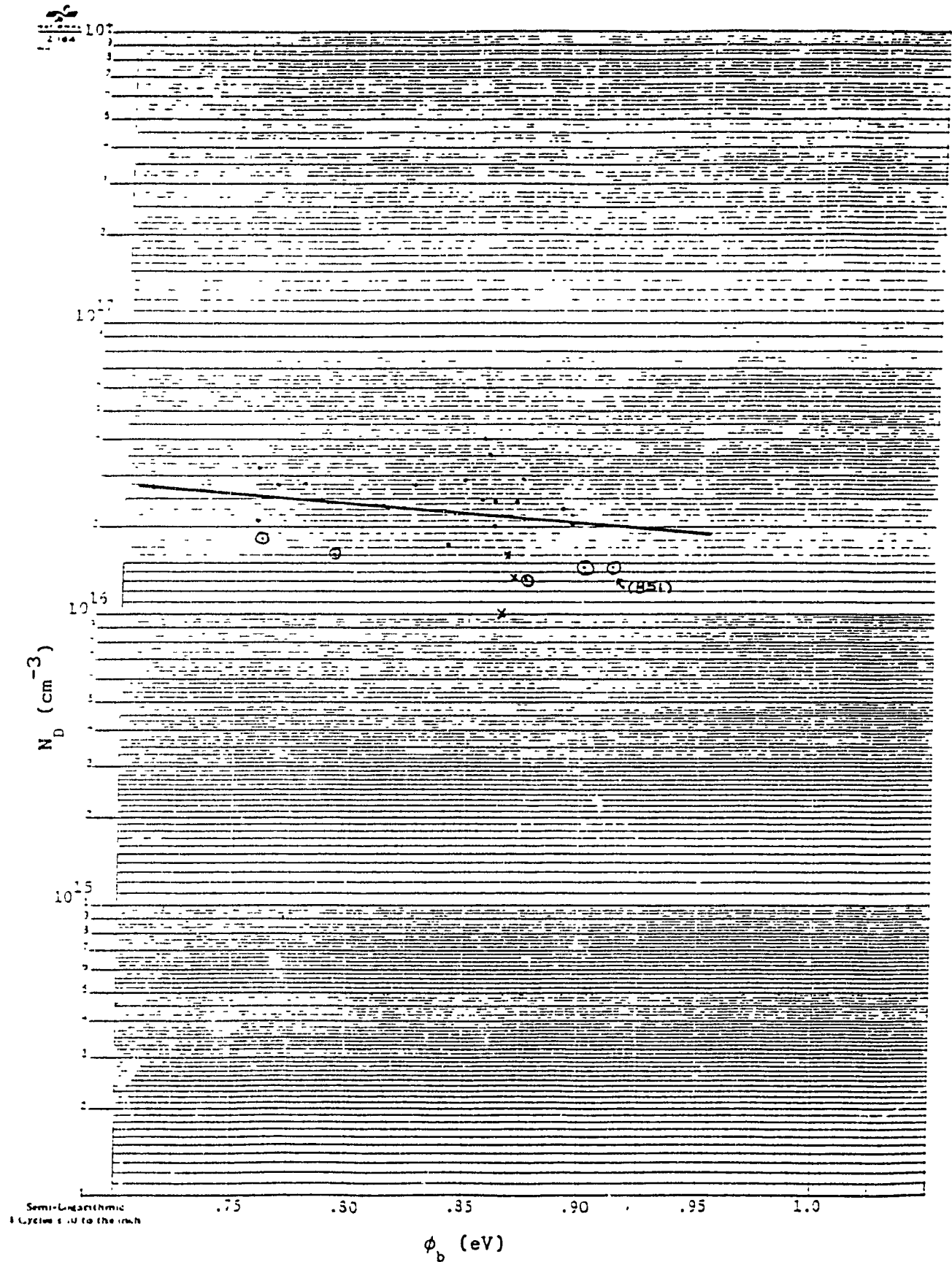


Fig. 5.13 Graph of N_D vs ϕ_b for samples B39 through B60

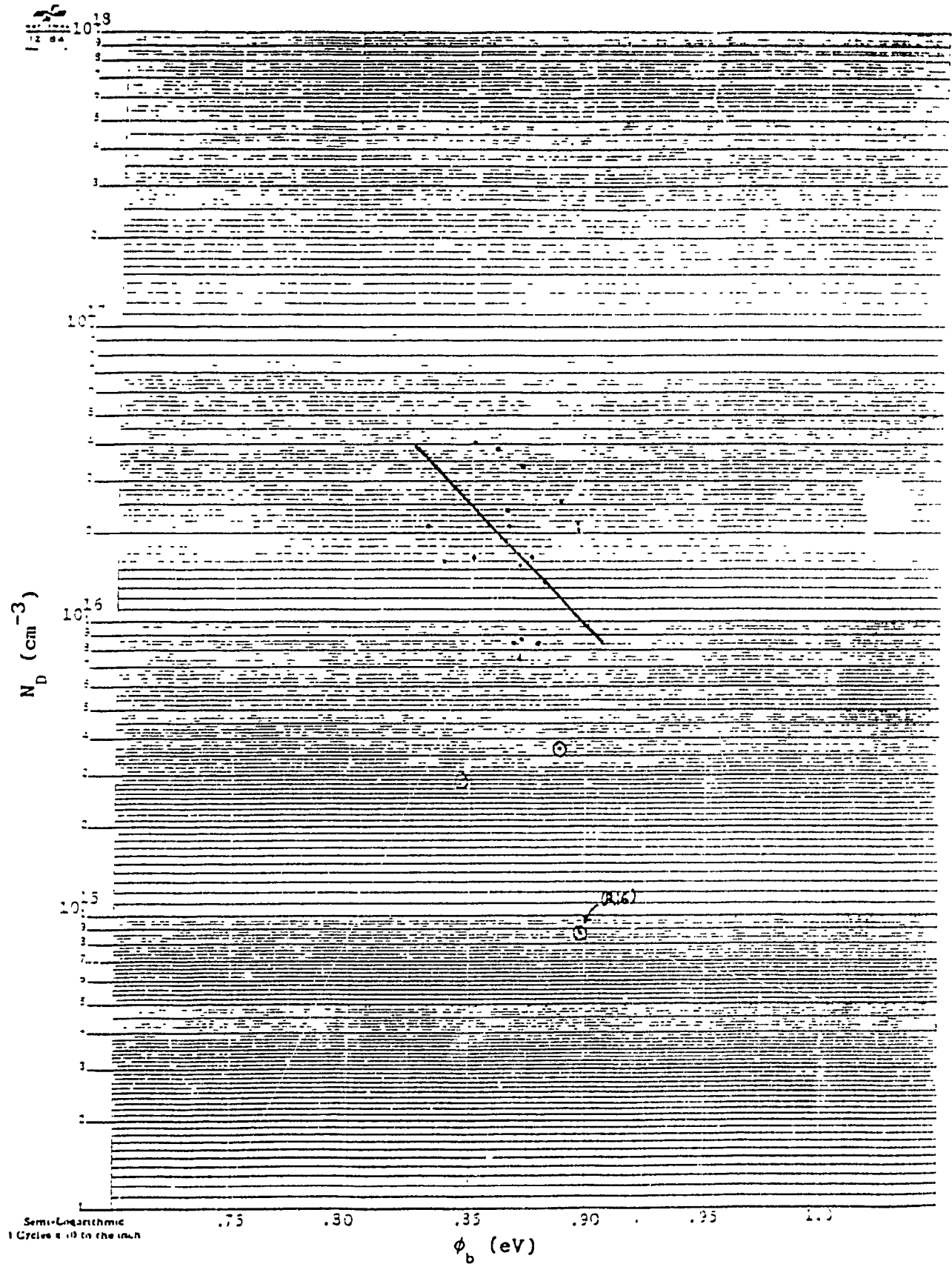


Fig. 5.14 Graph of N_D vs ϕ_b for samples R2 through R16

5.4.2 Plots of EL2 vs ϕ_b and ELCS1 vs ϕ_b

It is noticed that the DLTS signal for the mid gap level EL2 seems to be dependent on the Schottky barrier height ϕ_b for samples labeled R and B. Thus we have plot the concentration N_t for EL2 vs ϕ_b . This is shown in figure 5.15. That figure shows that the concentration N_t for EL2 is fairly constant for ϕ_b greater than 0.75eV regardless the point dispersions as discussed previously. As suggested by reference (22), for barrier height between 0.62 and 0.82eV, the observe DLTS signal intensity is function of ϕ_b ; consequently the deduced concentration of EL2 level become unreliable. However, in our case, the EL2 deep level donor trap concentration was not affected much by the change in ϕ_b as the graph shows, leading to its proper measurement. The few points left on the right hand side bottom where the EL2 is seen at a lower concentration are found in samples R10 and B42. In sub section 5.5.1 we will discuss a proposed model for the EL2 donor trap level that will give us some indication for its change in concentration in the material.

Figure 5.16 shows the curve for $N_t(\text{ELCS1})$ vs ϕ_b for samples labeled R and B. Note here that we have taken $N_t(\text{ELCS1})$ at the surface of the samples only; that is no $N_t(\text{ELCS1})$ after an etch are given on the graph. From the results given in table IX.1, it can be seen that after one etch of about one μm at a time, $N_t(\text{ELCS1})$ decreases even if ϕ_b is increasing. We have plot $N_t(\text{ELCS1})$ vs ϕ_b for all other samples and they show similar results as the one shown in figure 5.16. Thus for this trap (figure 5.16), we notice that $N_t(\text{ELCS1})$ seems to be dependent on ϕ_b . This is observed between 0.75 to 0.90eV. Therefore, it seems that the measurement of the trap concentration N_t for ELCS1

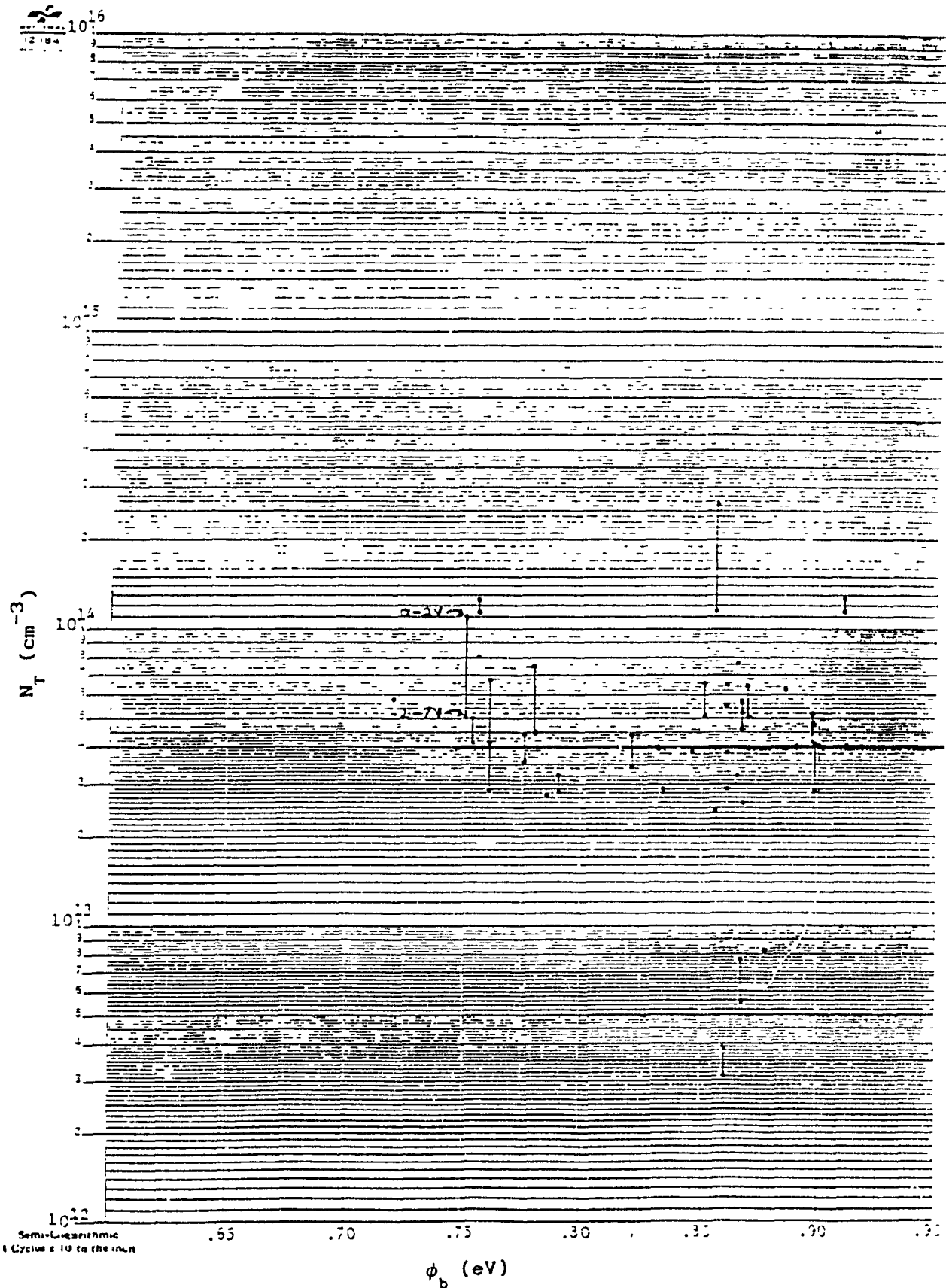


Fig. 5.15 Graph of $N_T(\text{EL2})$ vs ϕ_b for samples R and B series

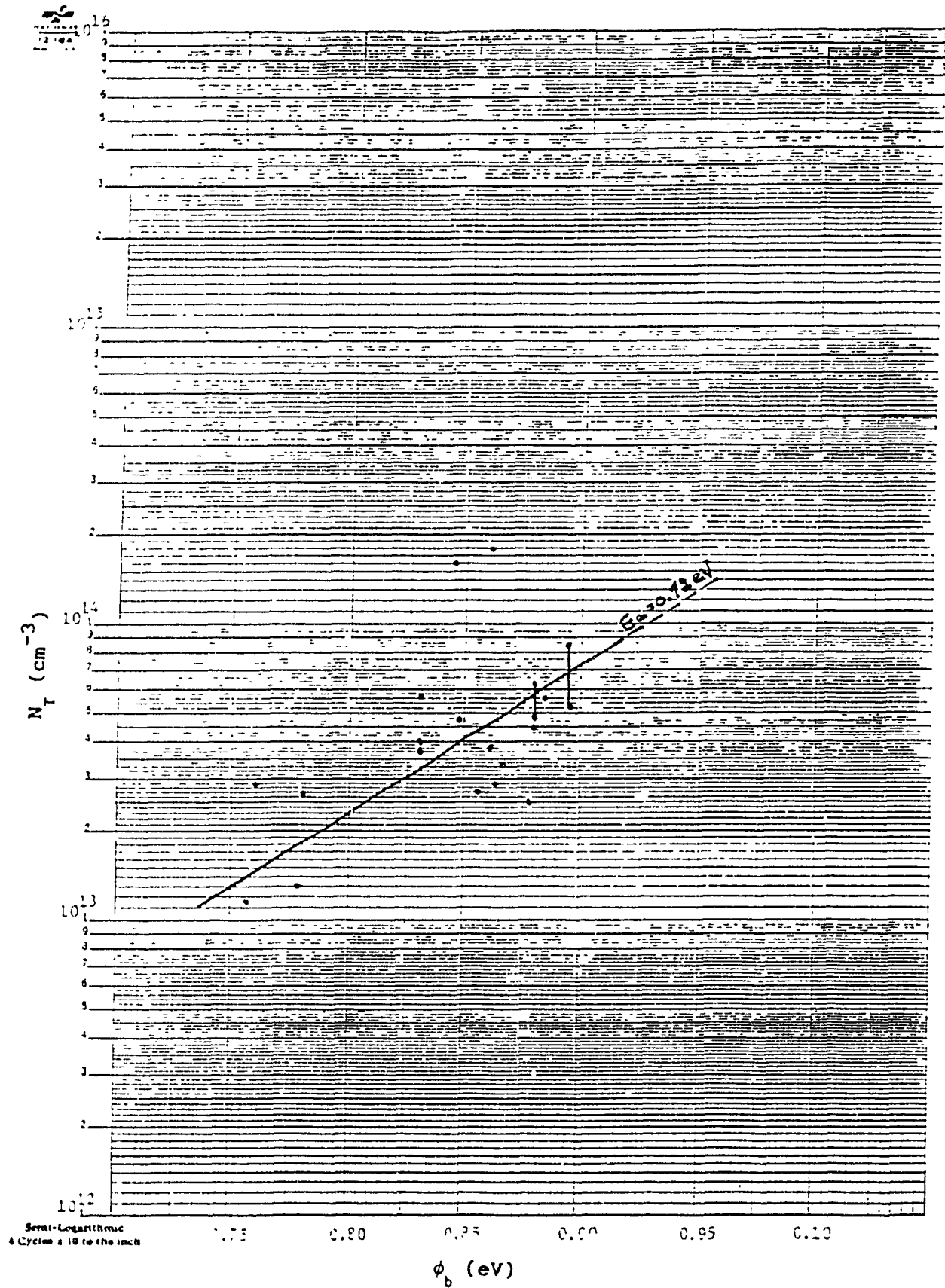


Fig. 5.16 Graph of $N_T(\text{ELCS1})$ vs ϕ_b for samples R and B series

varies linearly within one decade for $0.75\text{eV} < \phi_b < 0.90\text{eV}$ whereas the measurement of N_T for EL2 seems to be independent of ϕ_b as discussed above knowing that ϕ_b lies within this range.

5.4.3 Comparison for V_b from $C(V)$ and for ϕ_b from $I(V)$ measurement

We have stated in section 3.2.4 that the barrier height determined by the $I(V)$ measurement could be close to one determined from the $C(V)$ measurement if the former is multiplied by the ideality factor n . In order to verify it we have taken the percentage of error for all barrier height involving V_b and ϕ_b available in table IX.1.

For eight samples (series AL, AS and AU) available studied in Montpellier France we have compared the barrier heights as follows; for example, for sample (AS40MEP14,4), $\phi_b = 0.785\text{eV}$, $n = 1.265$, $V_b = 0.97$; therefore $V_b' = 0.785 * 1.265 = 0.993\text{eV}$. The percentage of error between V_b and V_b' is 2.3%. We have thus calculated each percentage of error for all samples with ϕ_b and V_b available and we have made the average. Thus we found that the above statement is true but with a 12.7% of error.

We have checked with fourteen samples in the series D369 through D379 (table 5.11) and, S29E and S30R (table 5.15) studied in Montréal and we have found an average error between V_b and V_b' of 11.3%. The reasons for having V_b and ϕ_b different was stated in section 3.2.4.

The reason for correcting ϕ_b by a factor n can be seen by the fact that equation 3.7 does not take n into account. References (84) and (85) suggest that n should be included in the expression for the saturation current I_0 since the effects which cause the deviation from n equal to unity at higher bias voltage are also present at zero bias. Thus equation 3.7 can be rewritten as

$$I_0 = SA^* T^2 e^{(-\phi_b/nkT)} \quad (5.1)$$

where

$$\phi_b' = n\phi_b = (nkT/q) \ln(A^* ST^2/I_0) \quad (5.2)$$

The average 10% of error between V_b and V_b' is probably due to the fact that V_b is taken on the x axis from the $1/C(V)^2$ plot. As discussed previously, if points P1 and P2 are not properly chosen, it may induce a small variation in the slope of the linear fit thus changing the value of V_b (section 3.1.2).

5.5 Experimental Observations on EL2 and ELCS1 Traps

In samples R16, B46 and B51, we have studied the as-grown epitaxial layer grown by CSVT, by removing about $1\mu m$ layer one step at the time from the surface by chemical etching. The chemical etching solution was made from $H_2SO_4-H_2O_2-H_2O$ (5:1:1) and was used at $60^\circ C$.

Figure 5.17 shows two DLTS spectra of the CSVT epitaxial layers. We have chosen sample R16 (substrate temperature $T_s = 860^\circ C$) since it represents well the two main traps found in section 5.2.1. In figure 5.17a, we recognize the trap at 300K (ELCS1) and the trap at 335K (EL2) with both the emission rate at 0.39s for Schottky barriers made on the as-grown surface. Figure 5.17b was obtained by the DLTS measurement after a removal of about $1\mu m$ from the surface. It is noticed from the figure that the EL2 trap level remains the same even after a chemical etching whereas the other trap level decreases to a negligible amount.

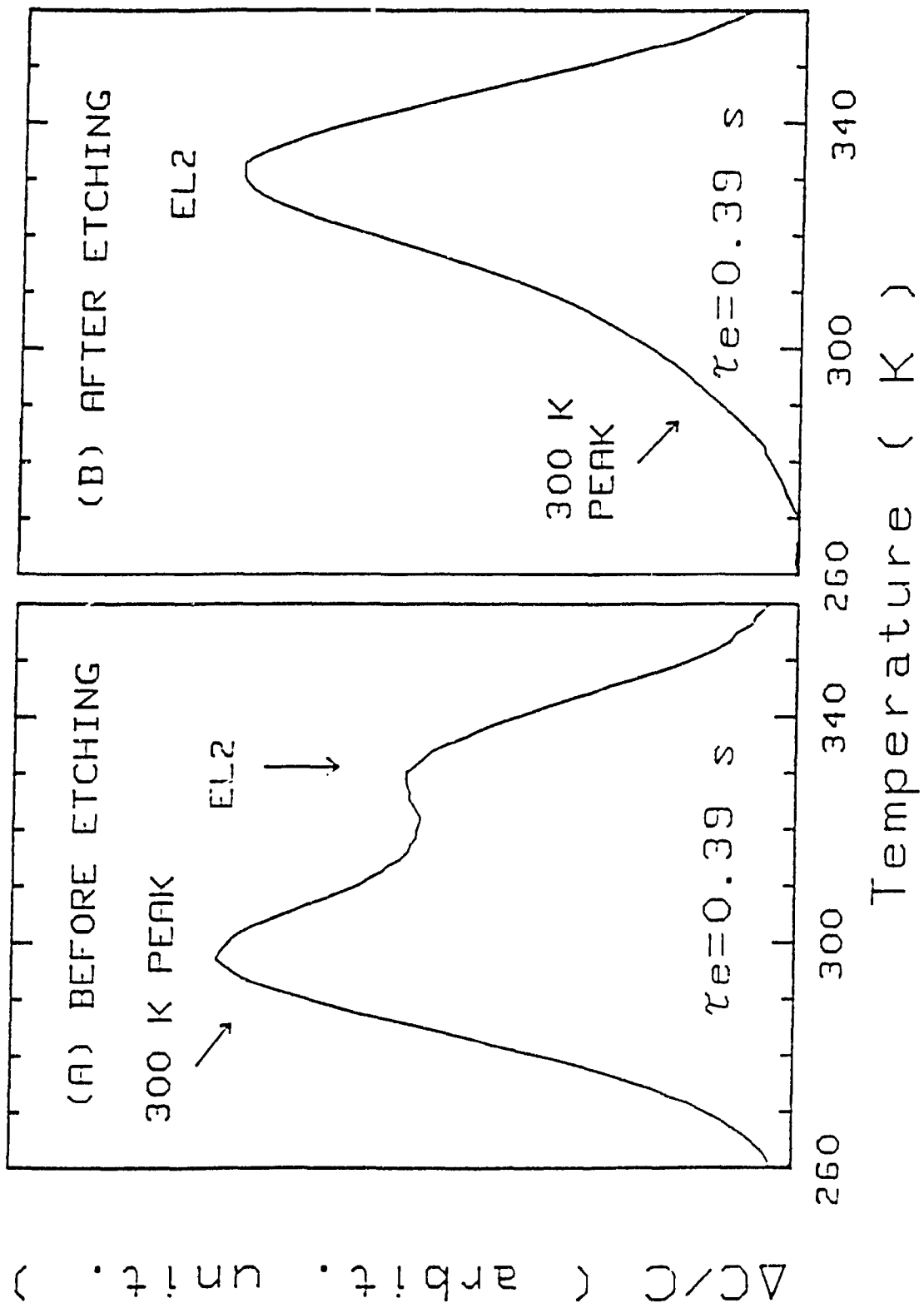


Fig. 5.17 DLTS spectra of the CSVT epitaxial layers.

In order to verify further the depth profile of the concentrations of these two traps, we have plot their concentrations N_r as function of the distance from the junction. Different bias conditions and progressive chemical etching depths were used in the DLTS scans. Figures 5.18, 5.19 and 5.20 show the results for samples R16, B46 ($T_s=850K$) and B51 ($T_s=880K$) respectively. The lines linking the two points corresponding to W_0 and W_1 represent the zones investigated during the DLTS scan after every chemical etching step. It can be seen for the three cases, that while the EL2 trap concentration remains constant in the bulk, the density of the ELCS1 trap decreases with depth in the epitaxial layer. Further investigations in sample B48 and B50 shows that after a chemical etch of about $5\mu m$ to both samples, the trap concentration N_r for ELCS1 is not seen whereas the trap concentration N_r for EL2 is about $3.8 \times 10^{13} \text{ cm}^{-3}$.

The trap concentration of the DLTS signal for ELCS1 from the above samples studied varies approximately between 2×10^{13} to $2 \times 10^{14} \text{ cm}^{-3}$. However, it noticed that the ELCS1 diminishes closer to the as-grown surface with increasing deposition temperature. This is shown in figure 5.21 were we have plot the concentration N_r for ELCS1 as function of the substrate temperature.

Figure 5.22 shows the variation of the measured EL2 concentration as function of the substrate temperature. It is observed that the variation of its concentration is approximately between 1.0×10^{13} to $1.3 \times 10^{14} \text{ cm}^{-3}$. This comparable with those already reported in other epitaxial growth technique such as VPE and OMVPE, where arsenic pressure is taken into account (S6). A monotonic increase of the EL2 concentration from 750 to 850°C deposition temperatures is observed.

Above 850°C a decreasing tendency can be seen.

In order to verify if the values of the shallow donor concentration had an effect on the EL2 trap concentration, we have plot N_D as function of the substrate temperature $\{N_T(T)\}$. This plot is shown in figure 5.23 for samples series labeled with R and B. It is observe that the free carrier concentration $N_D(T)$ is fairly constant regardless sample R16 to which has a low free carrier concentration N_D . This leads us to believe, with the help of equation 4.30, that the the trap concentration as function of substrate temperature $N_T(T)$ is not influenced by $N_D(T)$ and should not be influenced by the term in the bracket since it is usually very small (56). Therefore $N_T(T)$ depends on the maximum DLTS peak $S(T_M)$ measured from experimentation.

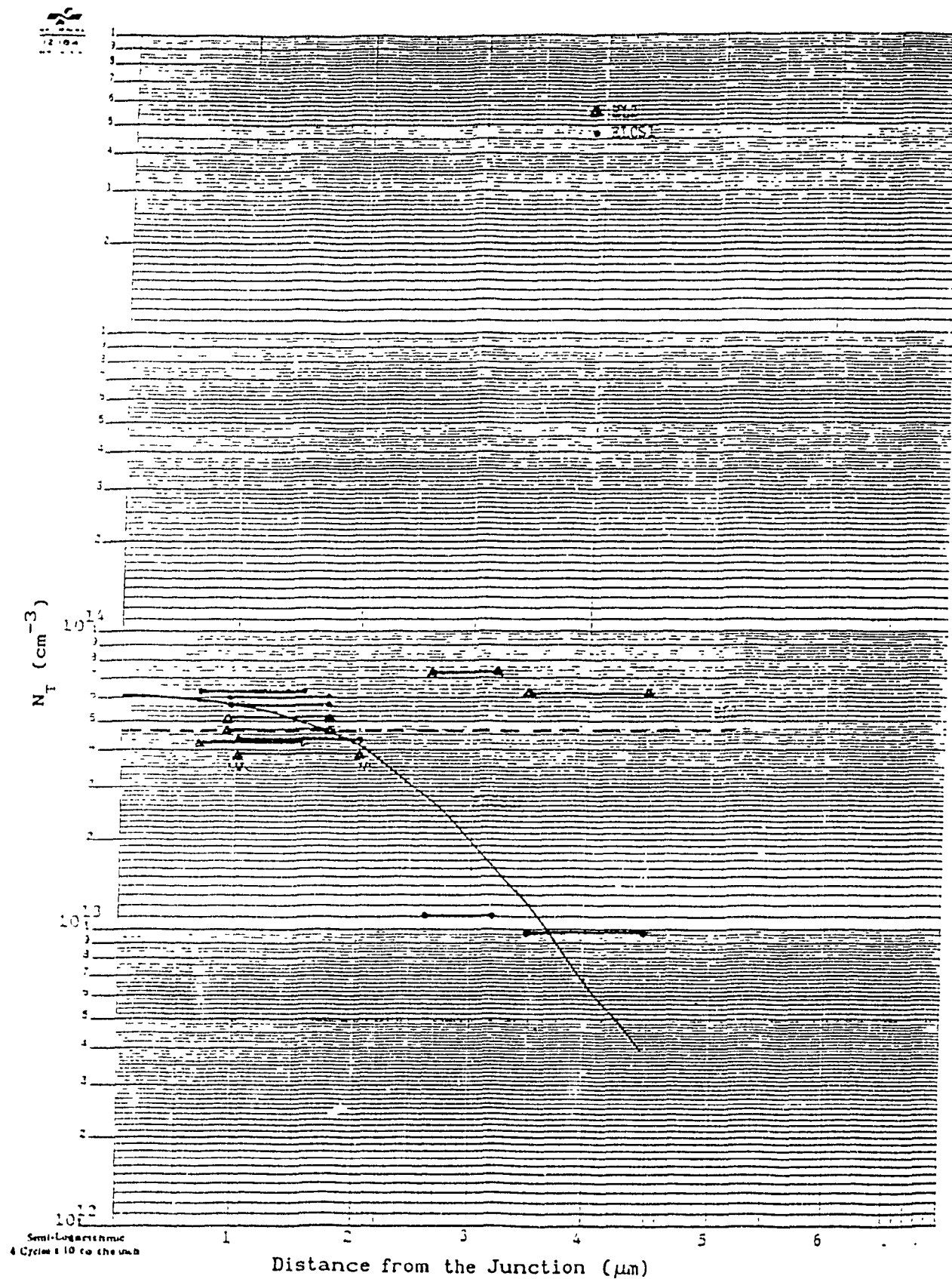


Fig. 5.18 Graph of N_T vs the distance from the junction (sample R16)

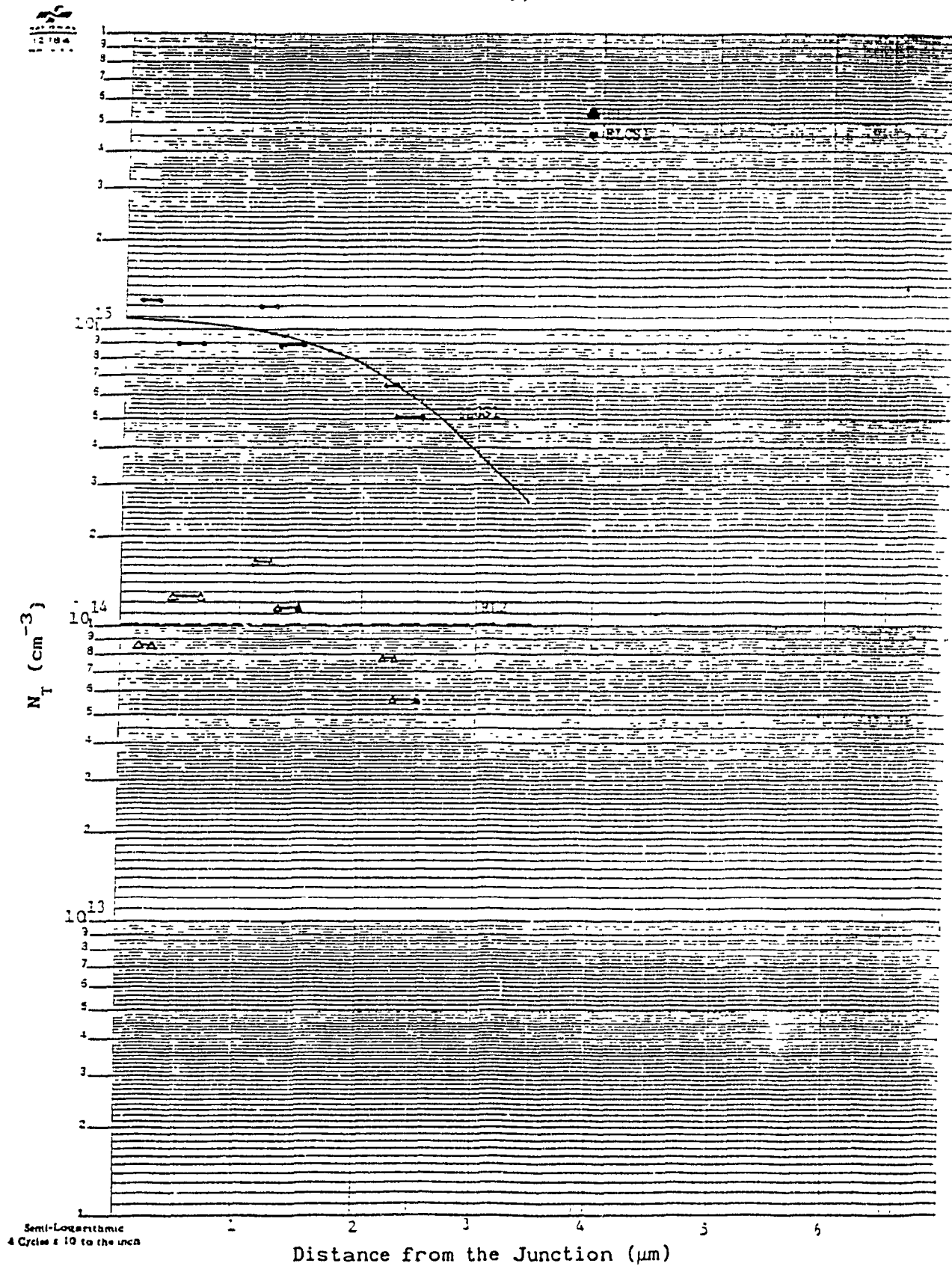


Fig. 5.19 Graph of N_T vs the distance from the junction (sample B46)

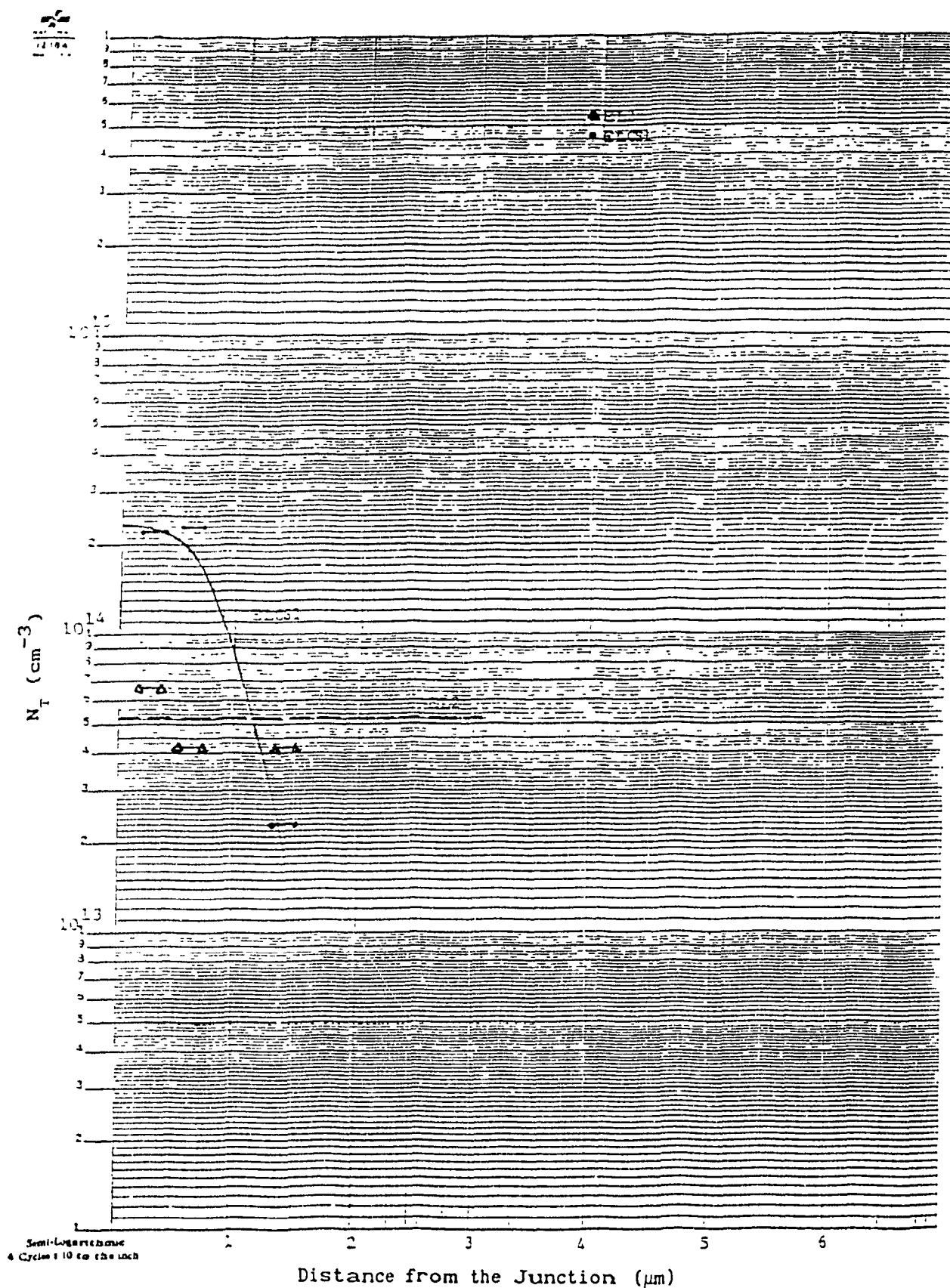


Fig. 5.20 Graph of N_T vs the distance from the junction (sample B51)

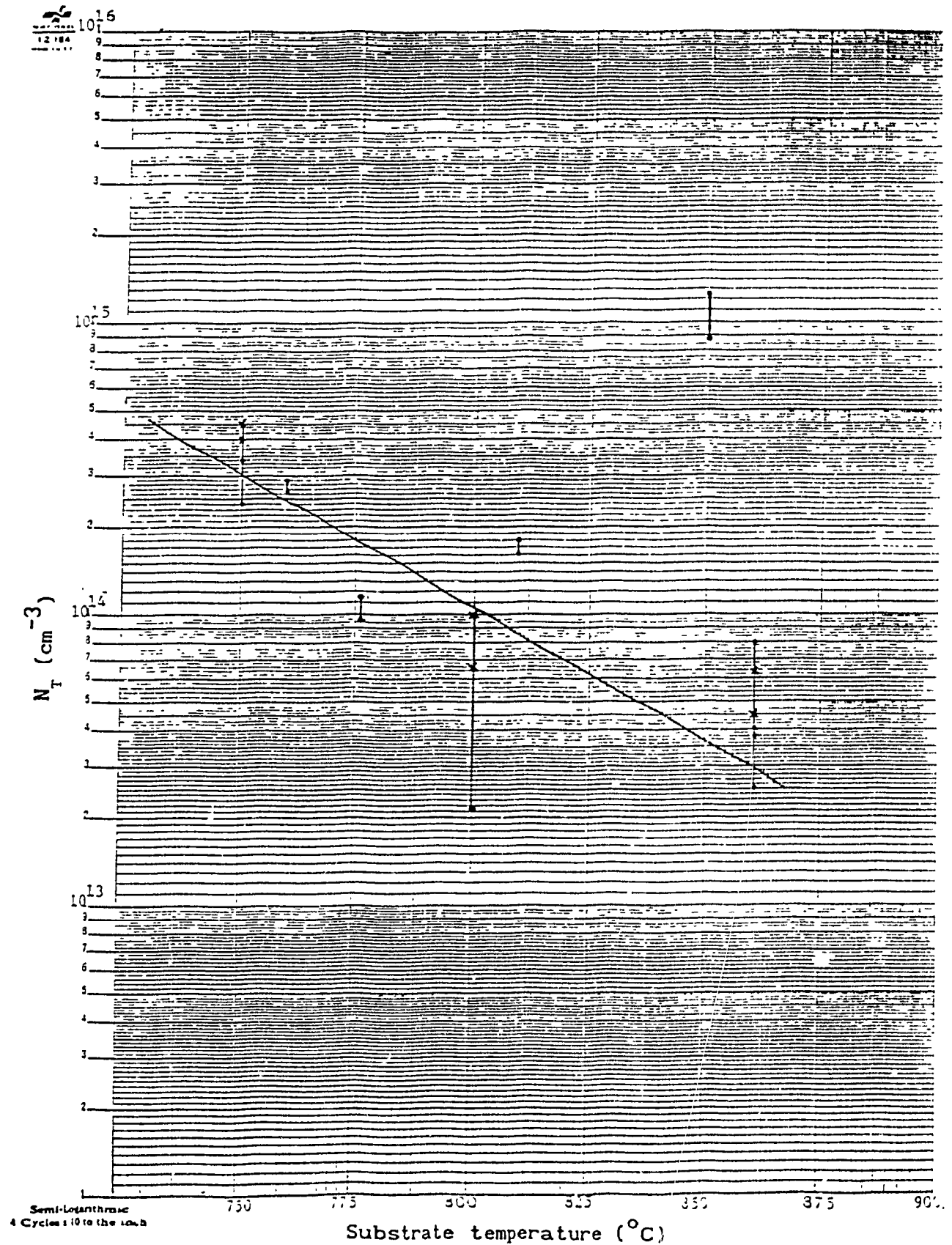


Fig. 5.21 Graph of N_T (ELCS1) vs the substrate temp. (series R & B)

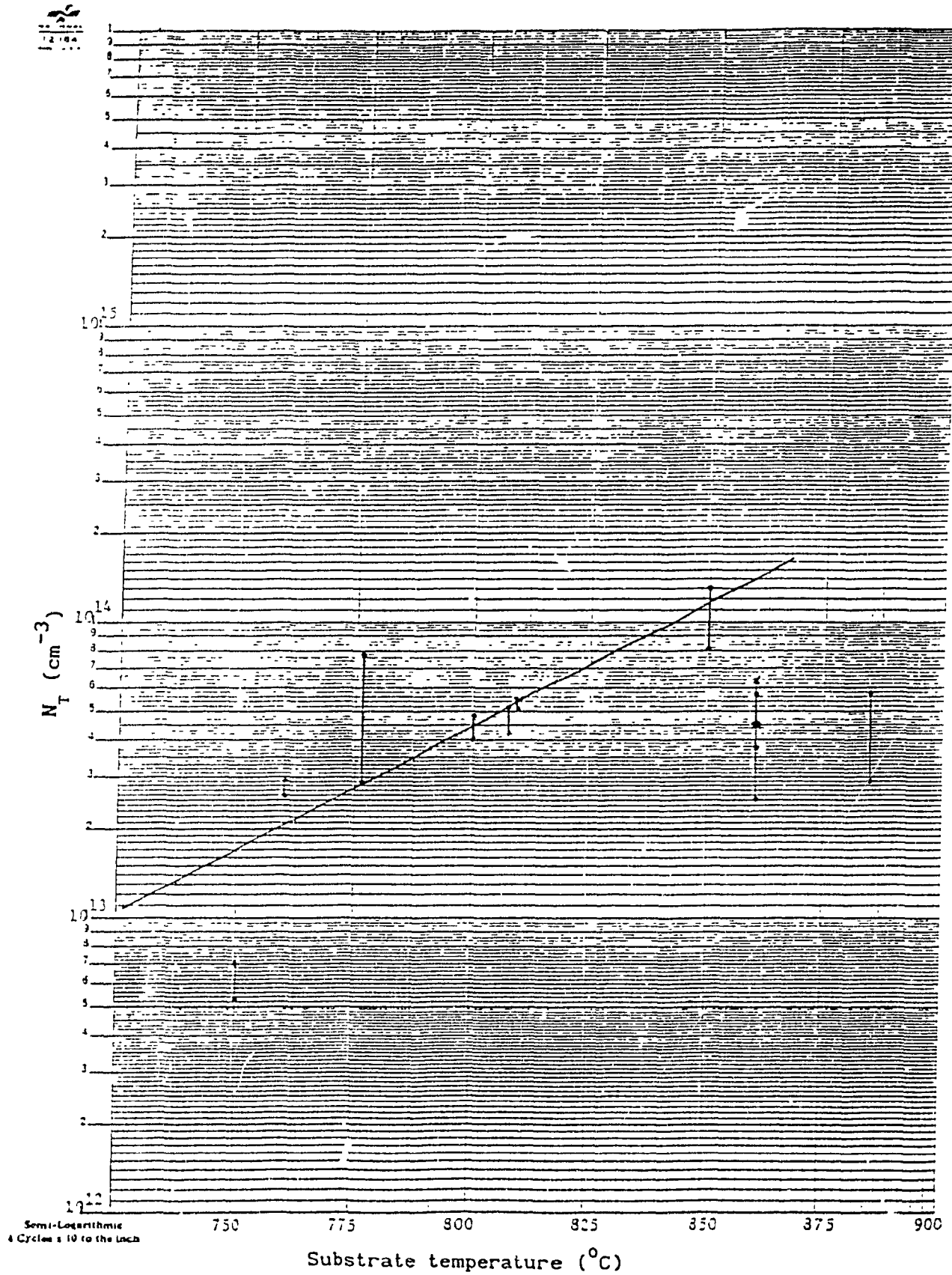


Fig. 5.22 Graph of N_T (EL2) vs the substrate temp. (series R & B)

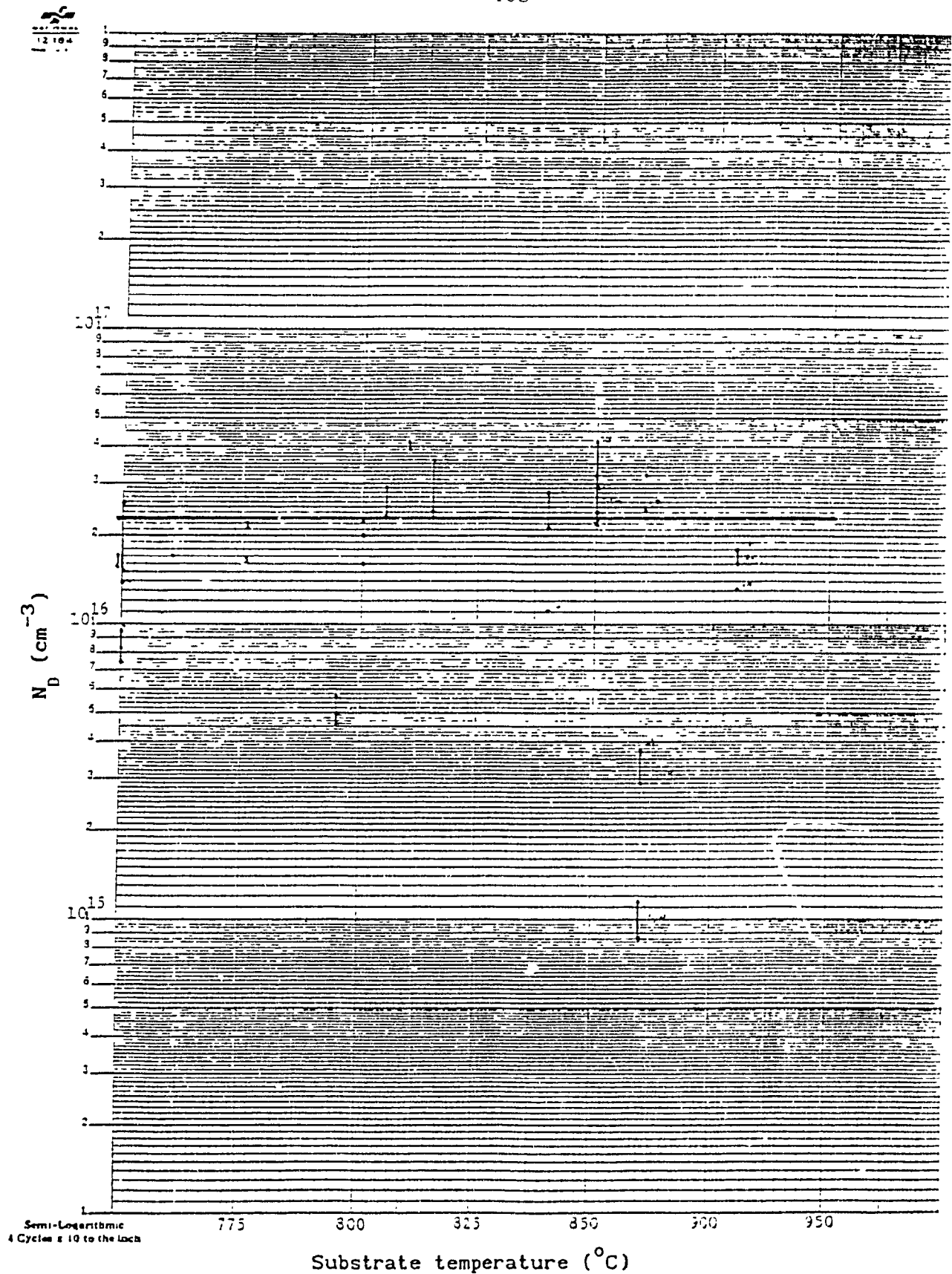


Fig. 5.23 Graph of N_D vs the substrate temp. (series R & B)

5.5.1 Proposed model for EL2 deep donor trap

In order to investigate further the above observations, we discuss first the EL2 model proposed by references (87)(88) and (89), which suggests that EL2 is formed by a complex of gallium vacancies V_{Ga} in As-rich conditions, and anti sites centers formed by the occupation of a gallium vacancy by an arsenic atom of GaAs host lattice leaving behind an arsenic vacancy V_{As} . This is represented in figure 5.24 (89). This figure shows the formation of the so called EL2 complex ($As_{Ga} + V_{As}$). Other authors also agree with the origin of the EL2 complex (65)(90)(91)(92). In figure 5.24a, the gallium vacancy V_{Ga} is shown and in b the complex is represented after the migration of an As atom in V_{Ga} .

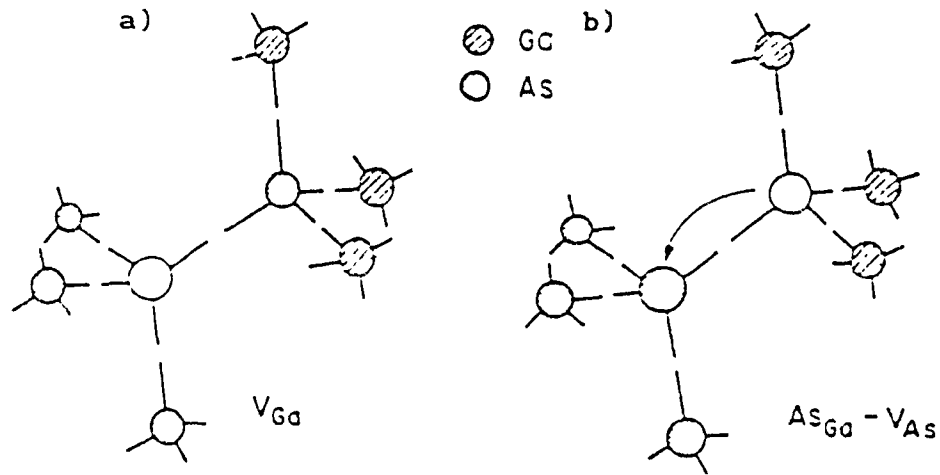


Fig. 5.24 Formation for EL2 complex

The EL2 complex is assumed to be a divalent deep lying donor center and a shallow monovalent donor level (87). This can be explained by the electronic configurations for atoms in the ground state and in the tetrahedral coordination system. For GaAs, the gallium has the configuration; Ga: $[Ar]3d^{10}4s^24p^1$ meaning that there are three electrons in the 4s and 4p sub shells whereas arsenic has the

configuration; As: $[\text{Ar}]3d^{10}4s^24p^3$ showing five electrons on the 4s and 4p sub shells (93). When one atom of Ga and one atom of As are brought together to form GaAs crystal, eight electrons are present on the 4s4p sub shells completing the octet, thus forming the semiconductor's predominantly covalent bonds. As shown in figure 5.25a, if a gallium is removed from its site, thus leaving a gallium vacancy V_{Ga} , V_{Ga} will be surrounded by five electrons belonging to the four neighboring arsenic atoms. Now, as shown in figure 5.25b, if a neutral arsenic atom with its five valence electrons occupies the gallium to form an anti site complex, the result may be a site possessing ten electrons. Since eight electrons complete the octet for tetrahedral coordination, two free electrons are left in excess. These excess electrons are thus responsible for the origin of divalent deep trap lying EL2 donor center (87). Note that the arsenic vacancy V_{As} left behind becomes a monovalent donor.

The energy of activation E_a of the EL2 complex has been suggested in the literature (65)(78) to be 25meV and 760meV for the shallow donor (V_{As}) and for the deep divalent donor anti site As_{Ga} respectively.

In order to allow the presence of a general shallow donor of variable concentration, silicon doping is introduced during GaAs crystal growth (87). It has been shown previously that silicon (Si) is an amphoteric impurity in GaAs (94) but because of our stoichiometric conditions (As-rich condition), it is reasonable to assume that the silicon acts as a shallow donor on the gallium sub lattice Si_{Ga} (94) (95). The presence of silicon as a shallow donor has an activation energy E_a equal to 0.002eV (21). Note here that Si can be introduced involuntary due to the presence of Si in the system, or purposely added

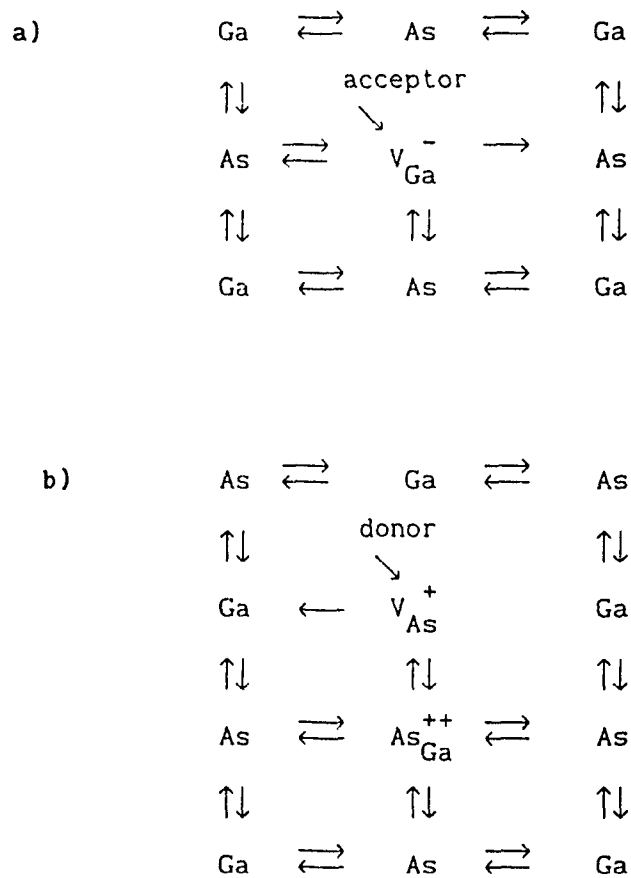


Fig. 5.25 Representation of EL2 formation

a) Gallium vacancy

b) Arsenic vacancy and arsenic
in site Gallium

for adjustable concentrations.

Now, by varying the Si shallow donor concentration impurity in GaAs, the material may be considered as n-type, semi-insulating or semi-conducting (21)(87) by compensation of the deep acceptor present in the GaAs crystal. This can be explained with the help of the diagram shown in figure 5.26.

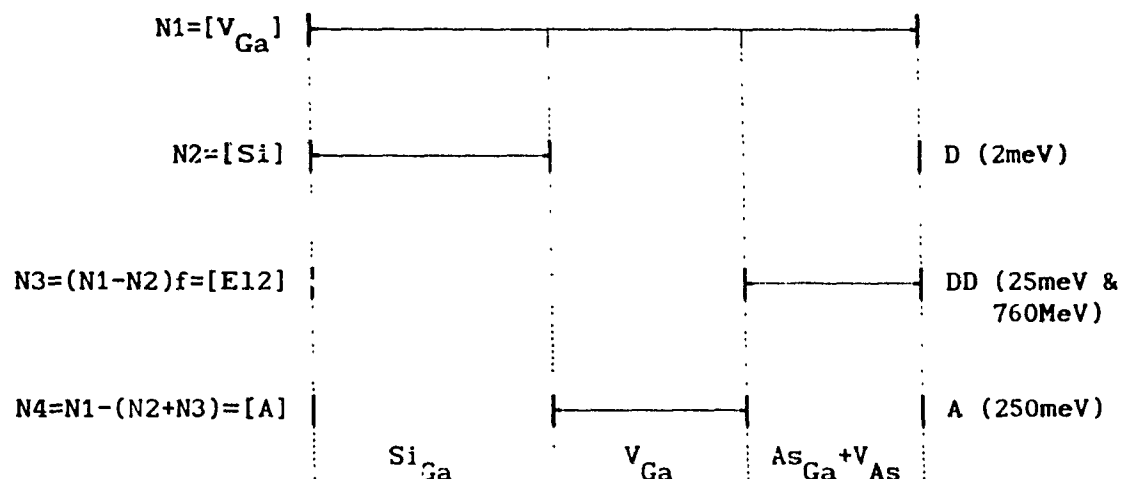


Fig 5.26 Diagram for compensation in GaAs crystal

The above figure suggests that $N1$ is the total concentration of Gallium vacancy V_{Ga} . The total V_{Ga} concentration is due to the fact that the crystal is grown in As-rich conditions (off-stoichiometric condition: As/Ga ratio greater but close to one)⁴. For example, it has been shown previously that the existing phase extent in GaAs containing approximately 2.22×10^{22} atoms/cm³ (96), of the limiting composition of the arsenic-rich side of its $Ga_{49.999}As_{50.001}$ (off-stoichiometry) correspond to $N1 = 3 \times 10^{17}$ atoms/cm³ corresponding to a maximum V_{Ga} (21) (87). Then, $N2$ is the concentration of Si shallow donor introduced in the crystal. $N3$ is the concentration of the EL2 in the crystal and is formed with the gallium vacancy concentration available ($N1 - N2$) for the formation of anti sites (As_{Ga}) assuming that a fraction f of these unfilled gallium vacancies become occupied by arsenic atoms resulting in V_{As} . The fraction f was calculated with the thermodynamics

⁴ Pure stoichiometry if As/Ga = 1

expressions found in references (5)(62) and (87), and was given as 0.15. Finally, N_4 represents the concentration of gallium vacancy (V_{Ga}) which are left unoccupied by either silicon or arsenic atoms. Therefore, the deep acceptor concentration $[A]$ available to compensate the donors present in As-rich GaAs crystal is given by N_4 .

With the help of the above figure, we can explain the behavior of EL2 by varying the stoichiometry with the temperature of a GaAs crystal during its growth or by doping it with Si. For instance, according to the above diagram, if we assume that the concentration of Si remains constant (N_2 constant), and during the post growth of the crystal, the As/Ga ratio has increased, more gallium vacancies V_{Ga} are formed. Since there is more V_{Ga} , more arsenic can take place in these, thus increasing the probability of an As in Ga site (As_{Ga}) with an arsenic vacancy V_{As} . Therefore, it follows for this case, that the EL2 deep donor trap in the bulk will increase in concentration since $(As_{Ga} + V_{As})$ will increase in concentration.

Now, if we vary the concentration of silicon, it is possible to obtain a semi-insulating GaAs crystal. According to the diagram, by introducing Si as donor impurity, it will influence the EL2 donor trap concentration. If both EL2 (N_3) and Si (N_2) as donors are in concentration near to the deep acceptor V_{Ga} it will compensate to give an SI material (87). The calculation of the Fermi level in order to show whether it is n-type, SI-type or semi-conducting type where shown in references (62) and (87) by using the Schottky curves. Note here that the silicon concentration influences the EL2 concentration the following way: if more Si are introduced in the GaAs crystal, more gallium vacancies will probably be occupied by Si thus forming an anti

site Si_{Ga} . This phenomenon will possibly live less gallium vacancies V_{Ga} , there will be less As_{Ga} for the formation of EL2 leading to its lower concentration (21)(87).

From our results obtained, we recall that in sample R16 for example, we were able to see the EL2 clearly after a DLTS scan. This is because the shallow donor concentration N_D found was around $3 \text{ to } 4 \times 10^{15} \text{ cm}^{-3}$ compared to as $3 \text{ to } 4 \times 10^{16} \text{ cm}^{-3}$ for the other samples. In most of the graphs shown before, we notice that the points plotted for sample R16 are obviously lower in concentration. These points are often apart from the others. It was shown by references (65) and (87) that for high concentration of shallow donor N_D , the EL2 is in very low concentration and for N_D low, the EL2 concentration is seen to be higher which seems to agree with our results.

5.5.2 Application of the EL2 Model to CSVT epitaxial growth

By experimental evidences, the thermodynamic considerations indicate that the CSVT deposited epitaxial layers are normally As-rich since the partial vapor pressure of As containing species is higher than partial vapor pressure of Ga_2O (5)(62)(87). Thus because of the arsenic rich condition, the EL2 originates from gallium vacancies V_{Ga} in the crystal (65)(88). The theoretical solidus curves, calculated for simple atomic disorder, indicate an increasing phase extension (As/Ga ratio) with increasing temperature between about 770°C and 1130°C (97). It has been shown that the concentration of the EL2 trap increases with the increase As/Ga ratio in the vapor phase during the growth (65)(86)(97) for LEC, VPE and MOCVD experiments. This suggest that the evolution of EL2 concentration is function of the

off-stoichiometry variation with the deposition temperature as was shown in figure 5.22 with our CSVT system.

In order to analyze further the results obtained above, we have plot the theoretical EL2 concentration (N_3) as function of the off-stoichiometry induced gallium vacancy density (N_1) by using $N_3 = (N_1 - N_2)f$ described from the diagram of figure 5.26. The result is shown in figure 5.27. Here we have assumed the silicon concentration constant ($N_2 = 5.8 \times 10^{16} \text{ cm}^{-3}$) for undoped layers based on previous results (5)(62) and the fraction f of available gallium vacancies contributing to the formation of the EL2 complex was assumed to be 0.0015. The value of f was equal to 0.15 originally from previous results (21)(27), but was decreased to 0.0015 since in the case of vapor phase growth at about 700°C in contrast to melt growth at 1238°C , the EL2 concentrations exhibit a 2 to 3 order magnitude decrease (86). Thus, by varying the off-stoichiometry induced gallium vacancy concentration (N_1) from 6×10^{16} to $1.1 \times 10^{17} \text{ cm}^{-3}$, we find that figure 5.27 is comparable to the DLTS measured EL2 concentrations as function of the deposition temperature in figure 5.22 (64). Figure 5.22 has been replotted with the same scale as in figure 5.27. This can be seen in figure 5.28. The comparison is now obvious between figures 5.27 and 5.28.

The origin of the decrease of the EL2 concentrations for temperature above 850°C in figure 5.22 is still unknown. However, it might be related to a surface decomposition of the epitaxial layer during the growth at these elevated temperatures.

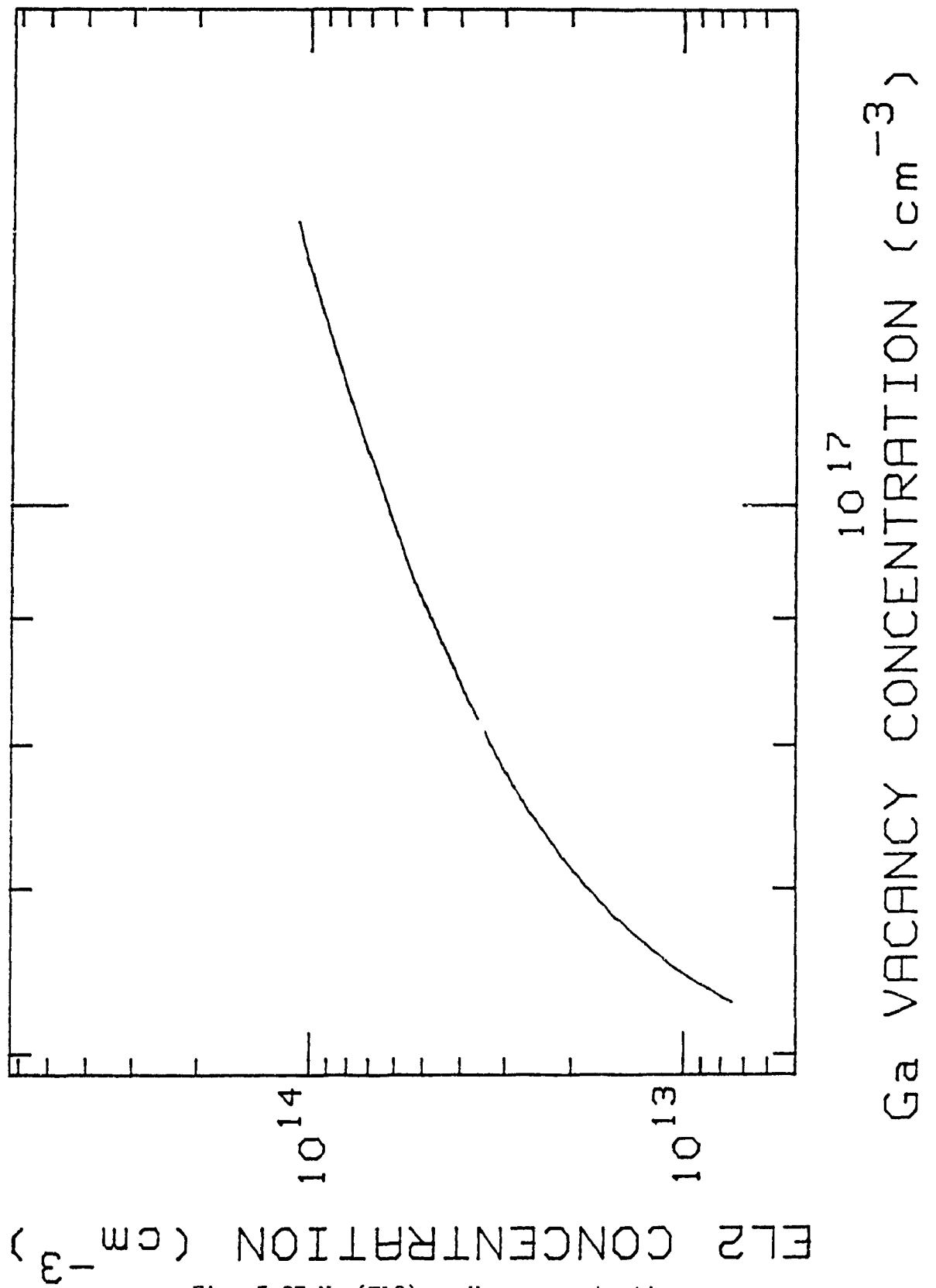


Fig. 5.27 N_r (EL2) vs V_{Ga} concentration

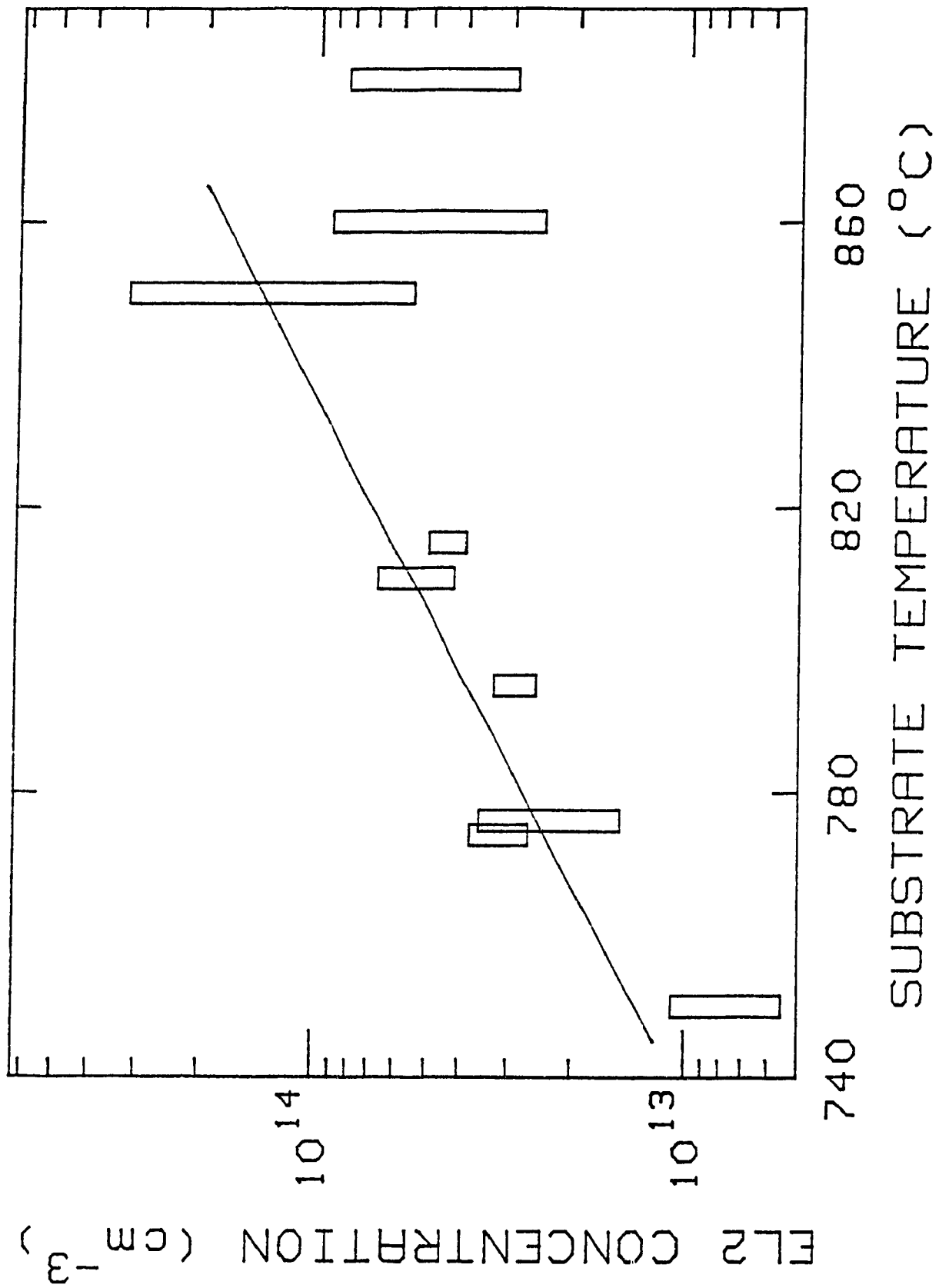


Fig. 5.28 Nr (EL2) vs substrate temperature

5.5.3 The 300K trap ELCS1

As shown in figures 5.18 to 5.20 , we have observed that the ELCS1 trap is not characteristic to the bulk; this trap was shown near the surface only. The source and substrate used were both Si wafers. While reference (79) suggested that ELCS1 trap is a bulk defect⁵ we have shown that the ELCS1 traps in GaAs samples grown by CSVT were seen near the surface only (64). After chemical etching of a few μm in depth from the surface, the ELCS1 (300K) trap has a tendency to vanish while EL2 remain constant throughout the bulk. These 300K levels have been found mainly in wafer submitted to a half and hour heat treatment in the reactor after epitaxial layer growth. As a result the surface structure of these layers might be altered (66). These can be due to out diffusion of impurities or arsenic itself. Therefore, these responsible decompositions of these effect surface layers might be responsible for the 300K (ELCS1) peak.

⁵The samples analyzed in reference (79) were fabricated using the CSVT set-up at Concordia University in Montreal.

6.0 CONCLUSIONS

This report has shown a thorough analysis on the DLTS method for the characterization of deep level traps in GaAs epitaxial layers grown by CSVT. The basic definitions on GaAs crystalline structure were given as an introduction to the other chapters. Then the derivation of capacitance-voltage characteristics of a Schottky barrier was given in order to find the shallow donor concentration N_D . Furthermore, the DLTS method required the capacitance of a diode under reverse bias for the measurement of deep level traps.

The current-voltage characteristics of a Schottky barrier was given also because of the importance for finding the ideality factor and the barrier height. These two parameters were important to identify since they indicated if the diode can operate properly. The ideality factor n between 1 and 1.1 indicated the thermionic current over the barrier and the barrier height ϕ_b greater than 8.2eV allowed to see the EL2 trap level with confidence.

For a thorough understanding of the DLTS method, the general equation of occupation of defect state was given in order to understand Schottky barriers taking deep levels into account. Thus the capacitance transient using a Schottky barrier was derived. This allowed one to the explanation of the DLTS measurements leading to the so called DLTS peaks. This was applied in practice using a capacitance meter, a multi meter and a pulse generator all controlled by the HP-300 computer. Then, once the DLTS peaks were found, the activation energy E_a was determined with the Arrhenius plot $\ln(\tau_n T^2)$ as function of $1000/T$.

Therefore, the experimental procedure to find all parameters by using the DLTS method required first to find the shallow donor concentration N_D by the $C(V)$ method. Then the DLTS peaks were found according to the DLTS measurement procedures. From those peaks, the energies of activation were found. Then the trap concentration N_T was found after the transition region λ was determined and the widths W_0 and W_1 that were easily calculated from simple formulas derived in the text.

The above analysis allowed the determination of the shallow donor concentration N_D and the barrier height ϕ_b of Schottky barriers in order to find the activation energy E_a and the carrier concentration N_T of deep level traps for several samples under investigation.

It has been observed first that the shallow donor concentration N_D was found sometimes with an approximate 30% error due to the surface area of the metal junction of a Schottky barrier and the choice of the points for the linear fit for the slope of $1/C(V)^2$. These errors were taken into account during our experiments. Then ϕ_b and n were found. ϕ_b was found experimentally to be greater than 0.75 eV in all the samples for a proper measurement of EL2. n was also found in the limit required. The values of V_b found with the $C(V)$ measurement and ϕ_b used with the $I(V)$ measurement were compared by multiplying the latter by n . An average 10% error was found. The equipment used for the measurement of N_D and ϕ_b were discussed and were found to be accurate according to the manufacturer when properly calibrated periodically.

The activation energy E_a was determined on several samples. A peak at 300K and a peak at 335K labeled ELCS1 and EL2 respectively for the same emission rate ($\tau_n=0.391$) were found in all samples to be

0.73eV for ELCS1 and 0.8eV for EL2 to which both agree with the literature. These peaks were found when the source was SI whether the substrate was SI or Si-doped. When the source was Si-doped, other peaks with other energies of activation were observed. The probable causes of error in finding E_a was discussed. It has been found that 1% of error in the temperature could be induced due to the platinum resistance. Another cause of error in temperature could be caused by an unconstant increase in the thermal velocity for warming up the cryostat. For a proper measurement of the DLTS peak, the thermal speed was set up at a constant ΔT equal to 1.5K/min.

Finally, the EL2 and ELCS1 traps were analyzed in GaAs epitaxial layers grown by CSVT. It has been shown that the evolution of EL2 concentration was function of the possible off stoichiometry variation with the deposition temperature according to the proposed model discussed. It has been shown also that EL2 is constant throughout the bulk. Then it has been found that ELCS1 was a trap found near the surface of the epitaxial layers grown by CSVT.

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Appendix I: List of Symbols and Results for all Samples

I.1 List of symbols

A	: Arbitrary constant
A^*	: Rickardson constant ($\text{Acm}^{-2}\text{K}^{-2}$)
As	: Arsenide atom
As_{Ga}	: Arsenide in gallium site
α	: Arbitrary constant
β	: Arbitrary constant
C	: Capacitance (F)
C	: Arbitrary constant
C_j	: Junction capacitance of the diode (F)
C_n	: Coefficient capture for electrons (cm^3/s)
C_p	: Coefficient capture for holes (cm^3/s)
$C(t)$: Capacitance as function of time
$C(V)$: Capacitance-Voltage measurement method
CB	: Conduction band
D	: Diameter (cm)
DLTS	: Deep Level Transient Spectroscopy
$\Delta C/C$: Normalize value of $C(t)$
$\Delta\phi_b$: Variation in ϕ_b due to image force lowering (eV)
ΔH_n	: Enthalpy
ΔS_n	: Entropy
Δt	: Pulse width (sec.)
E_a	: Apparent activation energy (eV)
E_b	: Gibbs free energy of transition (eV)
E_c	: Energy level at the conduction band (eV)
E_i	: Ionization energy level (eV)

E_{fs}	: Fermi level (SC) (eV)
E_g	: Band gap (eV)
E_t	: Energy level of a trap (eV)
E_v	: Energy level at the valence band (eV)
eV	: Electron volt
c_n	: Emission rate for electron (sec^{-1})
%er	: Percentage of error between V_b and $n^*\phi_b$
c_p	: Emission rate for hole (sec^{-1})
ϵ_s	: Semiconductor permittivity (F/cm)
$\epsilon(x)$: Electric field at any point x in the SC (V/cm)
ϕ_b	: Barrier height determined by the $I(V)$ measurement (eV)
ϕ_m	: Work function of the metal (eV)
ϕ_n	: Energy difference between E_c and E_{fs} (eV)
ϕ_s	: Work function of the semiconductor (eV)
G	: Conductance ($1/\Omega$)
Ga	: Gallium
G_{sh}	: Conductance shunt ($1/\Omega$)
g^*	: Degeneracy factor
I	: Current (A)
I_{mes}	: Current flowing out of the non-ideal diode (A)
I_{theo}	: Current flowing out of the ideal diode (A)
$I(V)$: Current-voltage measurement method
I_o	: Reverse saturation current (A)
J_s	: Reverse saturation current density (A/cm^2)
K	: Kelvin (K)
k	: Boltzmann constant (J/K)
K_n	: Capture rate for electron (Ccm^3/s)

K_p	: Capture rate for hole
λ	: Transition region (cm)
m_n^*	: Electron mass effective (kg)
m_p^*	: Hole mass effective
μ_n	: Electron mobility ($\text{cm}^2/\text{V-s}$)
μ_p	: Hole mobility
N_A	: Shallow acceptor impurity density (cm^{-3})
N_C	: Effective density of states in conduction band (cm^{-3})
N_D	: Shallow donor impurity density (cm^{-3})
N_{DH}	: Shallow donor impurity density found by Hall measurement (cm^{-3})
N_T	: Deep level trap concentration (cm^{-3})
N_V	: Effective density of states in the valence band (cm^{-3})
n	: Ideality factor
n	: Concentration of electrons in the conduction band (cm^{-3})
$n_T(t)$: Fraction of N_T (cm^{-3})
$n_{T_f}(t)$: Fraction of N_T for trap filling (cm^{-3})
$n_{T_e}(t)$: Fraction of N_T for trap emptying (cm^{-3})
q	: Magnitude of electronic charge (C)
R	: Resistance (Ω)
R_s	: Series resistance (Ω)
R_{sh}	: Shunt resistance (Ω)
S	: Junction area (cm^2)
SC	: Semiconductor
Si	: Silicon atom
SKB	: Schottky barrier
$S(T_M)$: Maximum height of the experimental DLTS peak
σ_n	: Capture cross section for electron (cm^2)

σ_p : Capture cross section for hole

T : Temperature (K)

T_M : Maximum temperature (K)

T_{sub} : Substrate temperature (K)

t : Time (second)

t_n : Rate window (second)

V : External voltage applied (V)

V_{As} : Arsenic vacancy

V_b : Barrier height determined by the C(V) measurement method (eV)

V_i : Contact potential (eV)

V_{Ga} : Gallium vacancy

V_{mes} : Measured voltage at the non-ideal diode (V)

V_{theo} : Voltage of the ideal diode (V)

$\langle V_{thn} \rangle$: Average thermal velocity of an electron (cm/s)

$\langle V_{thp} \rangle$: Average thermal velocity of a hole

W : Space charge region width at voltage V applied (cm)

W_o : Space charge region width at voltage V_o applied

Ω : Ohm (Ω)

X.2 Results for all samples

The results of our experimental data are given in the following table. In the table, "Tsubs" represents the substrate temperature during the epitaxial layer growth for a particular sample. Then the epitaxial layer thickness, the free carrier concentration (N_D) and the mobility (μ) are given. Both N_D and μ were found from the Hall effect measurements. Thus from the table, we can find in each column:

- Ea: The apparent activation energy (eV)
- W_0 : Depth from the junction corresponding to the bias voltage V_0 (μm)
- W_1 : Depth from the junction corresponding to the bias voltage V_1 (μm)
- Rs: The series resistance (Ω)
- Rsh: The shunt resistance ($1 \cdot E6$) (Ω)
- Js: The reverse saturation current ($1 \cdot E-9$) (A/cm^2)
- N_T : Deep level trap concentration ($1 \cdot E14$) (cm^{-3})
- N_D : Concentration of shallow donor ($1 \cdot E15$) (cm^{-3})
- n: The ideality factor
- ϕ_b : Barrier height determined by I(V) measurement (eV)
- V_b : Barrier height determined by C(V) measurement (eV)
- %er: Percentage of error between V_b and $n \cdot \phi_b$.

TABLE I.1: Results for all samples studied

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D369				T _{subs} = 820.0 °C									
Thickness = 8.0 μm				: N _D H =				at/cm ³		: μ =			
.52	0.416	0.269	5.43	3.95	69.8	05.59	13.30	-.75	0	1.008	0.792	0.860	07.7
.72	0.416	0.269				13.10	13.30	-.75	0				
.24	0.925	0.583				07.72	13.30	-7	-2				
.33	0.925	0.583				08.71	13.30	-7	-2				
.39	0.925	0.583				07.78	13.30	-7	-2				
.52	0.925	0.583				03.37	13.30	-7	-2				
.72	0.925	0.583				18.60	13.30	-7	-2				
.24	1.416	1.225	9.96	13.4	0.54	09.46	23.50	-2	-0	1.032	0.790	0.850	04.3
.33	1.416	1.225				10.50	23.50	-2	-0				
.39	1.416	1.225				09.71	23.50	-2	-0				
.52	1.416	1.225				04.66	23.50	-2	-0				
.72	1.416	1.225				17.80	23.50	-2	-0				
.24	1.557	1.416	8.25	2.82	37.2	09.97	25.90	-5	-2	1.006	0.793	0.990	24.1
.33	1.557	1.416				10.70	25.90	-5	-2				
.39	1.557	1.416				09.84	25.90	-5	-2				
.52	1.557	1.416				04.85	25.90	-5	-2				
.72	1.557	1.416				15.37	25.90	-5	-2				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V & n*φ _b
				E6	E-9	E14	E15						

Sample D371_1				T _{subs} = 810.0 °C				1 etch of 1μm					
Thickness = 8.1 μm				:N _D H =				:μ = cm ² /V-s					
.24	1.308	1.167	5.15	0.11	211.	05.43	43.90	-2	0	1.016	0.750	0.840	10.2
.33	1.308	1.167				05.96	43.90	-2	0				
.39	1.308	1.167				05.71	43.90	-2	0				
.72	1.308	1.167	66.4	2.45	163.	18.90	43.90	-2	0	2.151	0.755	---	
.24	1.438	1.308	4.96	2.37	57.8	04.86	46.00	-5	-2	1.034	0.784	0.800	-1.3
.33	1.438	1.308				04.85	46.00	-5	-2				
.39	1.438	1.308				04.96	46.00	-5	-2				
.72	1.438	1.308				14.60	46.00	-5	-2				

Sample D372				T _{subs} = 760.0 °C									
Thickness = 2.5 μm				:N _D H = 3.23E17 at/cm ³				:μ = 1480 cm ² /V-s					
.39	0.341	0.185	1.12	0.51	3.77	11.50	36.60	-2	0	1.120	0.845	0.900	-4.9
.62	0.341	0.185				123.0	36.00	-2	0				
.39	0.438	0.341				07.13	36.00	-4	-2				
.62	0.438	0.341				112.0	36.00	-4	-2				
.39	0.371	0.181	54.1	2.86	5.08	10.60	35.40	-2	0	1.043	0.844	0.850	-3.4
.62	0.371	0.181				114.0	35.40	-2	0				
.39	0.452	0.371				10.70	36.90	-4	-2				
.62	0.452	0.371				151.0	36.90	-4	-2				
.39	0.231	0.137	27.7	3.78	0.15	11.90	63.90	-1.5	0	1.144	0.830	0.850	-10.
.62	0.231	0.137	29.9	4.89	5.34	151.0	63.90	-1.5	0	1.086	0.857	---	

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D372e#1			Tsubs = 760.0 °C						1 etch of 1μm				
Thickness = 2.5 μm			:N _D H = 3.23E17 at/cm ³						:μ = 1480 cm ² /V-s				
.62	1.128	1.077	68.6	2.26	124.	57.30	243.0	-1.5	0	1.175	0.772	---	
.62	1.128	1.077				55.50	243.0	-1.5	-0.08				
.62	1.278	1.077	48.3		4.96	09.85	243.0	-0.5	-0	1.360	0.739	1.260	25.3

Sample D373#2			Tsubs = 810.0 °C										
Thickness = 9.3 μm			:N _D H = 1.53E17 at/cm ³						:μ = 2300 cm ² /V-s				
.62	0.452	0.179	25.2		1.47	05.93	43.20	-5	0	1.094	0.878	0.970	01.0
.39	0.452	0.179					43.20	-5	0				

Sample D374e#2			Tsubs = 760.0 °C						1 etch of 1μm				
Thickness = 3.5 μm			:N _D H = 4.77E17 at/cm ³						:μ = 1640 cm ² /V-s				
.62	1.116	1.073	34.2	3.81	15.6	22.20	274.0	-1.5	0	1.073	0.839	1.020	13.3
.62	1.116	1.073				20.30	274.0	-1.5	-0.08				
.62	1.091	1.073	52.5	2.57	27.5	23.00	274.0	-0.5	-0.08	1.095	0.824	---	

Sample D374Re_2			Tsubs = 760.0 °C						1 etch of 1 μm				
Thickness = 3.5 μm			:N _D H = 4.77E17 at/cm ³						:μ = 1640 cm ² /V-s				
.62	1.139	1.067	24.7	2.99	32.9	11.00	325.0	-1	0	1.097	0.817	0.950	06.0

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D374R_2			Tsubs = 760.0 °C										
Thickness = 3.5 μm			:N _D H = 4.77E17 at/cm ³					:μ = 1640 cm ² /V-s					
.24	1.422	1.023	59.5	12.6	.668	3.920	32.60	-1	0	1.092	0.921	---	
.33	1.422	1.023	56.3			4.100	32.60	-1	0	3.364	0.582	---	
.39	1.422	1.023				3.700	32.60	-1	0				

Sample D374			Tsubs = 760.0 °C										
Thickness = 3.5 μm			:N _D H = 4.77E17 at/cm ³					:μ = 1640 cm ² /V-s					
24	0.555	0.468	24.1	22.4	.215	21.10	35.30	-2	0	1.100	0.920	---	
.33	0.555	0.468				29.16	35.30	-2	0				
.39	0.555	0.468				29.11	35.30	-2	0				
.52	0.555	0.468				12.20	35.30	-2	0				
.24	0.641	0.555				26.20	74.60	-7	-2				
.33	0.641	0.555				42.40	74.60	-7	-2				
.39	0.641	0.555				43.80	74.60	-7	-2				
.52	0.641	0.555				30.20	74.60	-7	-2				

Sample D374_1			Tsubs = 760.0 °C										
Thickness = 3.5 μm			:N _D H = 4.77E17 at/cm ³					:μ = 1640 cm ² /V-s					
.24	0.550	0.507	25.3	14.2	.467	25.70	33.60	-1	0	1.062	0.906	---	
.33	0.550	0.507				23.00	33.60	-1	0				
.39	0.550	0.507				26.90	33.60	-1	0				
.52	0.550	0.507				11.00	33.60	-1	0				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D374_2				Tsubs = 760.0 °C									
Thickness = 3.5 μm				:N _D H = 4.77E17 at/cm ³				:μ = 1640 cm ² /V-s					
.24	0.620	0.550	29.3	5.52	4.33	30.07	54.80	-4	-1	1.095	0.871	---	
.33	0.620	0.550				50.20	54.80	-4	-1				
.39	0.620	0.550				54.40	54.80	-4	-1				
.52	0.620	0.550				29.50	54.80	-4	-1				

Sample D374_1a				Tsubs = 760.0 °C									
Thickness = 3.5 μm				:N _D H = 4.77E17 at/cm ³				:μ = 1640 cm ² /V-s					
.24	0.445	0.408	24.9	5.45	2.40	23.90	52.80	-1	0	1.053	0.887	---	
.33	0.445	0.408	29.4	5.54	4.33	27.90	52.80	-1	0	1.095	0.871	---	
.39	0.445	0.408				27.20	52.80	-1	0				
.52	0.445	0.408				13.70	52.80	-1	0				
.24	0.498	0.445				39.90	89.40	-4	-2				
.33	0.498	0.445				72.10	89.40	-4	-2				
.39	0.498	0.445				76.60	89.40	-4	-2				
.52	0.498	0.445				48.20	89.40	-4	-2				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D375				Tsubs = 810.0 °C									
Thickness = 10.0 μm				:N _D H = 1.87E18 at/cm ³				:μ = cm ² /V-s					
.24	1.316	0.063	41.6	3.28	44.2	1.910	22.80	-2	0	1.281	0.810	---	
.33	1.316	0.063				2.990	22.80	-2	0				
.39	1.316	0.063				3.900	22.80	-2	0				
.52	1.316	0.063				3.610	22.80	-2	0				

Sample D377#1				Tsubs = 780.0 °C									
Thickness = 3.7 μm				:N _D H = 04.0E17 at/cm ³				:μ = 1770 cm ² /V-s					
.72	0.278	0.119	24.6	3.13	7.41	35.90	89.70	-4	0	1.036	0.836	1.010	16.0
.39	0.278	0.119					64.20	-4	0				
.72	1.589	1.540	23.3	2.97	.178	12.60	52.10	-2	0	1.086	0.816	0.920	3.81
.39	1.589	1.540					52.10	-2	0				

Sample D378_1				Tsubs = 780.0 °C					1 etch of 1 μm				
Thickness = 3.8 μm				:N _D H = at/cm ³					:μ = cm ² /V-s				
.62	0.256	0.146	5.39	5.48	345.	14.60	58.40	-2	0	1.021	0.736	0.880	17.1
.62	0.371	0.256	5.50	.181	843.	11.40	64.20	-5	-2	1.075	0.709	0.880	15.3

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample D379#2				T _{subs} = 780.0 °C									
Thickness = 4.2 μm				:N _D H = 2.20E17 at/cm ³				:μ = 1500 cm ² /V-s					
.24	0.857	0.729	48.6		.121	13.30	29.80	-4	-0	1.571	0.822	---	
.33	0.857	0.729				25.20	29.80	-4	0				
.39	0.857	0.729				07.08	29.80	-4	0				
.52	0.857	0.729				03.57	29.80	-4	0				

Sample R2				Tsubs = 776.0 °C					1 etch of 1μm				
Thickness = 10.0 μm				:N _D H = 5.67E16 at/cm ³					:μ = 3680 cm ² /V-s				
.80	1.833	1.276	46.4	38.7	.407	0.284	16.50	-7	0	1.072	0.874	0.960	02.5
.72	1.833	1.276				1.040	16.50	-7	0				
.80	1.833	1.279	37.1	4.77	.245	0.286	16.10	-7	0	1.099	0.832	0.960	05.0
.72	1.833	1.279				0.957	16.10	-7	0				
.80	1.833	1.419				0.290	16.10	-7	-1				
.72	1.833	1.419				1.070	16.10	-7	-1				
			48.7	9.51	1.13		16.50			1.087	0.850	0.970	05.0

Sample R3				T _{subs} = 776.0 °C									
Thickness = 10.0 μm				:N _D H = 4.35E16 at/cm ³				:μ = 3660 cm ² /V-s					
.80	0.738	0.521				0.399	21.11	-3	0	1.200	0.830	---	
.72	0.738	0.521				2.020	21.11	-3	0				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample R5				Tsub _s = 774.0 °C									
Thickness = 09.0 μm				:N _D H = 5.20E16 at/cm ³				:μ = 3390 cm ² /V-s					
					.480		13.50	-7	0	1.138	0.870	1.010	02.1
					.344		25.73	-7	0	1.170	0.881	1.240	20.3
							23.90	-7	0	1.147	0.864	1.030	03.9

Sample R6				Tsub _s = 810.0 °C									
Thickness = 13.0 μm				:N _D H = 3.83E16 at/cm ³				:μ = 4080 cm ² /V-s					
.80	0.572	0.193	31.2		1.08	0.548	38.80	-7	0	1.082	0.860	0.910	02.2
.72	0.572	0.193				1.820	38.80	-7	0				
.80	0.286	0.193				---	38.80	-1	0				
.72	0.286	0.193				2.230	38.80	-1	0				
.80	0.572	0.353				0.548	38.80	-7	-2				
.72	0.572	0.353				1.823	38.80	-7	-2				
.80	0.521	0.182	40.8	17.1	.721	0.511	40.10	-7	0	1.091	0.846	0.920	00.3
.72	0.521	0.182				1.641	40.10	-7	0				

TABLE I.1 (Continued)

Ea	W _O	W ₁	Rs	Rsh	Js	N _T	N _D	V _O	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample R8				T _{subs} = 860.0 °C				1 etch of 1μm					
Thickness = 30.0 μm				:N _D H = 6.66E16 at/cm ³				:μ = 3850 cm ² /V-s					
.80	1.595	1.282	13.4	86.9	.701	0.570	33.80	-7	-1	1.080	0.868	0.890	05.1
.72	1.595	1.282				0.400	33.80	-7	-1				
.80	1.595	1.282				0.526	33.80	-7	-1				
.72	1.595	1.282				0.400	33.80	-7	-1				
.80	1.282	1.194				0.452	38.80	-1	0				
.80	1.282	1.194				0.799	38.80	-1	0				

Sample R10				T _{subs} = 750.0 °C				1 etch of ≈ 1μm					
Thickness = 06.0 μm				:N _D H = 2.90E16 at/cm ³				:μ = 3680 cm ² /V-s					
.80	2.051	1.329	256.	174.	.640	0.071	08.39	-7	0	1.089	0.877	1.300	35.0
.72	2.051	1.329				---	08.39	-7	0				
.80	1.772	1.303				0.052	07.41	-2	0	1.089	0.867	1.000	05.9
.72	1.772	1.303				0.529	07.41	-2	0				
.80	2.760	1.772				0.089	09.63	-7	-2				
.72	2.760	1.772				0.835	09.63	-7	-2				
			205.	10.8	.430					1.080	0.879	---	
			203.	14.5	.350					1.079	0.781	0.980	04.3
			256.	14.6	.402					1.089	0.867	1.000	05.9

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample R16				Tsubs = 860.0 °C									
Thickness = 41.0 μm				: N _D H = 8.15E15 at/cm ³				: μ = 4760 cm ² /V-s					
.80	1.534	0.620	30.4	140.	.626	0.417	03.69	-5	0	1.074	0.880	1.060	12.1
.72	1.534	0.620				0.631	03.69	-5	0				
.80	1.767	0.911				0.516	03.69	-7	-1				
.72	1.767	0.911				0.572	03.69	-7	-1				
.80	1.767	0.911				0.485	03.69	-7	-1				
.72	1.767	0.911				0.608	03.69	-7	-1				
.80	1.985	1.029	33.1	9.64	.907	0.394	02.93	-7	-1	1.095	0.847	0.950	02.4
.72	1.985	1.029				0.461	02.93	-7	-1				
.80	1.985	1.029				0.390	02.93	-7	-1				
.72	1.985	1.029				0.447	02.93	-7	-1				
.80	2.200	1.166	163.	11.0	.861	0.749	0.861	-2	0	1.099	0.887	---	
.72	2.200	1.166				0.110	0.861	-2	0				
.80	3.470	2.450				0.622	1.061	-7	-3				
.72	3.470	2.450				0.097	1.061	-7	-3				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	R _s	R _{sh}	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample B39			T _{subs} = 805.0 °C										
Thickness = 21.0 μm			: N _D H = 7.53E16 at/cm ³					: μ = 3460 cm ² /V-s					
				139.	.381	---	29.10	-5	0	1.087	0.872	1.030	8.66
				4.69	3.63	---	23.30	-4	0	1.089	0.821	0.870	02.3

Sample B41			T _{subs} = 800.0 °C										
Thickness = 20.0 μm			: N _D H = 7.00E16 at/cm ³					: μ = 3530 cm ² /V-s					
.72	0.729	0.223	6.93	11.7	.750	0.660	22.40	-7	0	1.070	0.830	---	

Sample B42			T _{subs} = 800.0 °C										
Thickness = 20.5 μm			: N _D H = 4.30E16 at/cm ³					: μ = 3825 cm ² /V-s					
90	7.050	5.560	28.8	9.38	1.14	0.041	19.90	-7	0	1.087	0.860	0.930	-.52
.72	7.050	5.560				0.215	19.90	-7	0				
90	7.050	5.560				0.049	19.90	-7	0				
72	7.050	5.560				0.215	19.90	-7	0				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample B46			Tsub = 850.0 °C										
Thickness = 70.0 μm			: N _D H = 5.11E16 at/cm ³					: μ = 4150 cm ² /V-s					
.80	0.535	0.230	4.33	2.39	99.0	01.13	32.10	-5	0	1.316	0.757	---	
.72	0.535	0.230				---	32.10	-5	0				
.80	0.663	0.416	5.47		34.6	01.27	27.26	-7	-2	1.310	0.763	---	
.72	0.663	0.416				08.91	27.26	-7	-2				
.80	0.353	0.237				0.806	73.90	-1	0	---	---	0.970	
.72	0.353	0.237				12.40	73.90	-1	0				
.80	1.116	1.035	6.27	13.2	1.07	2.655	40.70	-1	0	1.091	0.854	0.890	-4.5
.72	1.116	1.035				12.30	40.70	-1	0				
.80	1.395	1.196				01.16	40.70	-7	-2				
.72	1.395	1.186				09.10	40.70	-7	-2				
.80	2.475	2.363				0.736	79.20	-1	0	1.083	0.846	0.850	-7.2
.72	2.475	2.363				6.420	79.20	-1	0				
.80	2.737	2.475				0.551	79.20	-5	-1				
.72	2.737	2.475				5.180	79.20	-5	-1				
.80	3.365	3.410				---	22.00	-2	0	1.068	0.894	0.880	-7.8
.72	3.465	3.410				4.761	22.00	-2	0				
.80	3.465	3.465				---	22.00	-7	-2				
.72	3.846	3.465				4.180	22.00	-7	-2				

TABLE 1.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample B47			Tsub _s = 840.0 °C					1 etch of 1μm					
Thickness = 32.0 μm			:N _D H = 1.07E17 at/cm ³					:μ = 3290 cm ² /V-s					
			5.09	6.53	2.81	---	78.40	-5	0	1.094	0.824	0.880	02.4
			5.32	2.94	25.3	---	78.30	-7	0	1.162	0.777	0.830	08.1
			7.90	2.65	40.0	---	71.60	-7	0	1.108	0.757	0.840	00.2

Sample B48			Tsub _s = 860.0 °C					Etch 4.8μm					
Thickness = 50.0 μm			:N _D H = 2.76E16 at/cm ³					:μ = 4260 cm ² /V-s					
.80	5.463	5.077	8.15	15.9	.990	0.385	24.60	-7	0	1.084	0.860	0.940	0.83
.80	5.494	5.156	8.09	6.85	.698	0.247	24.70	-7	-1	1.073	0.854	0.970	5.80

Sample B50			Tsub _s = 815.0 °C					Etch 4.8μm					
Thickness = 18.0 μm			:N _D H = 7.11E16 at/cm ³					:μ = 4290 cm ² /V-s					
30	5.355	5.033	16.5	14.5	1.07	0.388	22.80	-4	0	1.062	0.830	0.880	06.9
			18.0	28.0	.636	---	24.20	-7	0	1.074	0.868	0.990	06.2
			16.9	5.14	1.26	---	36.30	-7	0	1.089	0.853	0.890	04.2

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample B51				Tsub = 880.0 °C									
Thickness = 44.0 μm				: N _D H = 6.90E16 at/cm ³				: μ = 3940 cm ² /V-s					
.80	0.670	0.267	3.61	10.9	53.1	0.292	18.20	-5	0	1.382	0.760	0.940	10.5
.72	0.670	0.267				---	18.20	-5	0				
.80	0.757	0.535				0.403	18.20	-7	-2				
.72	0.757	0.535				2.183	18.20	-7	-2				
.80	0.416	0.267				0.680	18.20	-1	0				
.72	0.416	0.267				2.270	18.20	-1	0				
.80	0.729	0.286	5.92	9.45	1.89	0.274	16.70	-5	0	1.314	0.786	0.910	11.9
.72	0.729	0.286				---	16.70	-5	0				
						---	13.30	-1	0	1.064	0.876	1.330	0.85
						---	13.30	-1	0				
.80	1.433	1.147				0.420	13.30	-7	0				
.72	1.433	1.147				0.229	13.30	-7	0				
.80	2.706	2.382	6.84	10.7	2.09	1.130	14.50	-2	0	1.025	0.911	---	
.72	2.706	2.382				---	14.50	-2	0				
.80						1.230	14.50	-7	-2				
.72						---	14.50	-7	-2				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	R _s	R _{sh}	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample B52			T _{subs} = 760.0 °C										
Thickness = 07.0 μm			: N _D H = 7.79E16 at/cm ³					: μ = 3580 cm ² /V-s					
.80			41.8	6.69	2.08	0.294	17.10	-2	0	1.130	0.862	0.910	6.57
.72						1.950	17.10	-2	0				
.80						0.273	19.50	-7	-3				
.72						1.653	19.50	-7	-3				

Sample B57			T _{subs} = 840.0 °C										
Thickness = 26.0 μm			: N _D H = 8.98E16 at/cm ³					: μ = 3000 cm ² /V-s					
.80	0.932	0.397	7.18	3.46	1.23	0.337	10.70	-5	0	1.109	0.864	0.910	5.03
.72	0.932	0.397				1.660	10.70	-5	0				

Sample B53			T _{subs} = 750.0 °C										
Thickness = 06.0 μm			: N _D H = 5.35E16 at/cm ³					: μ = 3300 cm ² /V-s					
.72	1.296	0.341	91.2	35.3	1.504	0.448	13.40	-7	0	1.088	0.870	0.910	04.0
.72	1.296	0.511				0.445	13.40	-7	-1				
.72	0.972	0.341				0.403	11.70	-3	0				

Sample B60			T _{subs} = 800.0 °C										
Thickness = 15.0 μm			: N _D H = 6.07E16 at/cm ³					: μ = 3080 cm ² /V-s					
.80	1.643	1.092	36.2	11.3	1.68	0.254	16.30	-7	0	1.091	0.867	0.980	3.61
.72	1.643	1.092				0.989	16.30	-7	0				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n•φ _b
				E6	E-9	E14	E15						

Sample AS40MEP14.4			Tsub _s = 750.0 °C										
Thickness = 14.4 μm			:N _D H =			at/cm ³			:μ =				
.72	1.268	0.675	24.2	27.3	11.8	2.944	04.60	-2	0	1.265	0.785	0.970	02.3
.72	1.827	1.268				2.810		-5	-2				
.72	1.827	0.675				3.263		-5	-0				
.72	1.664	1.029				3.110		-4	-1				

Sample AS10MEP3.3			Tsub _s = 750.0 °C										
Thickness = 3.3 μm			:N _D H =			at/cm ³			:μ =				
.72	1.165	0.681	26.1	14.2	19.0	2.070	08.50	-6	-2	1.350	0.777	1.000	04.8
.72	1.109	0.420				2.180		-5	0				
.72	1.109	0.716				1.343		-5	-3				

Sample AS2CM49C.2			Tsub _s = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =				
.72	1.493	0.612	66.5	6.49	17.8	2.620	04.40	-5	0	1.166	0.783	1.420	14.2
.72	1.493	1.093				2.260		-5	-2				

Sample ALU7M139_2			Tsub _s = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =				
.72	0.829	0.565	23.1	408.	3.97	7.780	29.00	-5	0	1.380	0.930	1.000	12.5
.72	0.496	0.388				2.270		-4	-2				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample ALUSMIN,2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72	1.042	0.690				0.149	09.30	-5	-1				
.72	0.690	0.489				0.679	06.40	-1	0				

Sample AU20M18,2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72	0.907	0.580	63.8	3.66	15.4	1.770	03.30	-2	0	1.138	0.840	1.020	06.7
.72	1.318	0.580				1.920	06.30	-6	0				

Sample AL20M18,2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
72	0.695	0.372	198.	10.0	370.	7.380	10.00	-2	0	1.897	0.787	---	
72	1.011	0.372				7.160	12.00	-6	0	1.897	7.280	1.160	16.0

Sample AU20M18,2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72	0.789	0.169	47.1	17.0	285.	5.770	08.10	-2	0	1.062	0.757	0.990	23.0
72	0.987	0.169				4.760	09.10	-6	0				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample 2AS2CM13.2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72	0.489	0.435				03.03	13.00	-2	0				
.72	1.078	0.489				03.09	13.00	-5	-2				
.72	1.078	0.435				03.17	13.00	-5	0				
.72	1.078	4.899				03.06	13.00	-5	-2				

Sample AUsM1N			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72			28.6	3.85	336.	0.521	09.31	-2	0	1.500	0.738	2.260	

Sample 2AS2CM13.2			Tsubs = 750.0 °C										
Thickness =			:N _D H =			at/cm ³			:μ =			cm ² /V-s	
.72	0.586	0.408				08.84	26.00	-1	0				
.72	0.946	0.408				09.96	26.00	-5	0				
.72	0.748	0.408				09.87	26.00	-3	0				
.72	0.946	0.934				07.48	26.00	-5	-4				
.72	0.834	0.701				11.10	26.00	-4	-2				

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample EPI6MIN, 1				Tsubs = 750.0 °C									
Thickness =				:N _D H =				at/cm ³		:μ =			
.72	0.643	0.295				06.99	27.00	-5	0			2.530	

Sample ASGA9MIN, 3				Tsubs = 750.0 °C									
Thickness =				:N _D H =				at/cm ³		:μ =			
.72						14.30	74.60	-5	0			1.350	
.72						08.90	74.60	-1	0				
.72						10.90	74.60	-4	-2				

Sample EPI8MIN, 3				Tsubs = 750.0 °C									
Thickness =				:N _D H =				at/cm ³		:μ =			
.72	0.315	0.133				15.40	99.00	-5	0			1.166	
.72	0.192	0.133				12.00	99.00	-1	0				
.72	0.270	0.133				15.50	99.00	-3	0				

Sample 2AS9MIN, 1				Tsubs = 750.0 °C									
Thickness =				:N _D H =				at/cm ³		:μ =			
.72	0.514	0.199				03.18	58.00	-5	0			0.960	

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	Js	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample S29E12			T _{subs} = 797.0 °C										
Thickness = 22.0 μm			N _D H = 4.68E16 at/cm ³					μ = 3430 cm ² /V-s					
.72	0.738	0.416				2.990	07.05	-2	0	1.082	0.800	1.070	23.6
.72	0.641	0.356				3.180	07.48	-2	0	1.028	0.910	1.000	06.9
.72	1.043	0.641				1.830	07.90	-7	-2	1.025	0.910	0.810	
.72	1.785	1.458				0.419	07.37	-0	0	1.082	0.380	1.070	12.4
.72	2.226	1.785				0.559	08.16	-7	-2	1.047	0.976	1.490	
.72	1.817	1.479				0.285	06.55	-2	0	1.047	0.976	1.080	05.7
.80	1.817	1.479				0.287	06.55	-2	0				
.72	2.463	2.257				0.514	19.20	-2	-0	1.120	0.839	0.880	06.3
.72	2.725	2.463				0.332	20.90	-7	-2	1.120	0.839	1.170	
.72	2.451	2.257				0.216	19.10	-2	-0	1.300	0.792	0.870	-15

TABLE I.1 (Continued)

Ea	W ₀	W ₁	Rs	Rsh	J _s	N _T	N _D	V ₀	V ₁	n	φ _b	V _b	%err
eV	μm	μm	Ω	Ω	A/cm ²	at/cm ³	at/cm ³	Volt	Volt		eV	eV	V _b & n*φ _b
				E6	E-9	E14	E15						

Sample S30R3			Tsubs = 778.0 °C										
Thickness = 22.0 μm			: N _D H = 2.15E16 at/cm ³					: μ = 3330 cm ² /V-s					
.72	0.243	0.238				2.450	21.19	-2	0	1.055	0.895	0.850	10.0
.80	0.248	0.238				0.518	21.19	-2	0				
.72	0.695	0.428				1.860	21.40	-7	-2	1.096	0.864	0.770	
.80	0.695	0.428				0.380	21.40	-7	-2				
.72	0.476	0.238				2.200	21.90	-2	0	1.096	0.864	0.840	-11.
.80	0.476	0.238				0.441	21.90	-2	0				
.72	1.672	1.376				0.546	09.52	-2	0	1.080	0.910	1.140	
.72	1.683	1.379				0.542	09.04	-2	0	1.131	0.882	0.920	07.7
.72	2.397	2.235				0.496	27.30	-2	0	1.100	0.884	1.040	06.9
.72	2.614	2.397				0.475	31.10	-7	-2	1.100	0.884	1.490	

APPENDIX II: Space charge region derivation for a Schottky barrier

In an n-type non degenerated and uniformly doped SC of a Schottky barrier, the Poisson equation for the space charge region can be written as (35)

$$\frac{d^2V}{dx^2} = -\frac{q}{\epsilon_s} [p(x) - n(x) + N_D] \quad (II.1)$$

where ϵ_s is the SC permittivity, N_D is the shallow donor concentration¹, and $n(x)$ and $p(x)$ are the electron and hole concentrations at any point x in the SC respectively, and are given by (35)

$$n(x) = n_0 e^{qV(x)/kT} \quad (II.2a)$$

and

$$p(x) = p_0 e^{-qV(x)/kT} \quad (II.2b)$$

where n_0 and p_0 are the intrinsic carrier concentrations, q is the electronic charge of an electron, k is the Boltzmann's constant, T is the absolute temperature and $V(x)$ is the voltage at any point x in the SC.

Equation II.1 can be simplified by neglecting the contribution of carriers (p-n) to the space charge region. Thus assuming complete ionization of the impurity ($N_D^+ = N_D$), we have

¹ Here N_A is neglected since $N_D \gg N_A$.

$$\frac{d^2V}{dx^2} = -\frac{q}{\epsilon_s} N_D \quad 0 < x < W \quad (\text{II.3a})$$

$$= 0 \quad x > 0 \quad (\text{II.3b})$$

where ϵ_s is the semiconductor permittivity, N_D the donor concentration, and n and p are the electron and hole concentration in the semiconductor respectively.

Now, referring to figure II.1 (36), we can solve the above equation by using the point form of Gauss law, $d\epsilon/dx = (q/\epsilon_s)N_D$, as follows:

$$\int_{\epsilon_m}^0 d\epsilon = \frac{-q}{\epsilon_s} N_D \int_0^W dx \quad 0 < x < W \quad (\text{II.4})$$

where the solution is

$$\epsilon_m = \frac{-q}{\epsilon_s} N_D W \quad (\text{II.5})$$

and

$$\epsilon(x) = \epsilon_m \left(1 - \frac{x}{W} \right) \quad (\text{II.6})$$

according to figure II.1c. Note that for the case where the electric field has to be found at $\epsilon(W-\lambda)$, we have to change the limit of integration of equation II.3 as follows;

$$\int_{\epsilon(W-\lambda)}^0 d\epsilon = \frac{-q}{\epsilon_s} N_D \int_{(W-\lambda)}^W dx \quad 0 < x < W-\lambda \quad (\text{II.7})$$

where the solution is

$$\epsilon(W-\lambda) = - \frac{qN_D}{\epsilon_s} \lambda \quad (II.8)$$

With the electric field it is now possible to relate the contact potential V_i by the relation;

$$\epsilon(x) = - \frac{dV(x)}{dx} \quad (II.9)$$

Thus, substituting equation II.6 into equation II.9 and solving for $V(x)$ with the boundary conditions: $V = 0$ at $x = W$ we get,

$$V(x) = \int_0^x \epsilon(x) dx = - \frac{qN_D}{2\epsilon_s} W^2 \left(1 - \frac{x}{W}\right)^2 \quad (II.10)$$

The contact potential is obtained for $V(x) = 0$ in equation II.10. Thus,

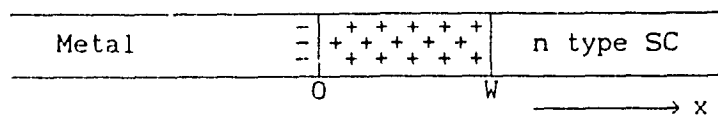
$$V_i = \frac{-q}{2\epsilon_s} N_D W^2 \quad (II.11)$$

Rearranging equation II.11 we obtain the space charge region at zero bias as

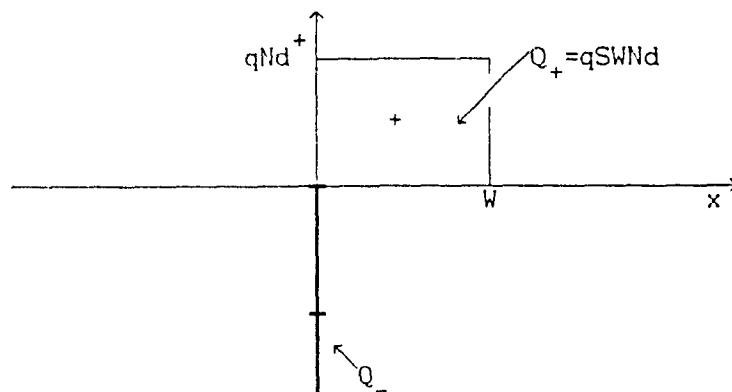
$$W = \left[\frac{2\epsilon_s}{qN_D} V_i \right]^{1/2} \quad (II.12)$$

Finally, with an external bias voltage V (reverse or forward), the space charge region can be written as follows (36);

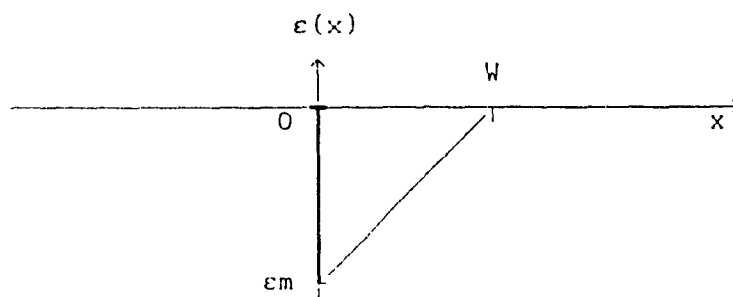
$$W = \left[\frac{2\epsilon_s}{qN_D} (V_i - V) \right]^{1/2} \quad (II.13)$$



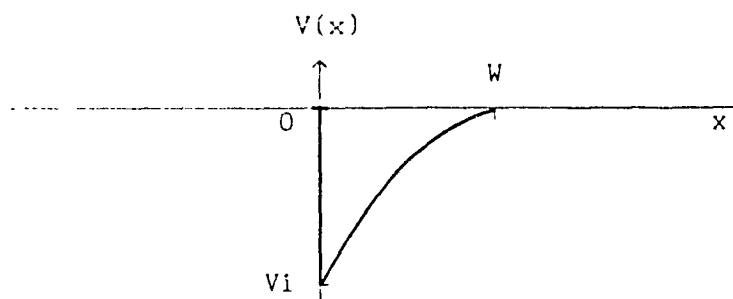
a) Transition region



b) Charge density



c) Electric field distribution



d) Potential distribution

Figure II. Schematic representation of a Schottky Barrier

a) Transition region b) charge density Q

c) Electric field distribution

d) Potential distribution

A more accurate result is obtained when $n(x)$ is taken into account and $p(x)$ is neglected in equation II.1, thus (27)

$$W = \left[\frac{2\epsilon_s}{qN_D} (V_i - kT/q - V) \right]^{1/2} \quad (II.14)$$

Now referring to figure II.1, it is seen that the charge Q in the transition region W (36) is given by

$$Q_+ = qSWN_D = S \left[2\epsilon_s q N_D (V_i - kT/q - V) \right]^{1/2} \quad (II.15)$$

where S is the surface cross sectional area of the junction.

With the charge Q in the transition region, the capacitance of the junction is easily found by using (27) (28) the relation

$$C = dQ/dV \quad (II.16)$$

Thus differentiating equation II.15 with respect to V we have the junction capacitance as

$$C_j = S \left[\frac{q\epsilon_s}{2(V_i - (kT/q) - V)} N_D \right]^{1/2} \quad (II.17)$$

where (kT/q) is the contribution of the majority carriers to the space charge.

It is clear here that the reverse bias structure forms a parallel plate capacitor comprising a layer of dielectric thickness W and dielectric constant ϵ_s between two conducting electrodes (28).

APPENDIX III: The image force barrier lowering

The image force barrier lowering known as the Schottky effect can be understood by referring to figure III.1 below. If an electron is at a distance x from the metal, an electric field perpendicular to the metal surface is created. This field is calculated by assuming a positive image charge q located at a distance $-x$ inside the metal. This creates the potential energy Fx of the electron relative to an electron at infinity. The potential energy Fx is thus added to the theoretical barrier energy $-q\phi$ giving the resultant barrier shown by the hard line on the figure. The maximum barrier height energy occurs at a distance x_m from the metal surface. The barrier height is therefore lowered by an amount (39)

$$\Delta\phi_b = \left[\frac{q^3 N_D}{8\pi^2 \epsilon_s^3} (V_i - V) \right]^{1/4} \quad (\text{III.1})$$

where ϵ_s is the permittivity and V the applied voltage.

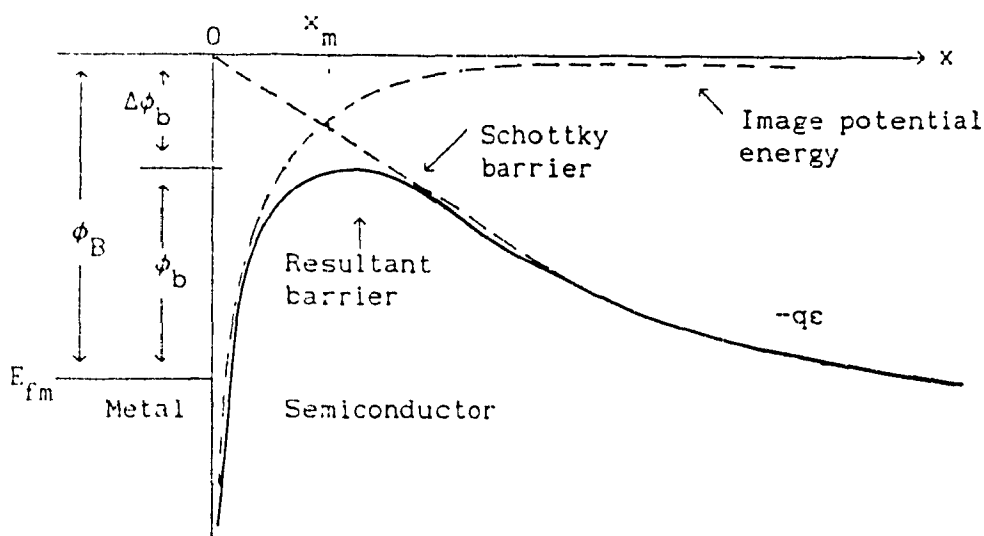


Fig. V.1 Diagram of the image force lowering of the barrier

Appendix IV: Emission rate at thermal equilibrium

An electron trap exchange carriers with the conduction band and a hole trap exchange carriers with the valence band. For the case of an electron trap, equation 4.1 can be rewritten as

$$\frac{dn_T}{dt} = nC_n(N_T - n_T) - enn_T \quad (\text{IV.1})$$

At *thermal equilibrium* the probability f_T that the state is occupied is given by the ratio of the concentration of defects occupied by electrons n_T to the total trap concentration N_T , thus (50)

$$f_T = \frac{n_T}{N_T} \quad (\text{IV.2})$$

which can be described by the Fermi-Dirac statistics

Recalling for the present case, that the Fermi-Dirac statistic states the probability that an energy level E_T is occupied by an electron at a given temperature T (50), thus

$$f_T = \frac{1}{1 + g_n \cdot e^{-\{(E_F - E_T)/kT\}}} \quad (\text{IV.3})$$

where g_n is the degeneracy factor and E_F is the Fermi level.

Now, substituting equation IV.2 into equation IV.1 we get

$$\frac{df_T}{dt} = -enn_T + nC_n(1 - f_T) \quad (\text{IV.4})$$

Consequently, the value of the emission rate e_n can be found by using the principle of detailed balance, which states that in thermal equilibrium the carrier capture and the emission for each electron state must be equal (16) (54). Thus, at equilibrium $df_T/dt = 0$ and equation IV.4 becomes

$$e_n f_T = n C_n (1 - f_T) \quad (IV.5)$$

Substituting equation IV.5 into equation IV.3 and solving for e_n we obtain

$$e_n = n C_n g_n^* e^{-((E_F - E_T)/kT)} \quad (IV.6)$$

where the electron concentration n is given by (57)

$$n = N_c e^{[-(E_C - E_F)/kT]} \quad (IV.7)$$

with N_c the effective density of states at the conduction band edge given by (57)

$$N_c = 2 \left(\frac{2 \pi m_n^* kT}{h^2} \right)^{3/2} \quad (IV.8)$$

where h is the Plank's constant. Now with $C_n = \sigma_n \langle V_{thn} \rangle$ and IV.7 into equation IV.6 we find the required value of e_n as (16)(17)(54)

$$e_n = 1/\tau_n = N_c \sigma_n \langle V_{thn} \rangle g_n^* e^{-(E_D/kT)} \quad (IV.9)$$

where E_D is the Gibbs free energy of transition between the energy levels E_T and E_C ($E_D = E_C - E_T$).

Similarly, for an hole trap we obtain;

$$\tau_p = 1/\tau_p = N_v \sigma_p \langle V_{thp} \rangle (g_p^\bullet)^{-1} e^{(-E_D/kT)} \quad (IV.10)$$

Appendix V: Determination of the transition region λ

The transition region λ can be found by integrating Poisson's equation where λ is defined in the space charge region as shown in figure 4.2b. After some mathematical manipulations, equation II.3 can be rewritten as

$$\frac{d}{dx} \left(x \frac{dV}{dx} - V \right) = - x \frac{\rho(x)}{\epsilon dx} \quad (V.1)$$

Integrating the above equation from $(W-\lambda)$ to W we find λ as follows;

$$\left[x \frac{dV}{dx} - V \right]_{(W-\lambda)}^W = - \frac{1}{\epsilon} \int_{(W-\lambda)}^W x \rho(x) dx \quad (V.2)$$

which leads to

$$V(W-\lambda) - V(W) + (W-\lambda)\epsilon(W-\lambda) = \frac{qNd}{2\epsilon} \{W^2 - (W-\lambda)^2\} \quad (V.3)$$

Now, from figure 4.2 it can be seen that $\{V(W-\lambda) - V(W)\}$ correspond to $[(E_F - E_T)/q]$ and $\epsilon(W-\lambda)$ is simply equal to $(qNd\lambda/\epsilon)$ (equation II.8 appendix II). Therefore,

$$\frac{(E_F - E_T)}{q} - (W-\lambda) \frac{-2qNd\lambda}{2\epsilon} = \frac{qNd}{2\epsilon} [W^2 - (W-\lambda)^2] \quad (V.4)$$

By simplifying this equation we obtain the transition region λ as (56)

$$\lambda = \left[\frac{2\epsilon}{q^2 Nd} (E_F - E_T) \right]^{1/2} \quad (V.5)$$

APPENDIX VI: Determination of $\Delta C/C_0$

In order to find $\Delta C/C_0$, we have to find the variation of the defect concentration between the limits $(W_1 - \lambda_1)$ and $(W_0 - \lambda_0)$ as shown in figure 4.4c. This is done by solving Poisson's equation or equation V.1 with the limits shown in figure 4.4c. Thus, we have

$$V(t) = \int_0^{W_0} x \frac{q}{\epsilon_s} N_D dx + \int_0^{W_1 - \lambda_1} x \frac{q}{\epsilon_s} N_T dx + \int_{W_1 - \lambda_1}^{W_0 - \lambda_0} x \frac{q}{\epsilon_s} N_T (1 - e^{-t/\tau_n}) dx \quad (VI.1)$$

The solution of the above equation is therefore

$$V(t) = \frac{q}{2\epsilon_s} N_D W_0^2 + \frac{q}{2\epsilon_s} N_T (W_1 - \lambda_1)^2 + \frac{q}{2\epsilon_s} N_T [(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2] (1 - e^{-t/\tau_n}) \quad (VI.2)$$

At $t=0$, the initial condition, we consider the initial width W_0 , the capacitance C_0 and $(W_1 - \lambda_1) = x_0$. Therefore equation VI.2 is rewritten as

$$V(0) = \frac{q}{2\epsilon_s} N_D W_0^2 + \frac{q}{2\epsilon_s} N_T (W_1 - \lambda_1)^2 = \frac{q}{2\epsilon_s} N_D W_0^2 + \frac{q}{2\epsilon_s} N_T x_0^2 \quad (VI.3)$$

At $V(0)$ we have an initial value of $(V_i + V_o)$ as shown in figure 4.4a which is therefore replaced in equation VI.3. We can rearrange the above equation in the following form as

$$\frac{2(V_o + V_i)\epsilon_s}{qN_D W_0^2} = \left[1 + \frac{N_T}{N_D} \left(\frac{x_0}{W_0} \right)^2 \right] \quad (VI.4)$$

Now with C_0 equals to ϵ_s/W_0 substituted in equation VI.4 we obtain

$$C_0 \left[\frac{2(V_0 + V_1)}{qN_D \epsilon_s} \right]^{1/2} = \left[1 + \frac{N_T}{N_D} \left(\frac{x_0}{W_0} \right)^2 \right]^{1/2} \quad (VI.5)$$

The root of the right hand side of this equation can be eliminated by expanding it in binomial expansion (59) and keeping the first order term since the total trap concentration is a lot smaller than the shallow donor concentration (i.e. $N_T \ll N_D$). Therefore, equation VI.5 becomes

$$C_0 \left[\frac{2(V_0 + V_1)}{qN_D \epsilon_s} \right]^{1/2} \approx \left[1 + \frac{N_T}{2N_D} \left(\frac{x_0}{W_0} \right)^2 \right] \quad (VI.6)$$

Now, at some value of t we consider the value of $V_0 + V_1$ constant since the variation in voltage is negligible due to the small change in nT_e between $(W_0 - \lambda_0)$ and $(W_1 - \lambda_1)$ (i.e. $V(t) \approx (V_0 + V_1)$). Thus proceeding the same ways as the above we obtain

$$C^2 \left[\frac{2(V_0 + V_1)}{qN_D \epsilon_s} \right] = 1 + \frac{N_T}{N_D} \left(\frac{x_0}{W_0} \right)^2 + \frac{N_T}{N_D} \frac{\{(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (VI.7)$$

Now, using the binomial expansion in equation VI.7 and keeping the first order term we get

$$C \left[\frac{2(V_0 + V_1)}{qN_D \epsilon_s} \right]^{1/2} = \left[1 + \frac{N_T}{2N_D} \left(\frac{x_0}{W_0} \right)^2 \right] + \frac{N_T}{2N_D} \frac{\{(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (VI.8)$$

We notice that the first two terms in the square bracket on the right hand side of the above equation is equation VI.6. This leads to

$$(C - C_0) \left[\frac{2(V_0 + V_1)}{qN_D \epsilon_s} \right]^{1/2} = \frac{N_T}{2N_D} \frac{\{(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (VI.9)$$

Finally, the term inside the left hand side bracket in equation VI.9 is the value of $1/C_0$ by comparing to equation II.17. This is justified by rewriting equation VI.6 in the following form;

$$C_0 = \left[\frac{q\epsilon_s}{2(V_0 + V_1)} \left\{ N_D + N_T \left(\frac{x_0}{W_0} \right)^2 \right\} \right] \quad (VI.10)$$

Since $N_T \ll N_D$ and $x_0 \ll W_0$, N_D remains and N_T is neglected. Therefore, equation VI.9 becomes (58)

$$\frac{\Delta C}{C_0} = \frac{C - C_0}{C_0} = \frac{N_T}{2N_D} \frac{\{(W_0 - \lambda_0)^2 - (W_1 - \lambda_1)^2\}}{W_0^2} (1 - e^{-t/\tau_n}) \quad (VI.11)$$

which the normalized variation of the capacitance between $(W_0 - \lambda_0)$ and $(W_1 - \lambda_1)$ due to trap defect when a bias pulse is applied to the Schottky barrier under reverse bias.

APPENDIX VII: Arrhenius Plot and Rate Window

VII.1 Arrhenius plot

The relation $1/\tau_n$ was given by equation 4.14. Now rewriting equation 4.14 and taking the natural logarithm on both sides we get

$$\ln(1) = \ln [\tau_n N_c \sigma_n \langle V_{th} \rangle e^{-E_a/kT}] \quad (VII.1)$$

The above equation can be rearranged by multiplying it by T^2/T^2 inside the bracket of the right hand side, thus we obtain

$$\ln(\tau_n T^2) = \frac{E_a}{kT} - \ln \left(\frac{N_c \sigma_n \langle V_{th} \rangle}{T^2} \right) \quad (VII.2)$$

where N_c and $\langle V_{th} \rangle$ can be simplified as $\alpha T^{3/2}$ and $\beta T^{1/2}$ respectively where

$$\alpha = 2 \left(\frac{2\pi m n k}{h^2} \right)^{3/2} \quad \text{and} \quad \beta = \{3K/m_n\}^{1/2} \quad (VII.3)$$

Therefore, the second term of the right hand side in equation VII.2 is independent of the temperature, thus

$$\ln(\tau_n T^2) = \frac{E_a}{kT} - \ln\{\alpha\beta\sigma_n\} \quad (VII.4)$$

Thus, the slope $\ln(\tau_n T^2)$ vs $(1000/T)$ is called the Arrhenius plot (6).

Its slope allow us to find the apparent activation energy E_a of the deep level trap and the capture cross section is obtain by the intercept with the y axis.

In fact, equation VII.4 is a straight line of the form $y = ax + b$ where x represents $1/T$. The slope is then given by

$$a = E_a/k \quad (\text{VII.5a})$$

and the intercept;

$$b = -\ln\{\alpha\beta\sigma_n\} \quad (\text{VII.5b})$$

which cuts the y axis. We recall here that a and b can be found from the least square method (31).

VII.2 Rate window

The rate window τ_n can be found by differentiating the normalized value of the DLTS peak $S(T)/C_0$ and equate it to zero in order to find its maximum. Thus,

$$\frac{S(T)}{C_0} = \left[\frac{N_T}{2N_D} \frac{\{(W_0-\lambda)^2 - (W_1-\lambda)^2\}}{W_0^2} \right] (e^{-t_1/\tau_n} - e^{-t_2/\tau_n}) \quad (\text{VII.6})$$

or

$$\frac{S(T)}{C_0} = \left[\frac{N_T}{2N_D} \frac{\{(W_0-\lambda)^2 - (W_1-\lambda)^2\}}{W_0^2} \right] (e^{-t_1\tau_n(T)} - e^{-t_2\tau_n(T)}) \quad (\text{VII.7})$$

Thus, differentiating with respect to temperature T we have

$$\frac{d}{dT} \frac{S(T)}{C_0} = \frac{d}{dT} \left[\frac{N_T}{2N_D} \frac{\{(W_0-\lambda)^2 - (W_1-\lambda)^2\}}{W_0^2} \right] (e^{-t_1\tau_n(T)} - e^{-t_2\tau_n(T)}) = 0 \quad (\text{VII.8})$$

Therefore

$$\frac{d}{dT} \frac{S(T)}{C_0} = \left[-t_1 \frac{de_n(T)}{dT} e^{-t_1 e_n(T)} + t_2 \frac{de_n(T)}{dT} e^{-t_2 e_n(T)} \right] = 0 \quad (\text{VII.9})$$

thus

$$\frac{de_n(T)}{dT} \left[-t_1 e^{-t_1 e_n(T)} + t_2 e^{-t_2 e_n(T)} \right] = 0 \quad (\text{VII.10})$$

We can now rewrite the above equation as follows

$$t_1 e^{-t_1 e_n(T)} = t_2 e^{-t_2 e_n(T)} \quad (\text{VII.11})$$

or

$$t_2/t_1 = e^{e_n(T)[t_2-t_1]} \quad (\text{VII.12})$$

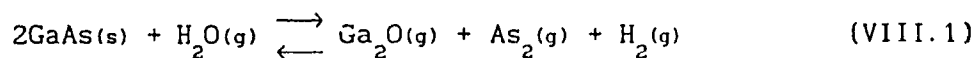
Finally, rearranging the above equation we obtain the rate window as

$$\tau_n = 1/e_n = \frac{[t_2 - t_1]}{\ln(t_2/t_1)} \quad (\text{VII.13})$$

APPENDIX VIII: Summary on epitaxial layer grown by CSVT technique

The closed space vapor transport (CSVT) is a chemical transport between source and substrate separated by a fused silica spacer plate. For GaAs, water is used as the transport reagent operating at atmospheric pressure and moderates temperatures which make a cost effective procedure. The reaction used for the transport of GaAs is:

(5)(62)



The source and substrate may be both semi-insulating (SI) type or Si-doped GaAs n-type. For the epitaxial growth of GaAs on GaAs, this reaction is happening at two places in the system; on the surface of GaAs source at temperature T_1 and, on the surface of GaAs substrate at temperature T_2 . The source temperature is higher than the temperature substrate by 40°C and the equilibrium is displaced to the left onto the substrate surface resulting in GaAs deposition onto the epitaxial layer.

The epitaxial layer set-up consists of a rectangular cross section ($6.8 \times 6.8 \text{ cm}^2$) fused silica chamber containing two graphite blocks as heat susceptors sandwiching between them the GaAs source and substrate separated by a thin fused silica spacer on the order of 0.3mm. One end of this reaction chamber, designed to accommodate 5cm diameter slice, is sealed while the other side is equipped with a fused silica taper joint containing the gas and thermocouple connections. The heat source is a set of 2KW globar (SiC) heating elements. The temperatures are

controlled by two thermocouples positioned in appropriate wells inside of the graphite blocks. The transport agent is wet hydrogen containing triply distilled water vapor corresponding to a saturator temperature of 0°C. The diagram of the CSVT system used for the growth of GaAs epitaxial layer is shown in figure VIII.1 (62).

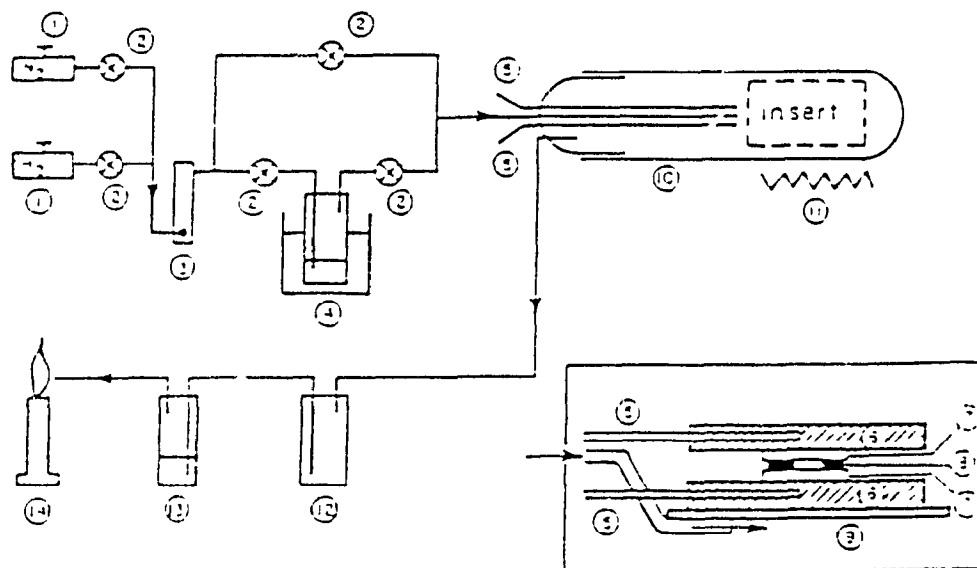


Fig VIII.1 Diagram of the CSVT system: (1) N₂ and H₂ gas cylinders; (2) valves; (3) fluxmeter; (4) water saturator; (5) thermocouples; (6) graphite blocs; (7) GaAs source and substrate; (8) fused silica spacer; (9) fused silica supporting plate; (10) fused silica reactor; (11) 2000W tungsten-hallogen lamp; (12) trap; (13) glycerol bubbler; (14) burner.

Appendix IX: Results for temperature regulator for DLTS

TABLE IX.1: Readings for R at the cryostat tail and at the sample

Cryostat R1 (Ω)	Sample R2 (Ω)	% error R1 & R2	Cryostat R1 (Ω)	Sample R2 (Ω)	% error R1 & R2
21.6	23.9	-9.62	88.0	87.86	0.46
22.0	24.2	-9.10	90.0	89.5	0.56
27.0	27.4	-1.46	95.0	94.5	0.53
30.0	29.9	0.33	97.0	96.6	0.62
33.0	32.7	0.92	100.0	99.1	0.91
36.0	35.6	1.23	103.0	102.1	0.88
40.0	39.4	1.52	105.0	104.1	0.86
44.0	43.5	1.15	108.0	107.2	0.75
47.0	46.4	1.29	110.0	109.2	0.73
50.0	49.3	0.02	113.0	112.1	0.80
53.0	52.4	1.34	115.0	114.1	0.79
55.0	54.4	1.10	118.0	117.1	0.77
58.0	57.5	0.87	121.0	120.0	0.83
61.0	60.5	0.83	123.0	121.9	0.90
65.0	64.5	0.77	125.0	123.9	0.89
70.0	69.5	0.72	127.0	125.9	0.87
75.0	74.5	0.67	130.0	128.8	0.93
79.0	80.7	-2.10	133.0	131.7	0.99
80.0	81.8	-2.2	135.0	133.6	1.05
82.0	83.7	-2.03	139.0	137.4	1.16
84.0	84.6	-0.71	142.0	140.4	1.14
86.0	84.5	0.58	145.0	143.3	1.18

TABLE IX.2: Results from circuit of fig. IX.II

V1 (-) volt	V2 (+) volt	V3 volt	DT (K)	V1-V2 volt	V1 (-) volt	V2 (+) volt	V3 volt	DT (K)	V1-V2 volt
2.89	2.81	9.90	1.21	-0.08	6.60	6.54	9.44	1.88	-0.06
3.05	3.05	13.90	1.28	-0.00	6.75	6.69	9.90	1.86	-0.06
3.22	3.20	12.20	1.51	-0.02	6.90	6.85	10.83	1.81	-0.05
3.40	3.37	10.04	2.00	-0.03	7.00	6.95	11.25	1.80	-0.05
3.58	3.50	9.66	2.34	-0.08	7.20	7.16	11.45	1.87	-0.04
3.76	3.68	9.66	2.49	-0.08	7.35	7.30	10.57	1.91	-0.05
3.90	3.81	9.71	2.40	-0.09	7.50	7.44	10.14	1.94	-0.06
4.00	3.93	9.46	2.22	-0.07	7.60	7.54	9.98	1.93	-0.06
4.15	4.10	10.30	2.05	-0.05	7.75	7.69	10.36	1.86	-0.06
4.27	4.23	10.68	1.99	-0.05	7.90	7.85	11.00	1.82	-0.05
4.46	4.41	9.80	2.04	-0.05	8.10	8.04	10.44	1.78	-0.06
4.65	4.59	9.27	2.07	-0.06	8.30	8.26	11.36	1.78	-0.04
4.88	4.82	9.37	2.03	-0.06	8.50	8.47	11.70	2.19	-0.03
5.00	4.95	9.90	2.00	-0.05	8.60	8.57	11.79	2.08	-0.03
5.20	5.15	10.50	1.96	-0.05	8.70	8.67	12.22	1.97	-0.03
5.36	5.30	10.47	1.97	-0.06	8.90	8.88	12.34	1.90	-0.02
5.50	5.45	10.85	2.00	-0.05	9.10	9.06	11.45	1.95	-0.04
5.73	5.67	9.96	2.02	-0.06	9.40	9.38	12.20	3.62	----
5.93	5.86	9.96	2.00	-0.07	9.60	9.58	12.10	3.15	-0.02
6.00	5.95	9.85	1.98	-0.05	9.70	9.67	11.64	2.45	-0.03
6.25	6.19	9.90	1.93	-0.06	9.80	9.76	11.40	2.23	-0.04
6.42	6.36	9.51	1.92	-0.06	9.90	9.85	11.63	2.10	-0.05

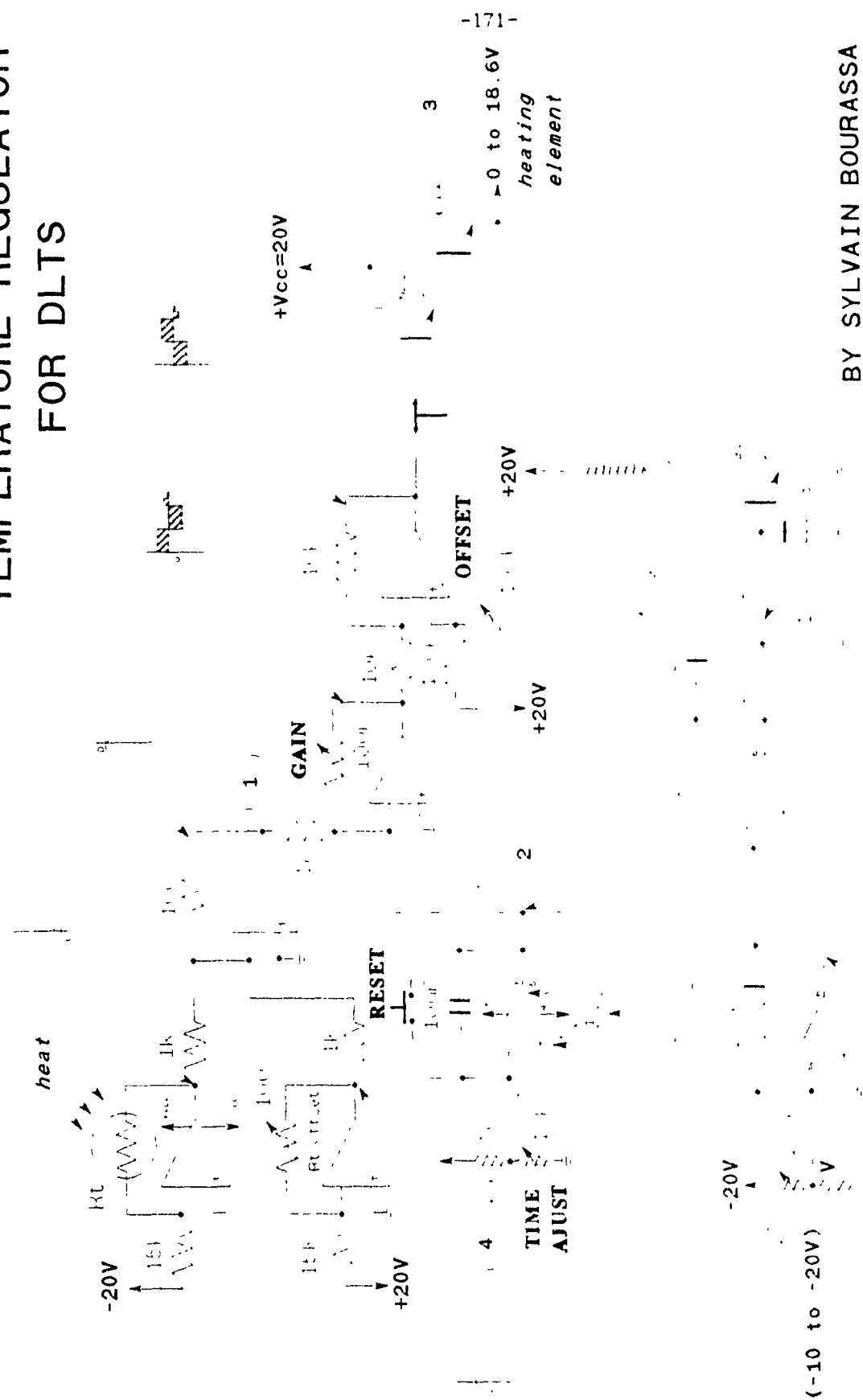
TABLE IX.2: (continued)

V1 (-) volt	V2 (+) volt	V3 volt	DT (K)	V1-V2 volt	V1 (-) volt	V2 (+) volt	V3 volt	DT (K)	V1-V2 volt
10.00	9.69	11.8	2.01	-0.04	12.80	12.80	16.10	1.31	0.00
10.10	10.60	11.60	1.85	-0.04	12.90	12.94	15.80	1.30	0.04
10.30	10.26	11.70	1.69	-0.04	13.10	13.04	10.06	1.50	-0.06
10.50	10.45	11.09	1.61	-0.05	13.40	13.34	13.26	1.26	-0.06
10.60	10.54	10.19	1.56	-0.06	13.45	13.50	18.20	1.02	0.05
10.80	10.77	12.58	1.40	-0.03	13.55	13.58	16.50	1.11	0.03
10.90	10.89	14.07	1.45	-0.01	13.70	13.65	10.14	1.22	-0.05
11.00	11.00	14.42	1.48	0.00	13.80	13.71	10.16	1.44	-0.09
11.10	11.09	12.50	1.51	-0.01	13.90	13.88	13.75	1.45	-0.02
11.30	11.23	9.86	1.62	-0.07	14.00	14.02	16.34	1.32	0.02
11.50	11.43	10.70	1.48	-0.07	14.10	14.13	17.32	1.31	0.03
11.60	11.58	13.50	1.25	-0.02	14.25	14.31	18.30	1.95	0.06
11.70	11.67	12.40	1.20	-0.03	14.40	14.36	11.70	2.01	-0.04
11.80	11.76	12.46	1.23	-0.04	14.55	14.42	9.31	2.08	-0.13
11.90	11.85	10.94	1.29	-0.05	14.60	14.47	9.38	2.03	-0.13
12.00	11.96	11.58	1.35	-0.04	14.70	14.63	11.32	1.44	-0.07
12.10	12.08	12.90	1.35	-0.02	14.75	14.73	14.55	1.11	-0.02
12.20	12.22	15.68	1.36	0.02	14.80	14.86	19.29	0.81	0.06
12.30	12.31	13.96	1.40	0.01	14.85	14.96	19.27	1.01	0.01
12.45	12.41	11.30	1.53	-0.04	15.00	15.04	19.29	1.46	0.04
12.60	12.51	10.07	1.63	-0.09	15.10	15.15	15.41	1.76	0.05
12.70	12.65	11.50	1.50	-0.05	15.20	15.18	13.26	1.96	-0.02

TABLE IX.2: (continued)

V1 (-) volt	V2 (+) volt	V3 volt	D1 (K)	V1-V2 volt	V1 (-) volt	V2 (+) volt	V3 volt	DT (K)	V1-V2 volt
15.30	15.26	12.43	1.90	-0.04	17.30	17.31	16.30	0.97	0.00
15.40	15.37	13.29	1.52	-0.03	17.40	17.53	19.26	0.83	0.13
15.45	15.44	14.40	1.42	-0.01	17.50	17.61	19.26	1.11	0.11
15.50	15.51	15.38	1.25	0.01	17.60	17.68	19.27	1.28	0.08
15.55	15.57	16.18	1.12	0.02	17.70	17.78	19.26	1.55	0.08
15.60	15.62	16.27	1.13	0.02	17.80	17.99	19.24	2.56	0.19
15.70	15.71	14.44	1.18	0.01	17.85	18.05	19.25	2.27	0.10
15.85	15.77	9.57	1.24	-0.08	17.86	18.14	19.25	2.27	0.28
15.90	15.81	9.64	1.21	-0.09					
15.95	15.99	17.38	0.88	0.04					
16.00	16.04	17.90	0.84	0.04					
16.10	16.14	17.83	0.92	0.04					
16.15	16.20	18.68	1.17	0.05					
16.20	16.25	18.34	1.35	0.05					
16.30	16.33	15.40	1.52	0.03					
16.40	16.36	12.57	1.63	-0.04					
16.50	16.47	12.90	1.55	-0.03					
16.60	16.63	16.77	1.15	0.03					
16.70	16.68	12.87	1.15	-0.02					
16.80	16.77	12.80	1.13	-0.03					
16.90	16.99	15.79	0.90	0.00					
17.00	17.04	17.90	0.84	0.04					

TEMPERATURE REGULATOR FOR DLTS



BY SYLVAIN BOURASSA

Figure IX.1

APPENDIX X: Schottky barrier fabrication

This appendix gives the steps to follow for the fabrication of a Schottky barrier diode on a GaAs epitaxial layer at Concordia University in the Electrical Engineering Solid State Device Research Laboratory.

A- Sample cleaning procedure

- 1- Rinse the slice in boiling trichloroethane for five minutes.
- 2- Rinse the slice in boiling acetone for five minutes.
- 3- Rinse the slice in boiling methanol (CH_3OH) for five minutes.
- 4- Dip the slice in HF 20% (HF + distilled water) for 30 sec.
- 5- Rinse the slice in running deionized water for 30 sec.
- 6- Dry with gas nitrogen.

B- Annealing for ohmic contact

- 1- Put the sample inside the glass oven.
- 2- Let the nitrogen (gas) flow through the oven for 30 sec. The flow rate is 30. DO NOT FORGET TO LIGHT UP THE GAS BURNER.
- 3- Heat up the heating element for five min. under nitrogen (put the variac to 20).
- 4- While heating up, plug in the thermocouple.
- 5- Put hydrogen (for about two min.) and then increase the variac to maximum until, 20mV (500°C) is read on the voltmeter.
- 6- Keep the 20mV reading constant for 2min. (Readjust the variac if necessary).
- 7- Turn off the variac and the hydrogen and put back the nitrogen (gas) and let it cool off for 20 minutes.

8- Check the ohmic contact with the curve tracer.

C- Pd-Al Schottky contact

i) Photo resist

- 1- Clean up the sample: repeat step A.
- 2- Meanwhile, prepare the negative photo resist under yellow light : two negative photo resist for one thinner .
- 3- Adjust the temperature of the oven to 120°C and turn on the UV mask aligner.
- 4- Put the sample in the oven for five min.
- 5- Take out the sample of the oven and apply the photo resist:
 - Put a piece of tape on the spinner and lay the sample on it.
 - Dry the sample with nitrogen (gas) before applying the photo resist.
 - Put a few drops of negative photo resist on the sample and spin at 3000 rpm for 15 sec.
 - Clean up the spinner.
- 6- Put the sample back into the oven at 80°C for 15 min.
- 7- Take the sample out of the oven and align the dots on the sample using the mask aligner (UV for 15 sec.).
- 8- Then develop into the developer for 30 sec. and more if necessary.
- 9- Rinse in running water (90°C) for one minute or more if necessary and dry with nitrogen (gas).
- 10- Put the sample back into the oven at 80°C for 15 min.

ii) Electroless solution preparation

1- a) Prepare the PdCl_2 electroless solution:

- Dissolve 0.3 g of PdCl_2 in 9ml of HCl concentrate.
- Mix the above solution in 9ml of deionized water.
- Pour the obtained solution in 864ml of acetic acid.
- Add 28ml of HF 49%.

b) Pour the electroless solution in a beecher and steer slowly with a magnetic agitator.

2- Prepare three beecher with --> 1-HCl, 2-DI water, 3-DI water.

- a- Dip in HCl for one min.
- b- Dip in water to stop the reaction.
- c- Rinse in water for 30 sec.
- d- Dry the sample with nitrogen (gas).

3- Put the sample on the support and soak in the solution for four min. without agitating.

4- Rinse in DI water and repeat step 2 b, c, and d.

iii) Evaporation

1- Put the sample on the special support for evaporation purpose.

2- Starting off the evaporation with the EDWARDS vacuum evaporator:

- a- The three valves of the evaporator are closed and the water is running then switch to rotary pump.
- b- Open the backing valve to a minimum of 30 min. before performing the evaporation.-->clean up the oil.
- c- Put to diff rot pump and wait for vacuum.

3- Install the support inside the bell jar:

- a- Let the air flow in the bell jar by opening the air

valve.

- b- Place an Al-pellet on the heating element and put the support inside the bell jar.
- c- Put the bell jar to its original place.
- d- Close the air valve and open the roughing valve.
- e- While the vacuum is taking place, pour some liquid nitrogen in the liquid nitrogen trap on the left side of the evaporator and wait for the primary vacuum inside the bell jar ($>10^{-2}$ torr).
- f- When primary vacuum is done, close the roughing valve.
- g- Open the main valve and wait until the secondary vacuum is reached to a maximum (10^{-6} to 10^{-7} torr).

4- Performing the evaporation:

- a- When the secondary vacuum is reached, add more liquid nitrogen. Heat up the element by increasing slowly the potentiometer. Check so that the vacuum (scale) remains as low as possible when increasing the current flowing through the heating element. Set up the potentiometer until the current element reaches 30A and let evaporate for 20 sec.
- b- To cool down the sample wait 15 min. under vacuum.
- c- Close the main valve and open the air valve. Let the air flow in until it is possible to remove the bell jar from the evaporator case. Then remove the sample.
- d- When the evaporation experiment is finished:

A- If by pass

-Close the air valve and the main valve.

-Open the roughing valve.

-Switch off the Diff-pump.

B- If for a long period of time

-Close the air valve and the main valve.

-Open the roughing valve.

-Switch off the diff-pump.

-Wait half a day.

-Close the main valve.

-Close the backing valve.

-Switch off the rotary pump.

-Turn off the running water.

iv) Photo resist removal

1- Dip the sample in hot trichloroethane for a few minutes until flaws are observed on the photo resist surface.

2- Take a swab-stick and rub gently until the photo resist is completely removed (if necessary).

3- Finally, check the electrical properties of the Schottky barrier has been made.

S.B.